Impact of GNSS Orbit Modelling on Reference Frame Parameters

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Overview

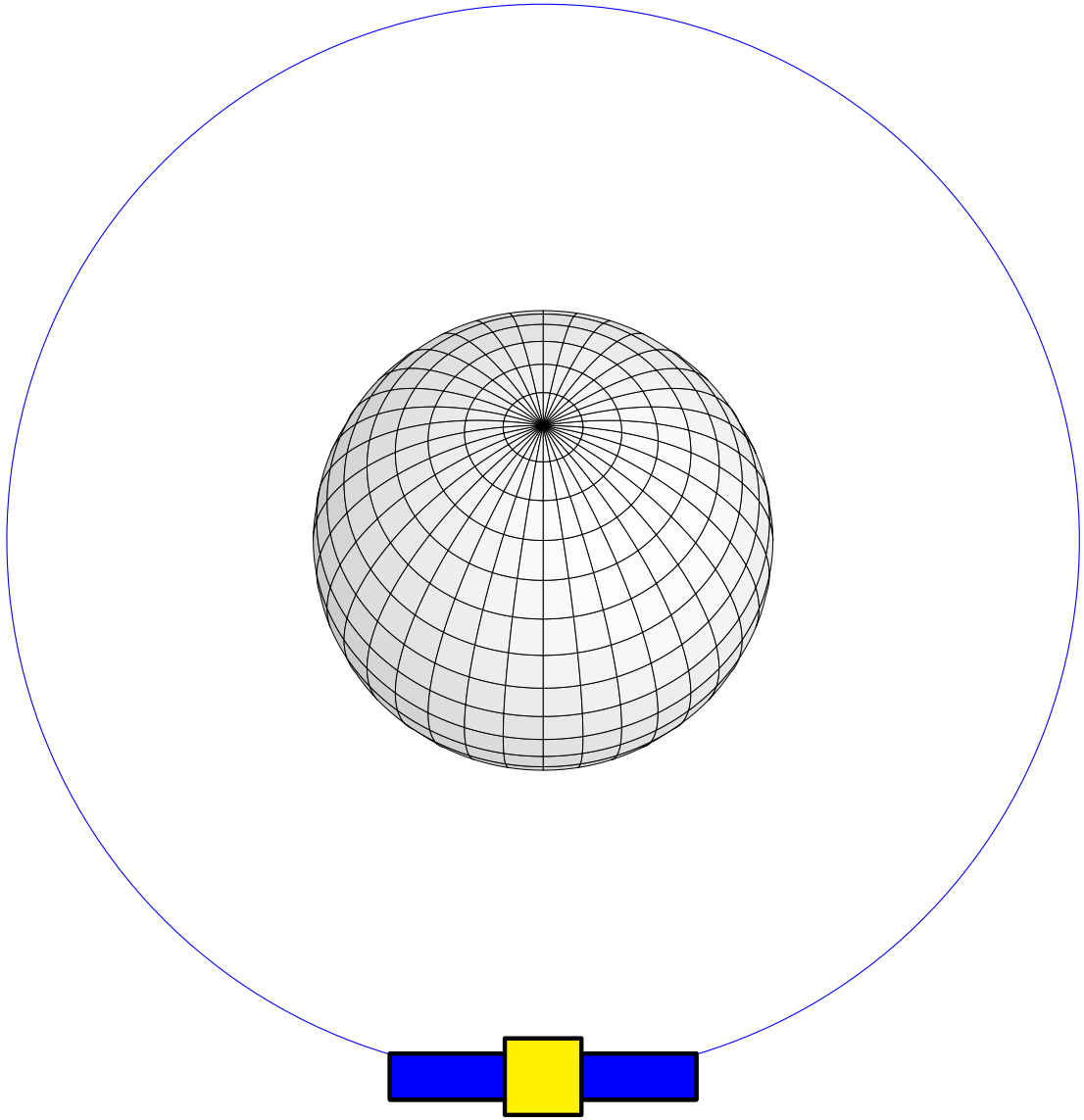
Solar Radiation Pressure for GNSS Satellites

Impact on the GNSS Satellite orbits

Impact on the Reference Frame Parameters

Long–Arc Solutions

Observing the satellite from the Sun



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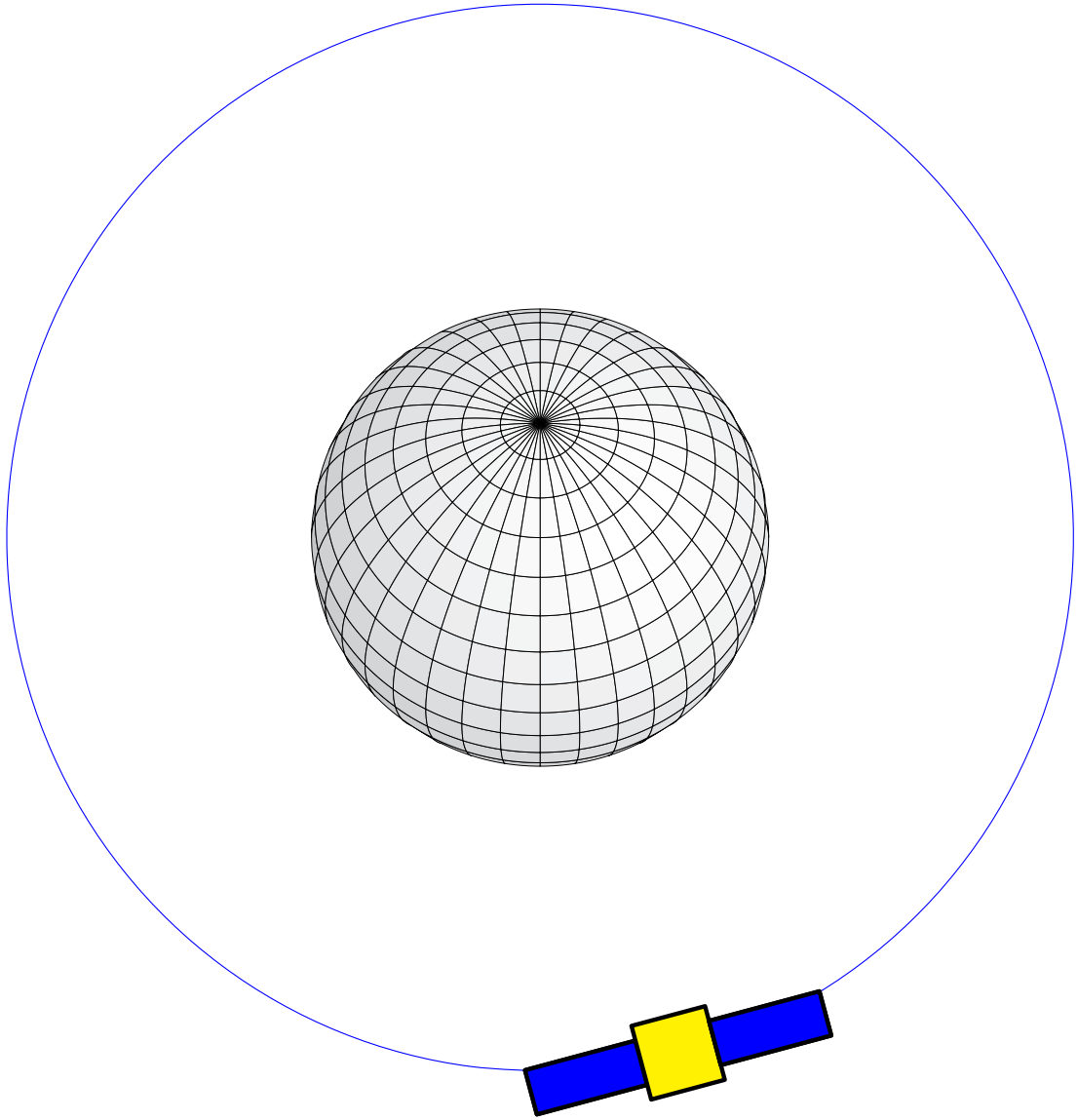

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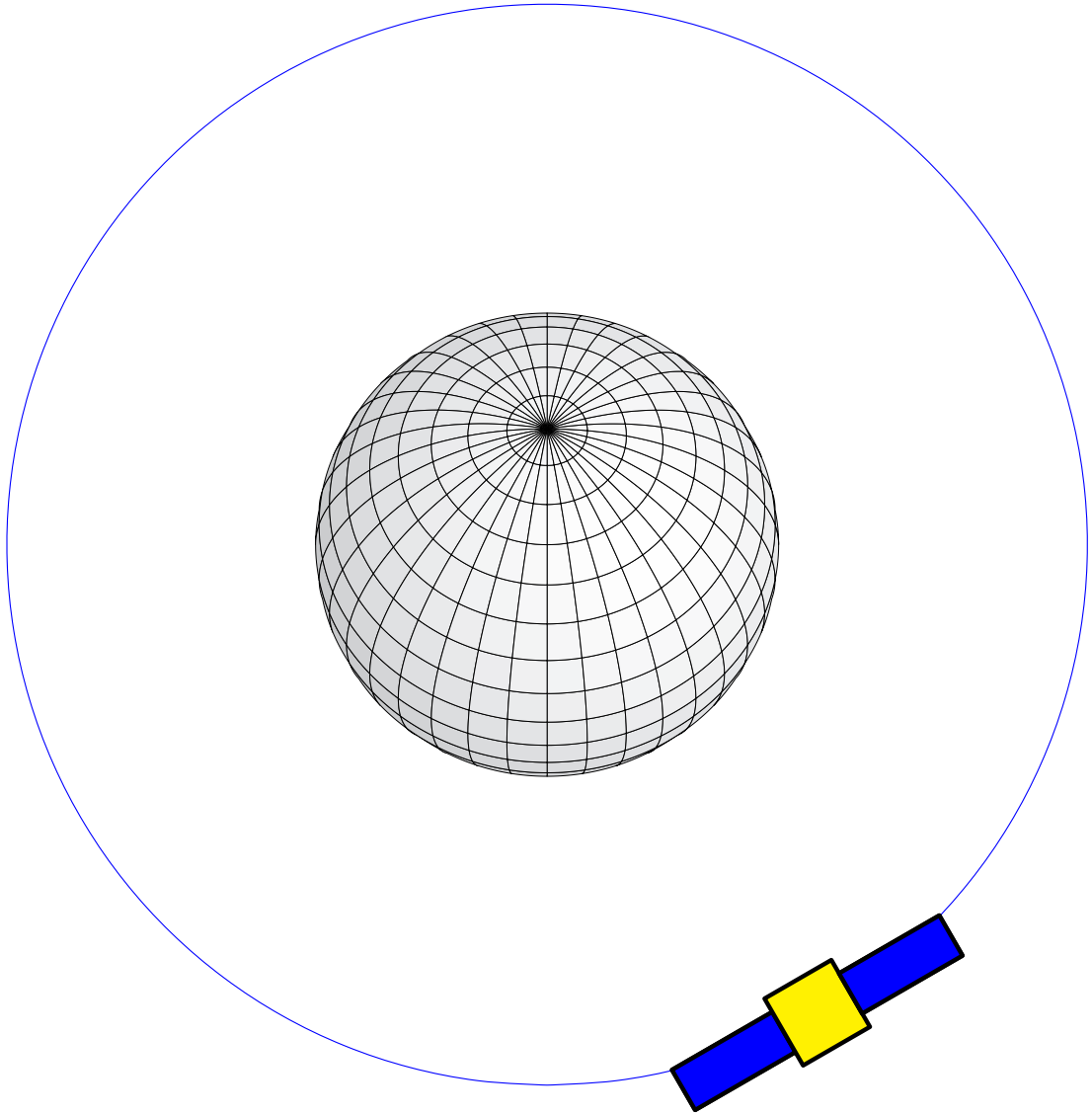

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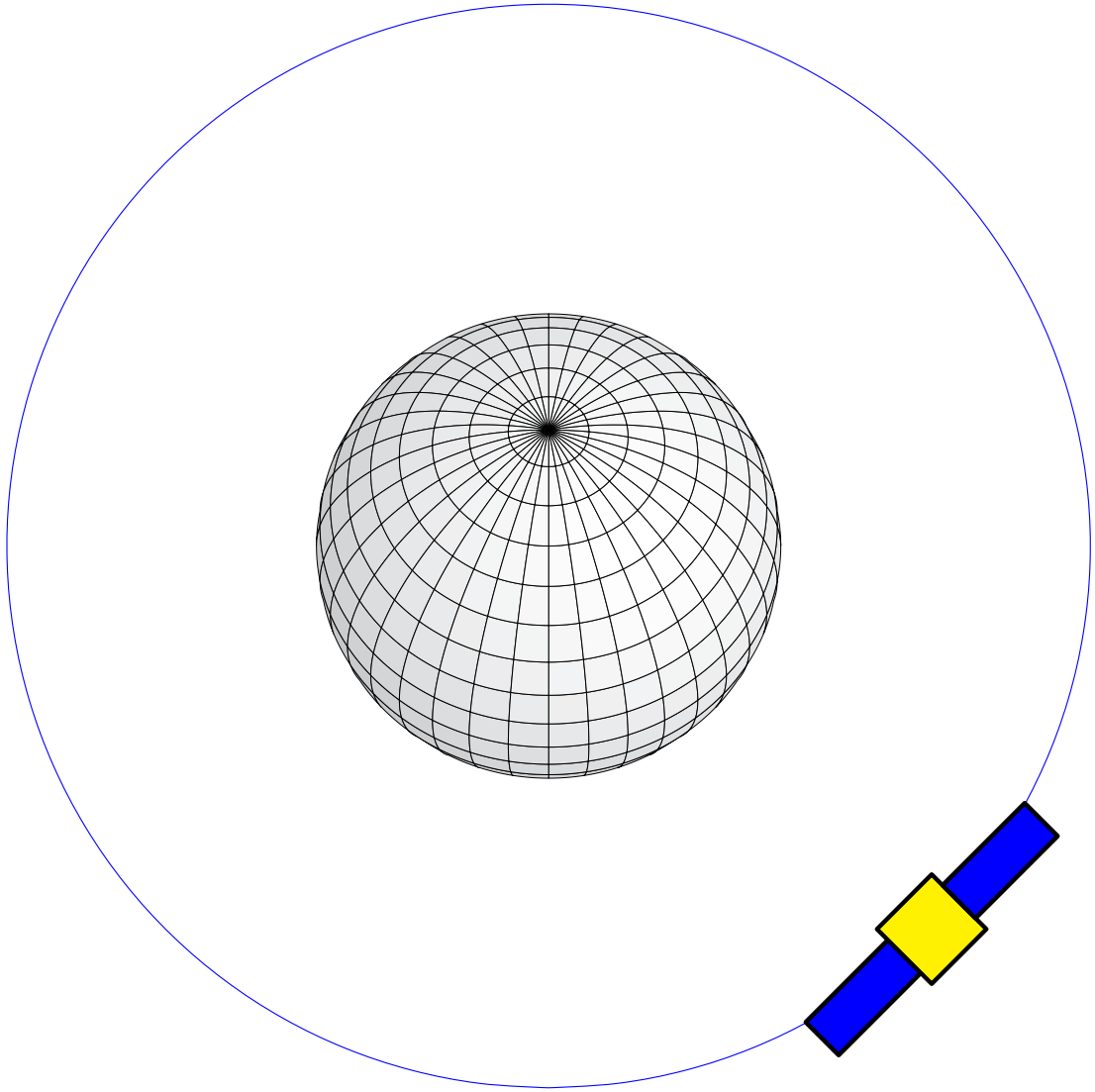

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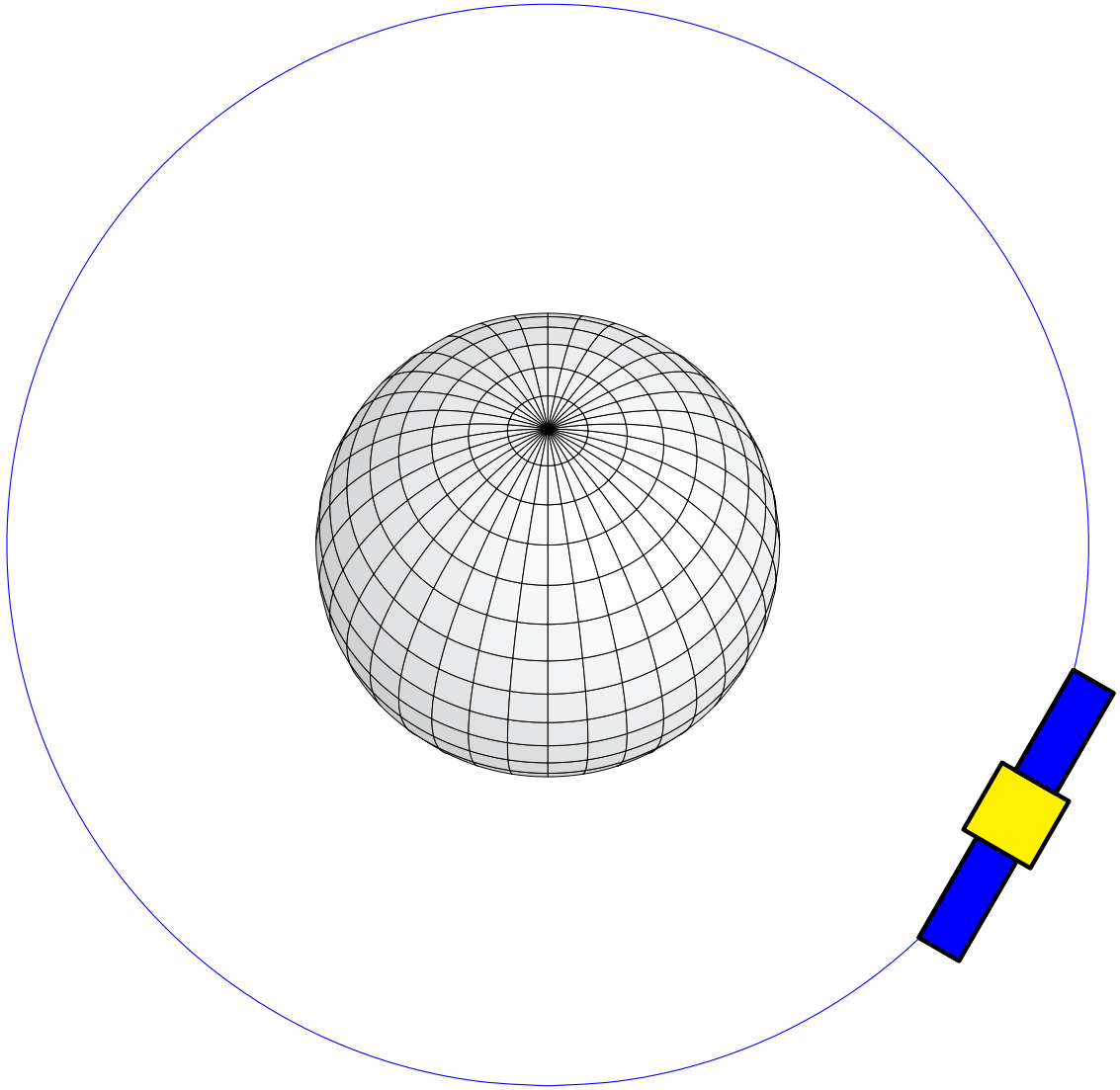

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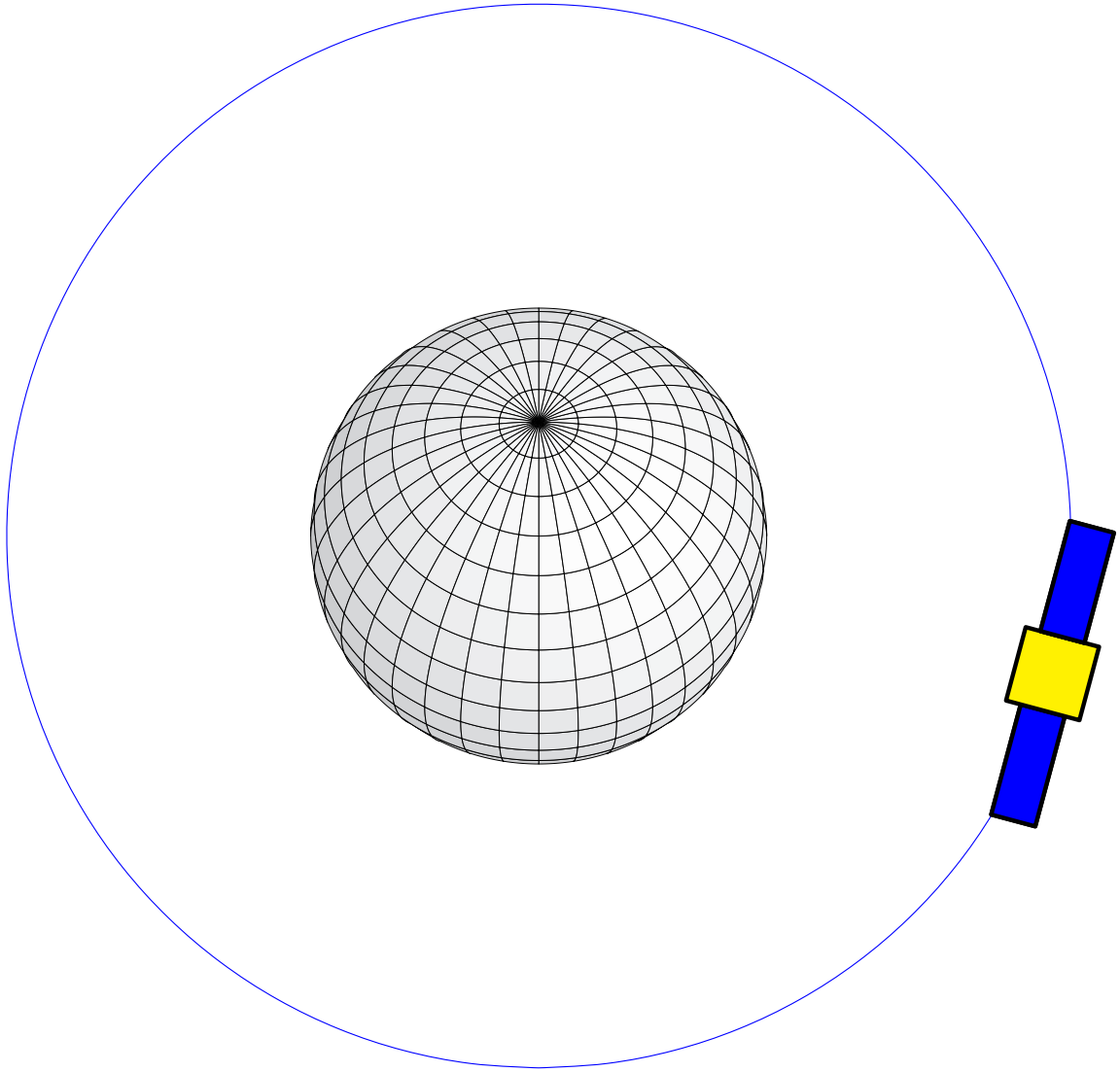

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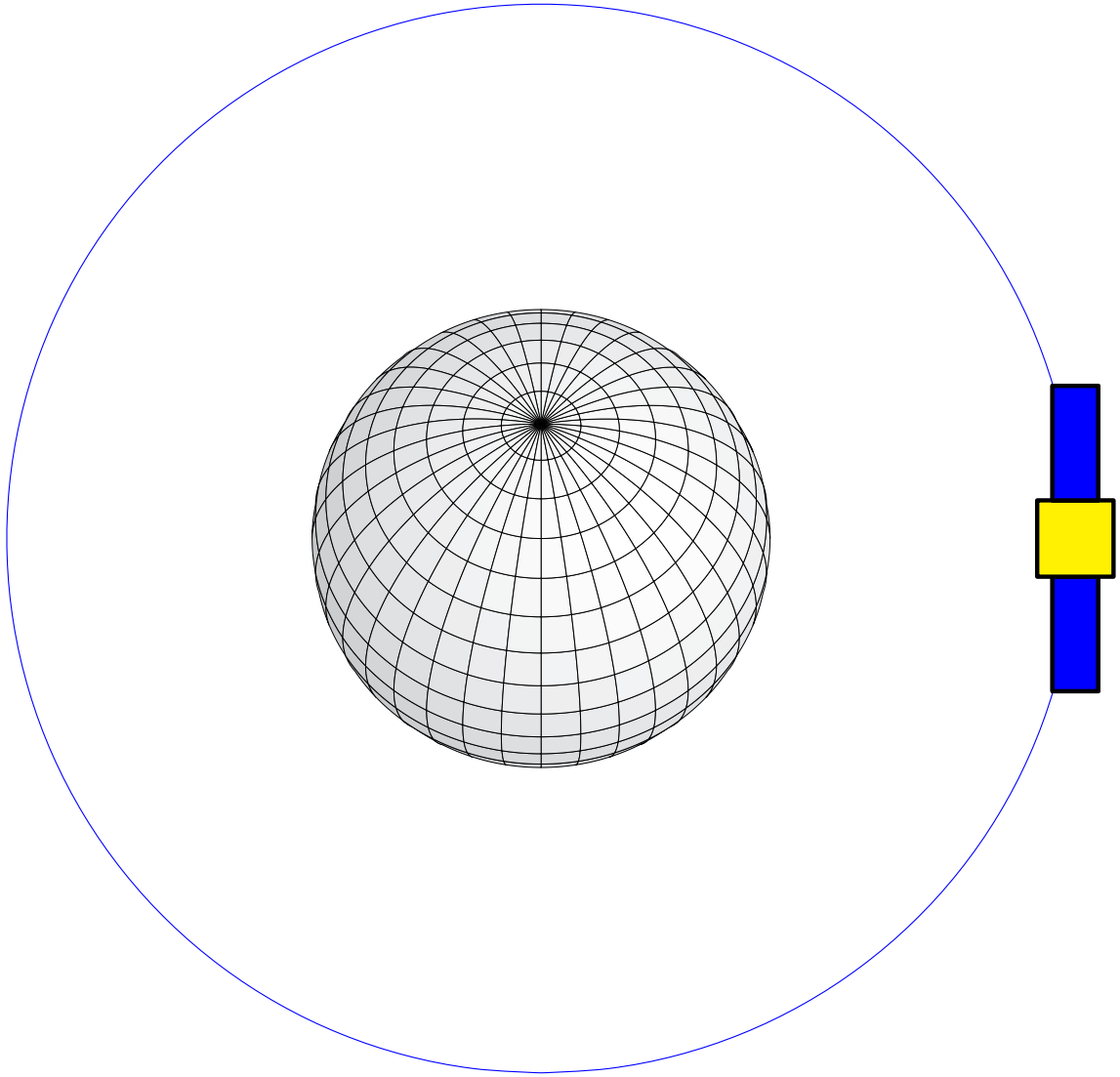

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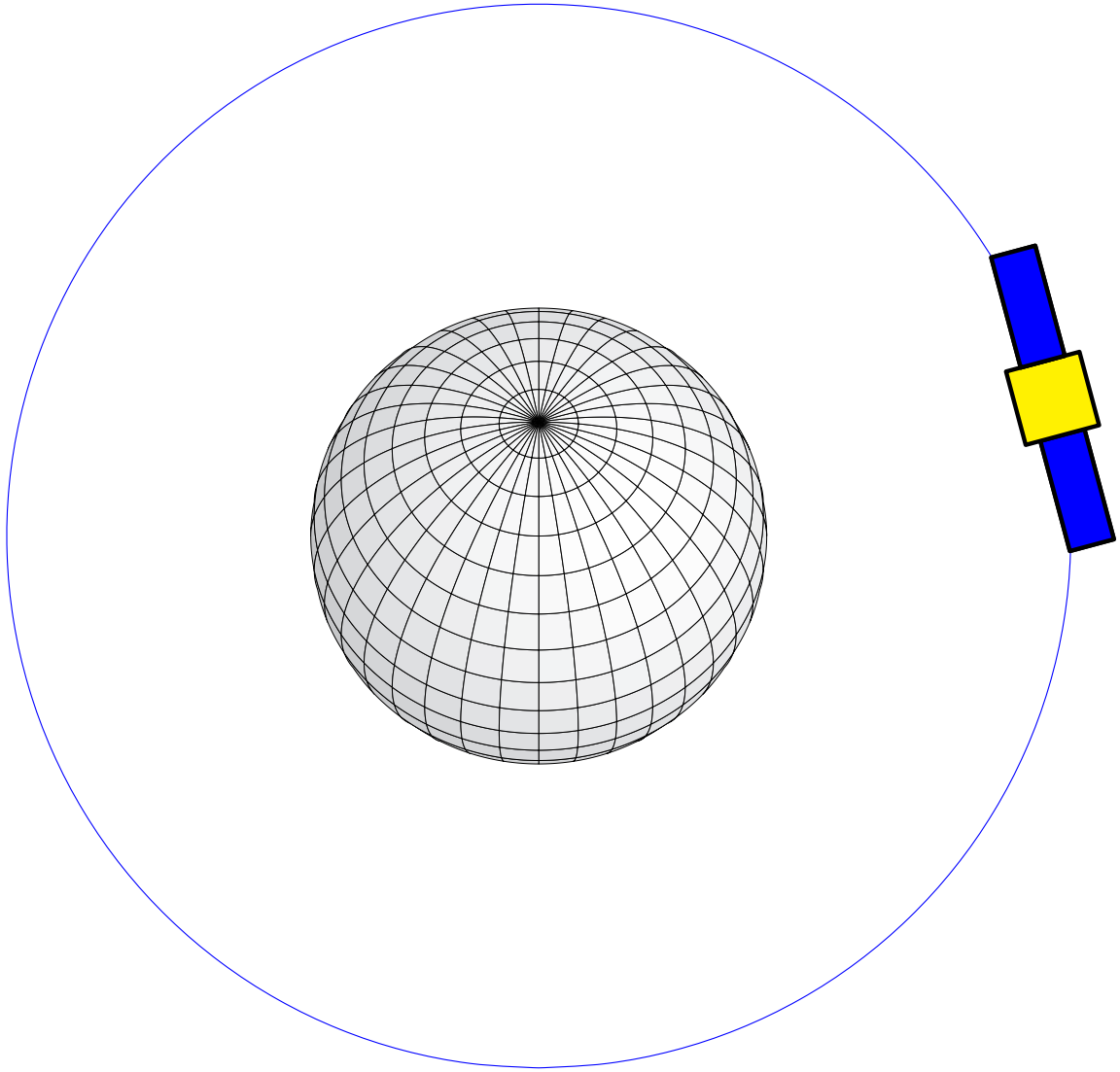

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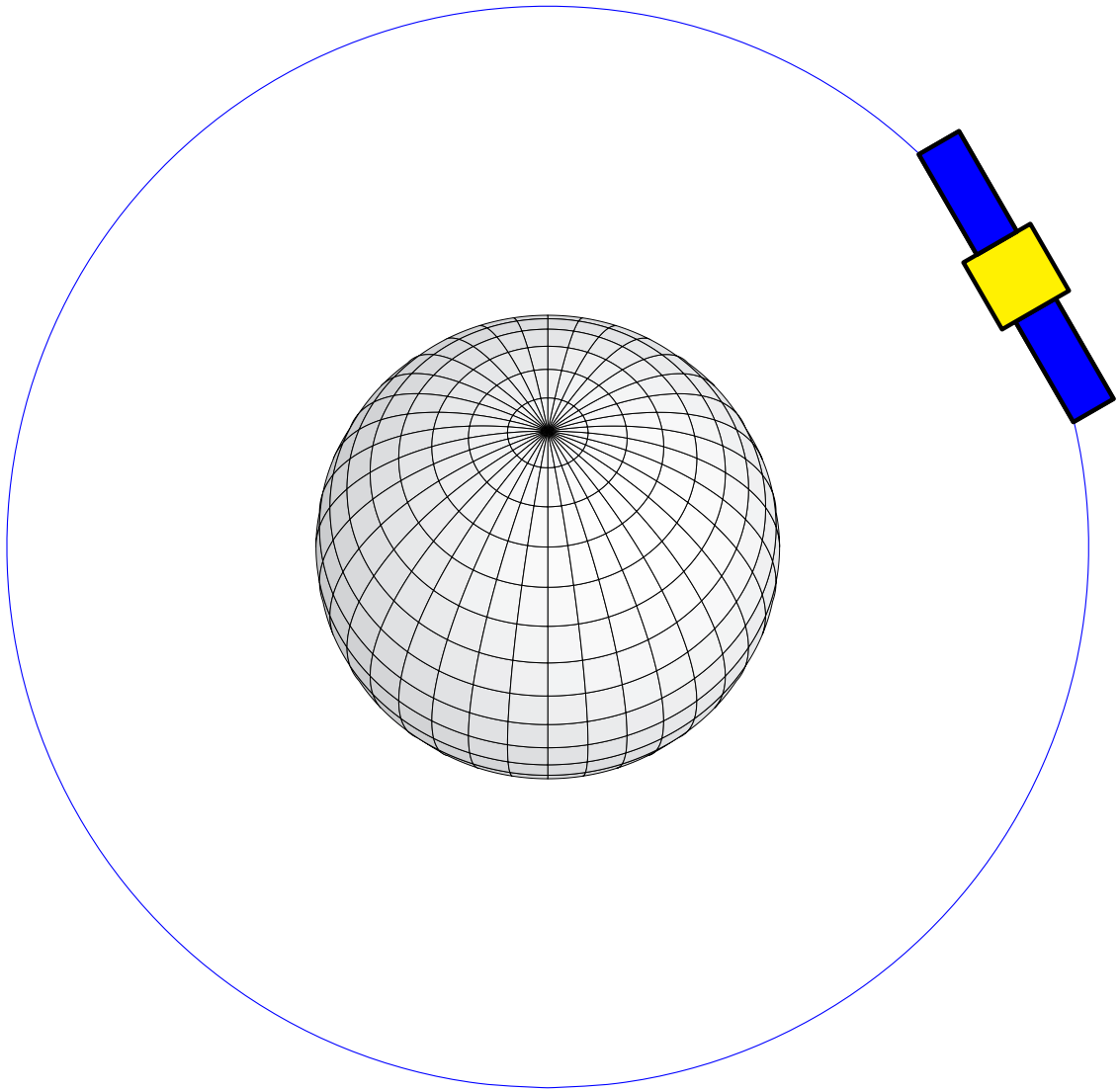

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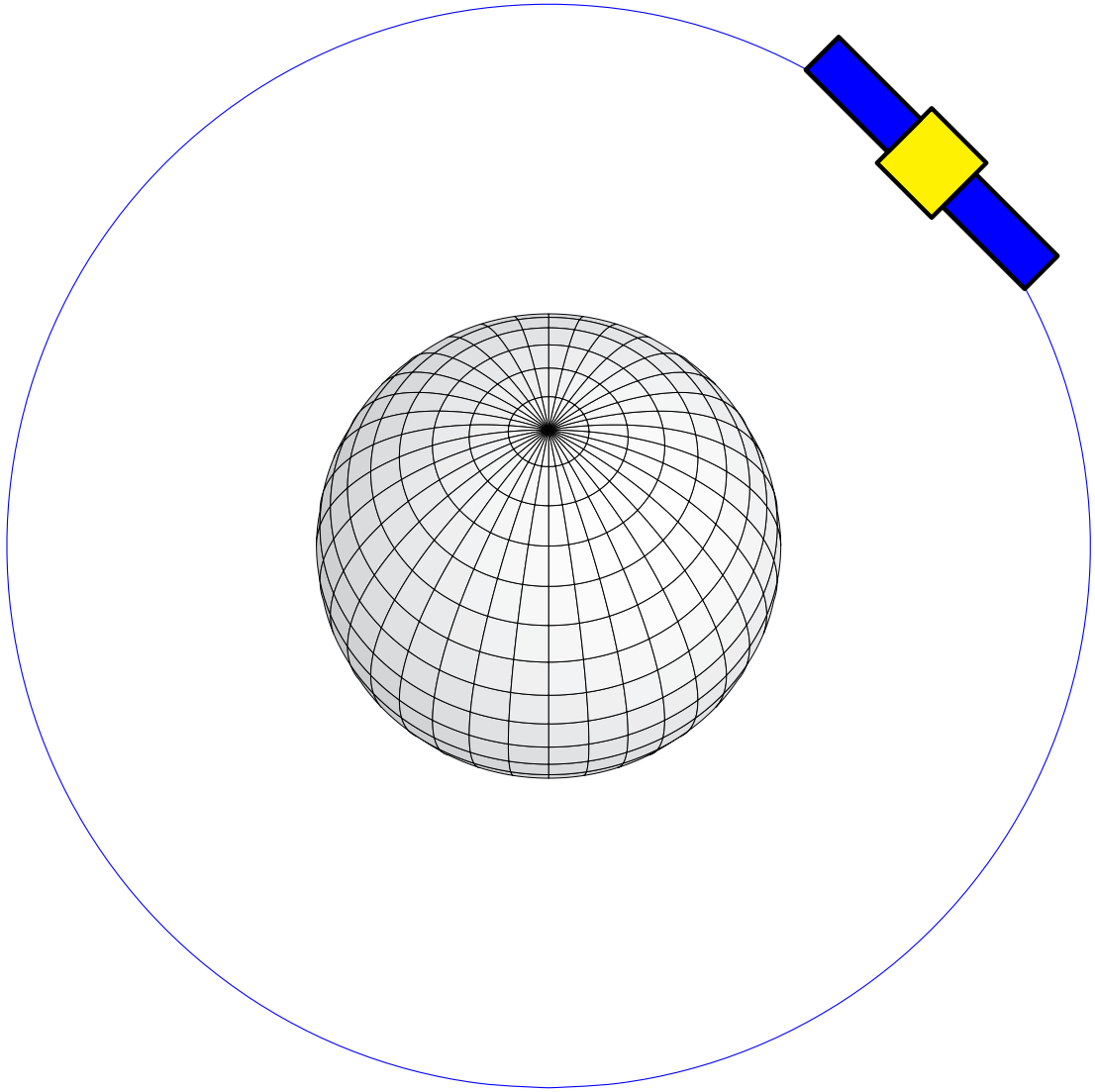

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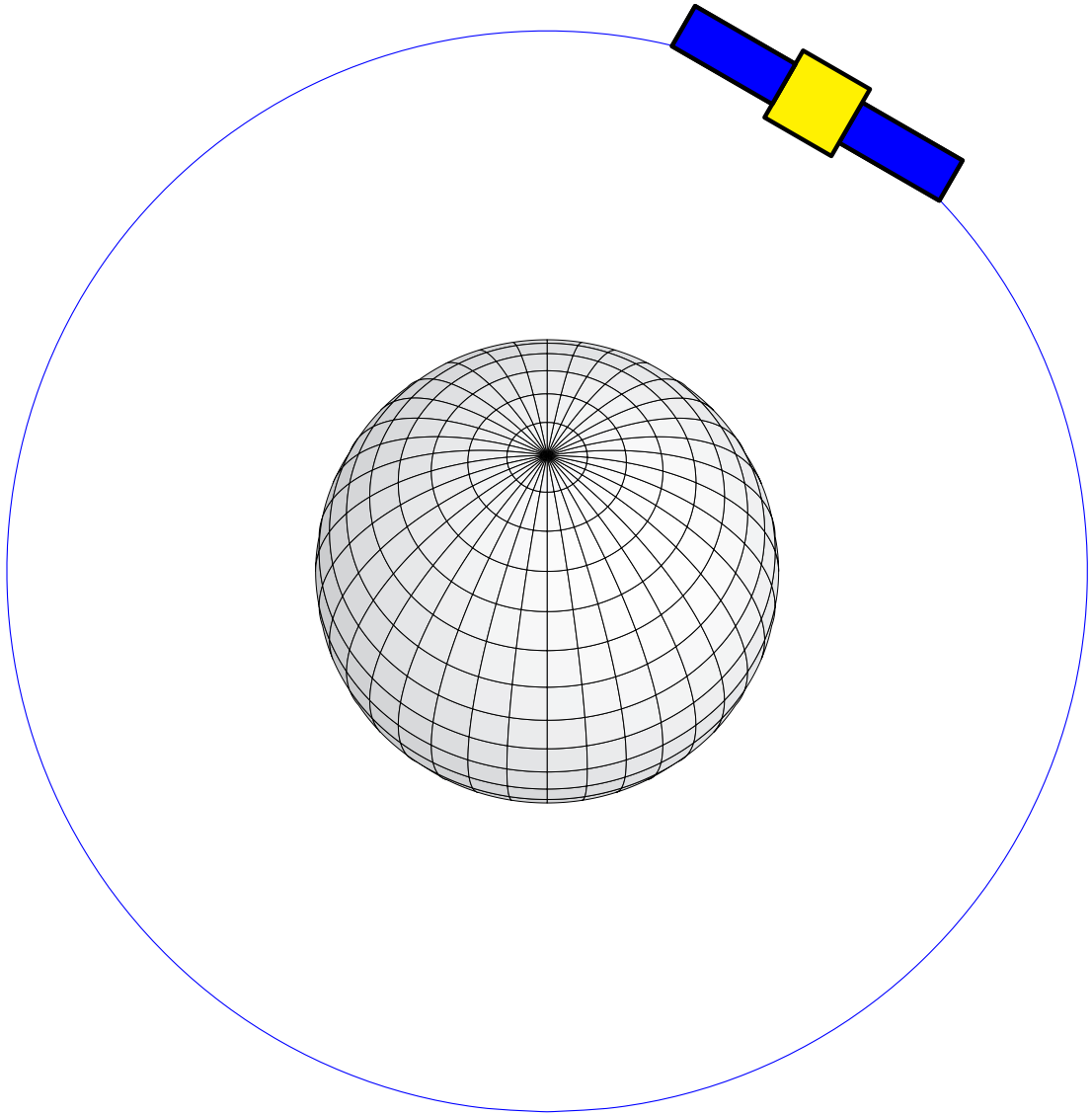

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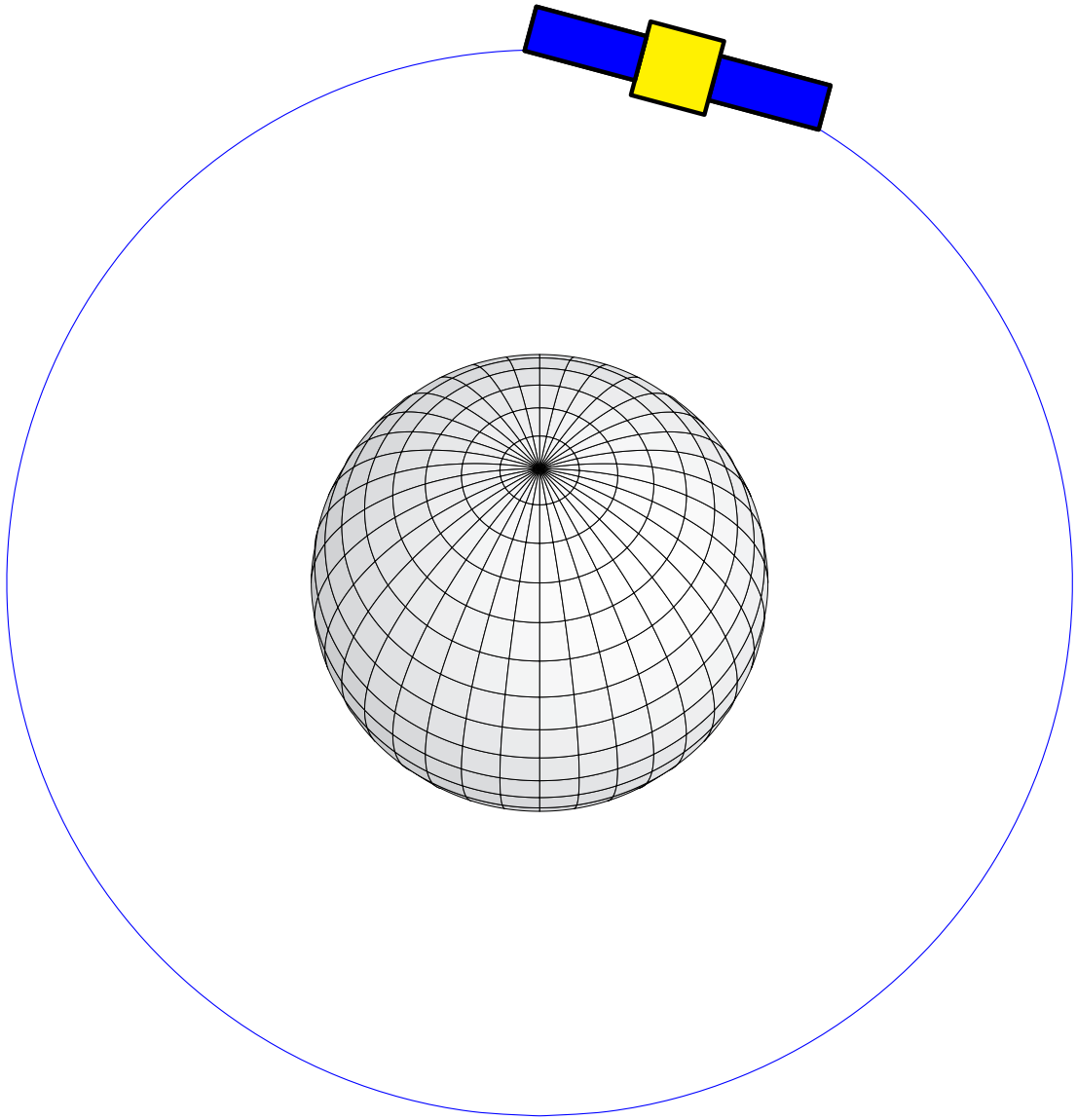

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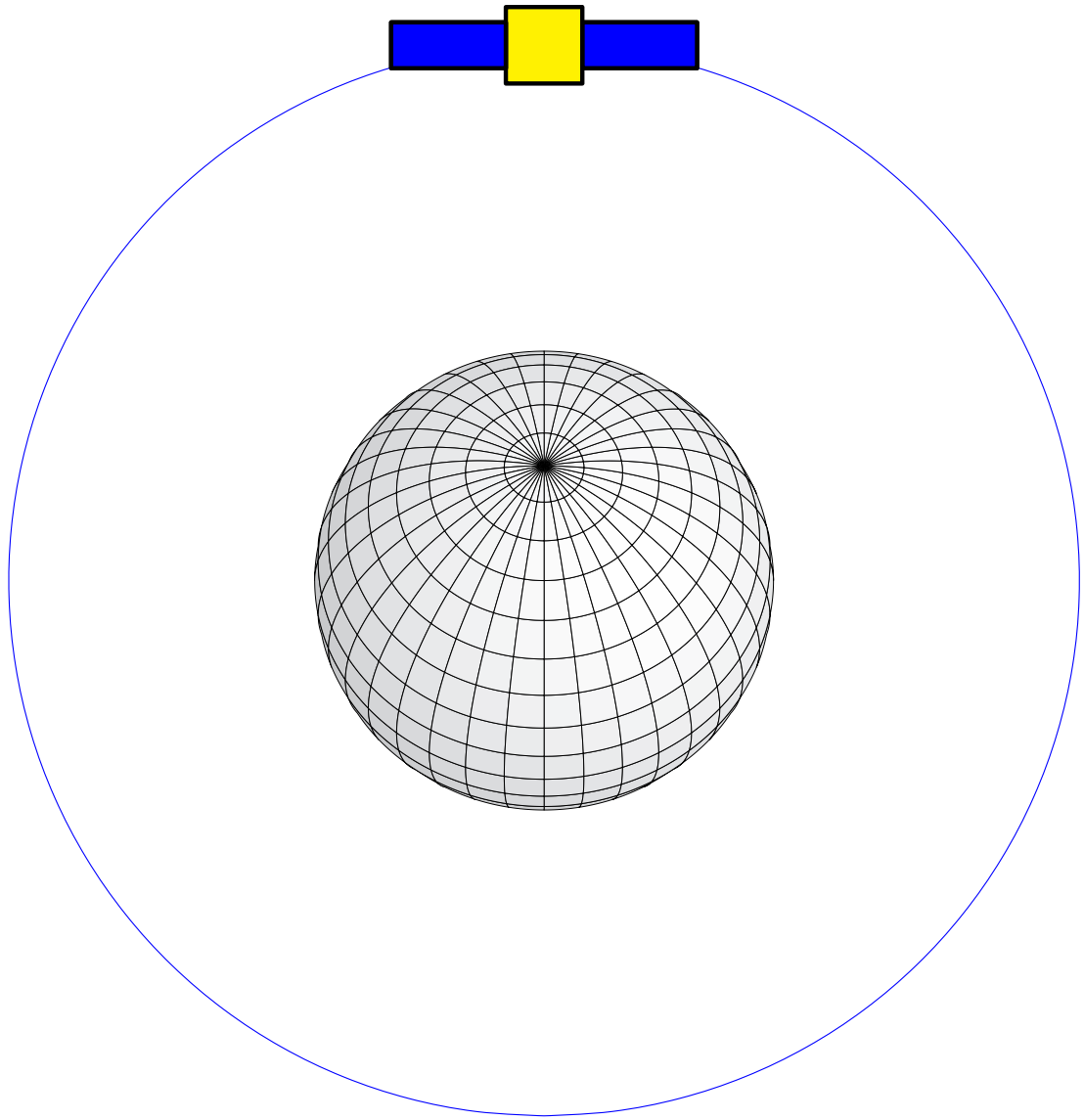

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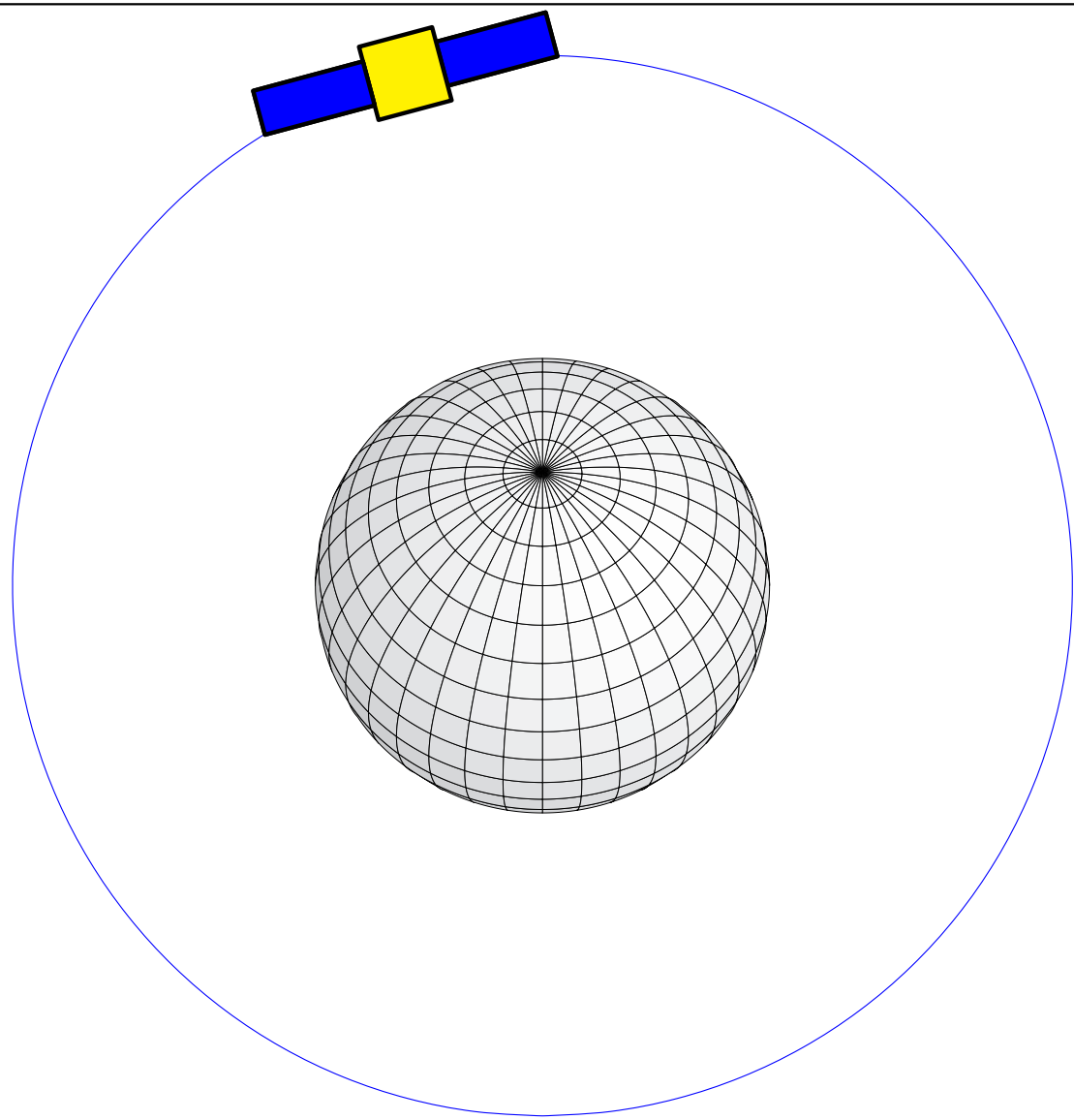

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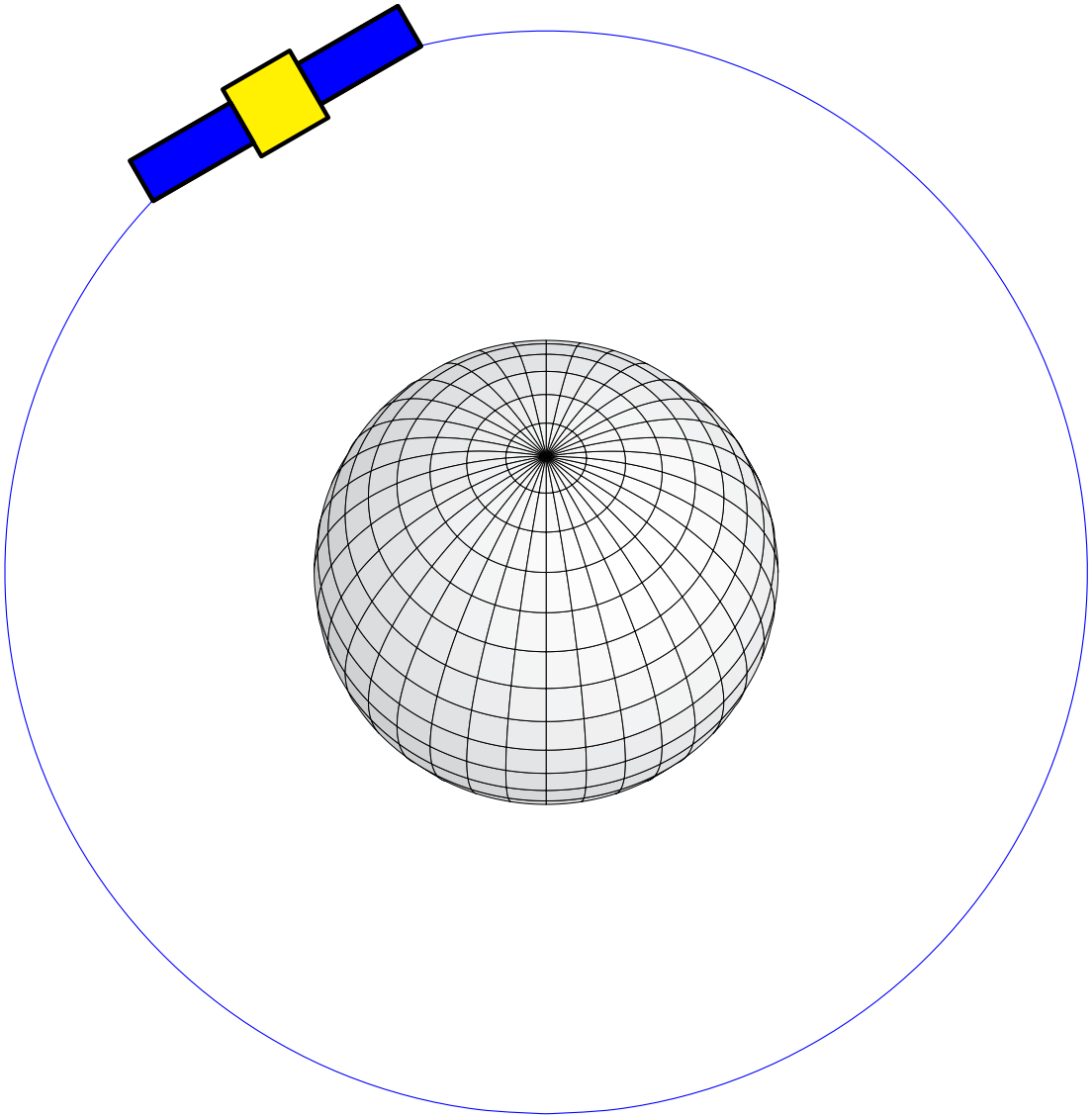

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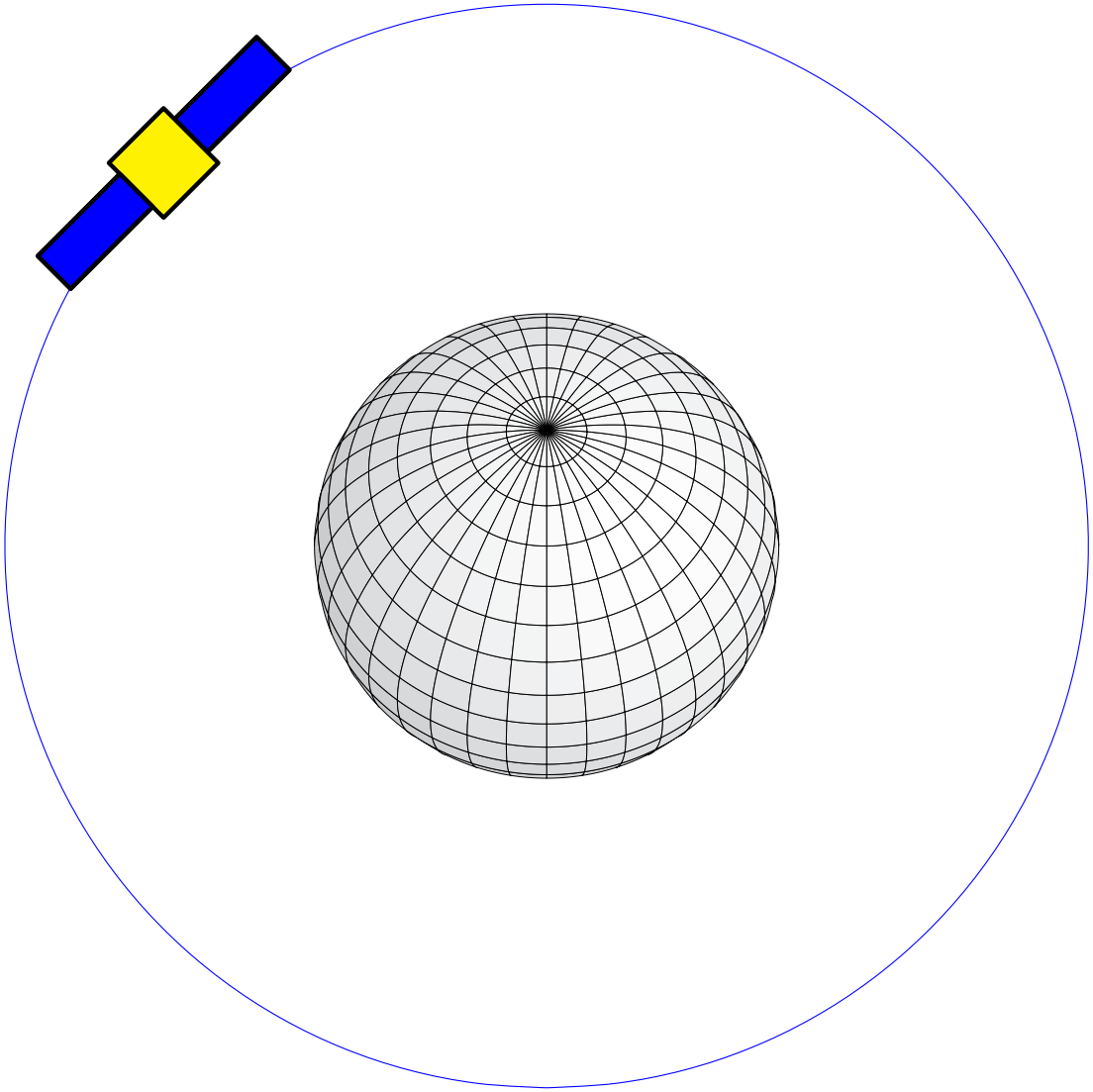

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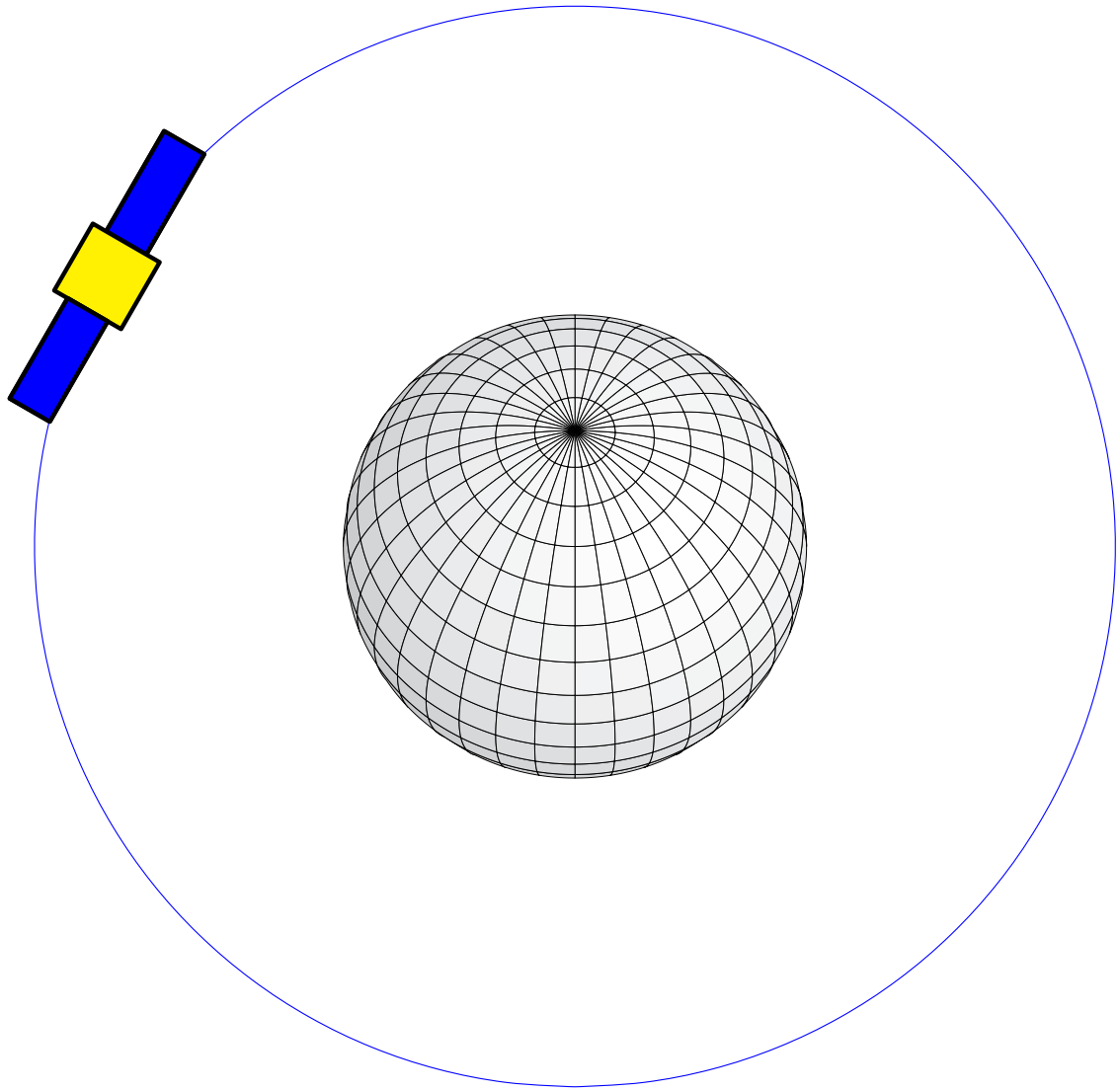

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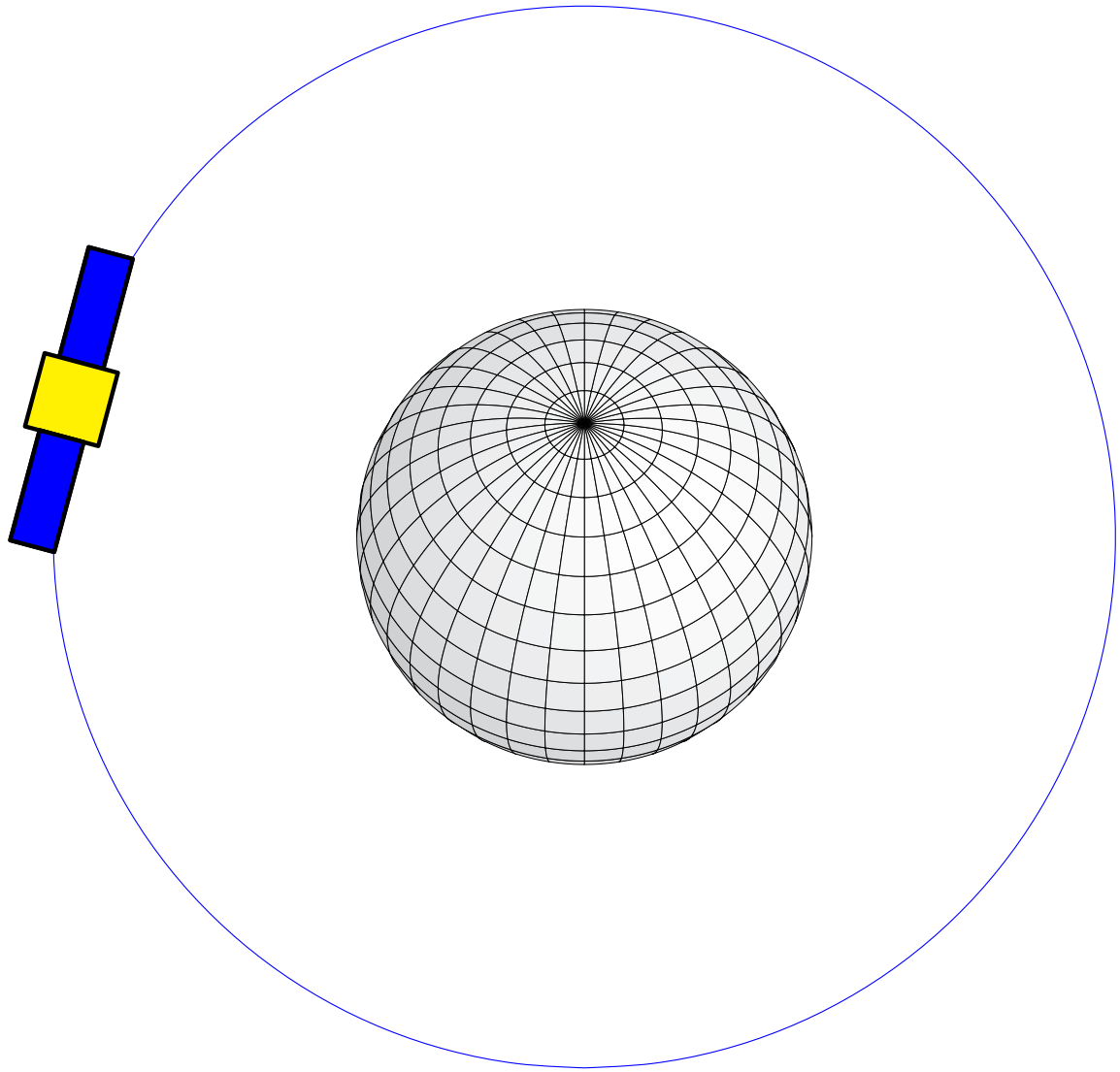

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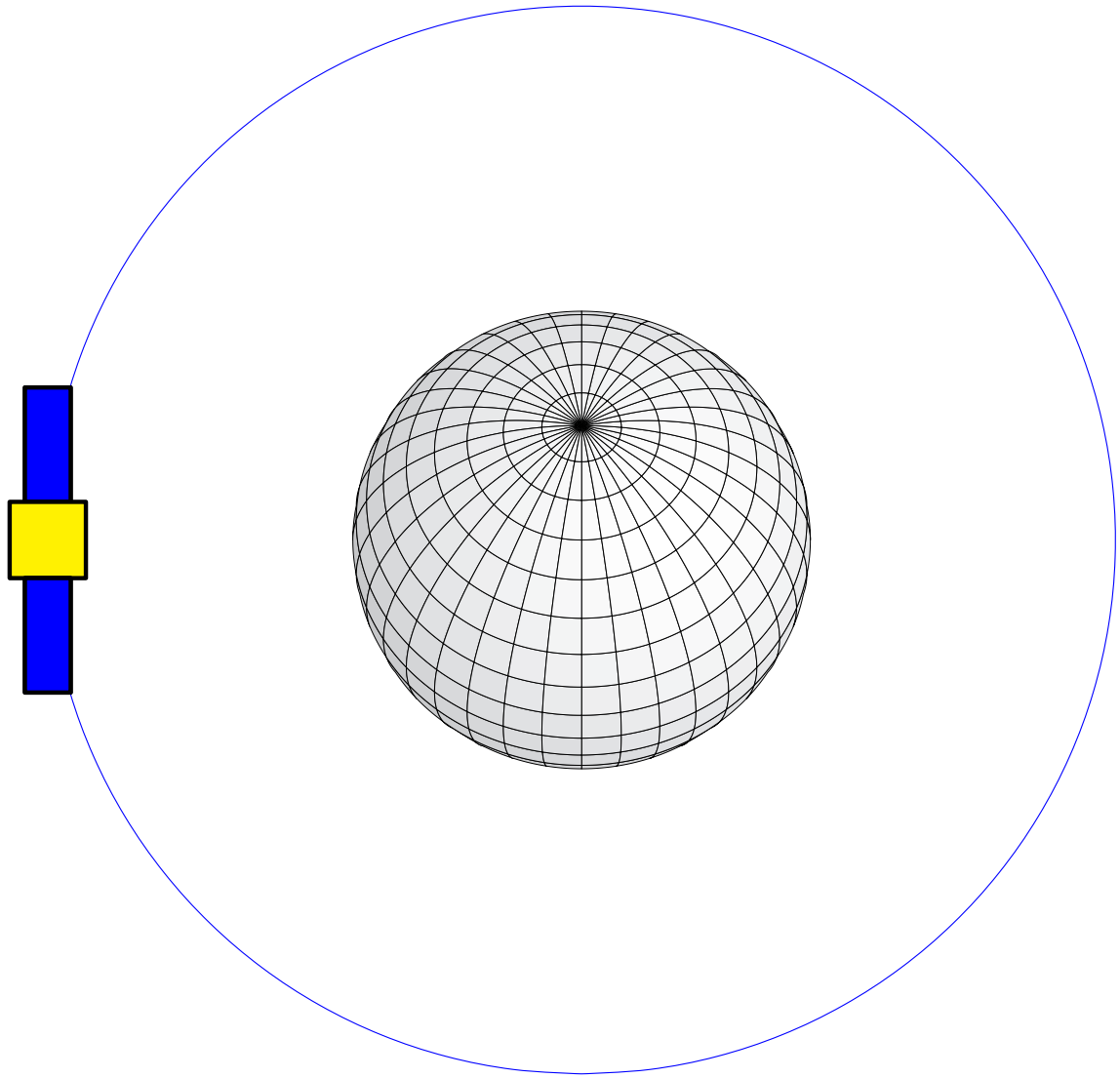

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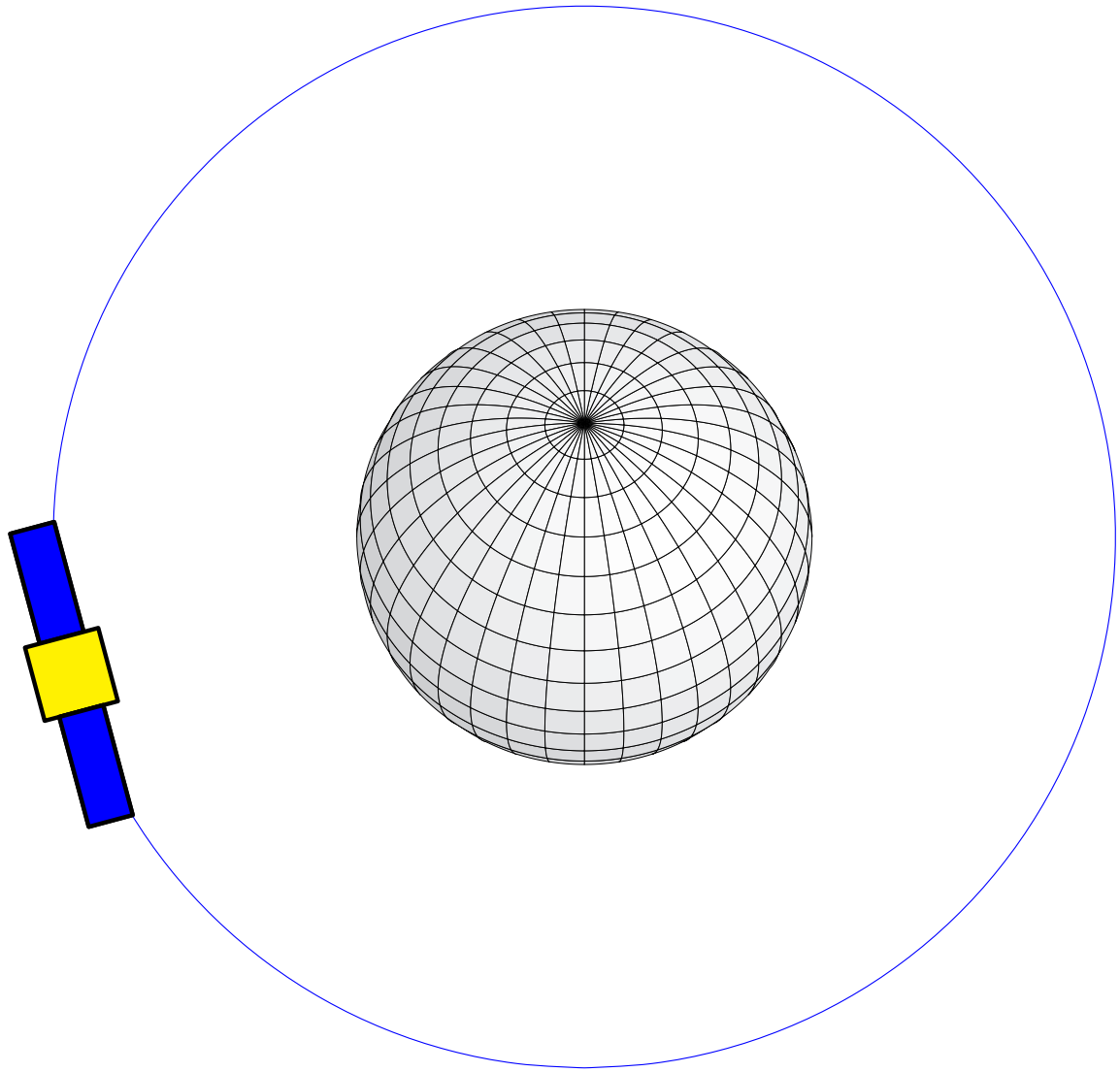

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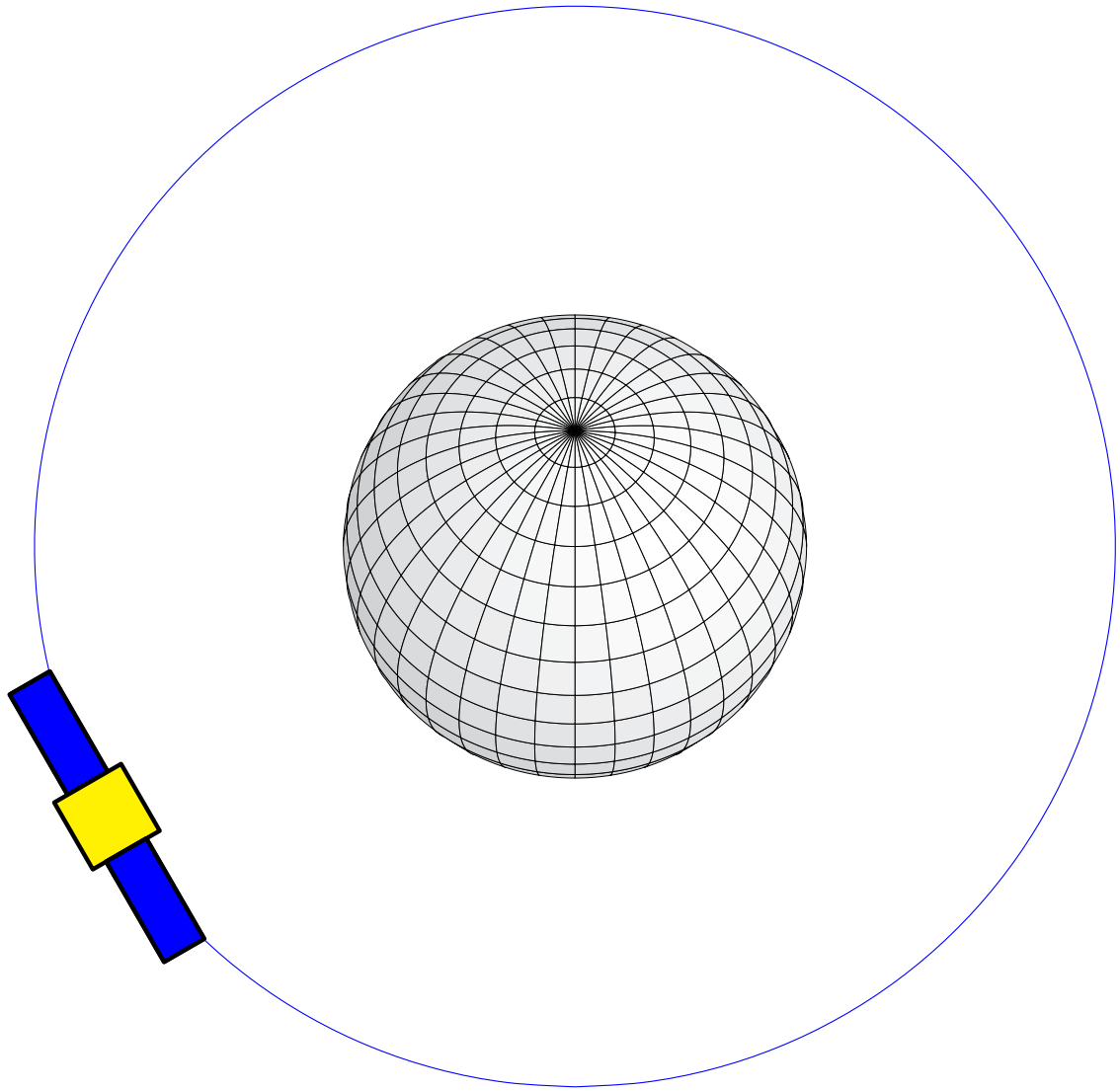

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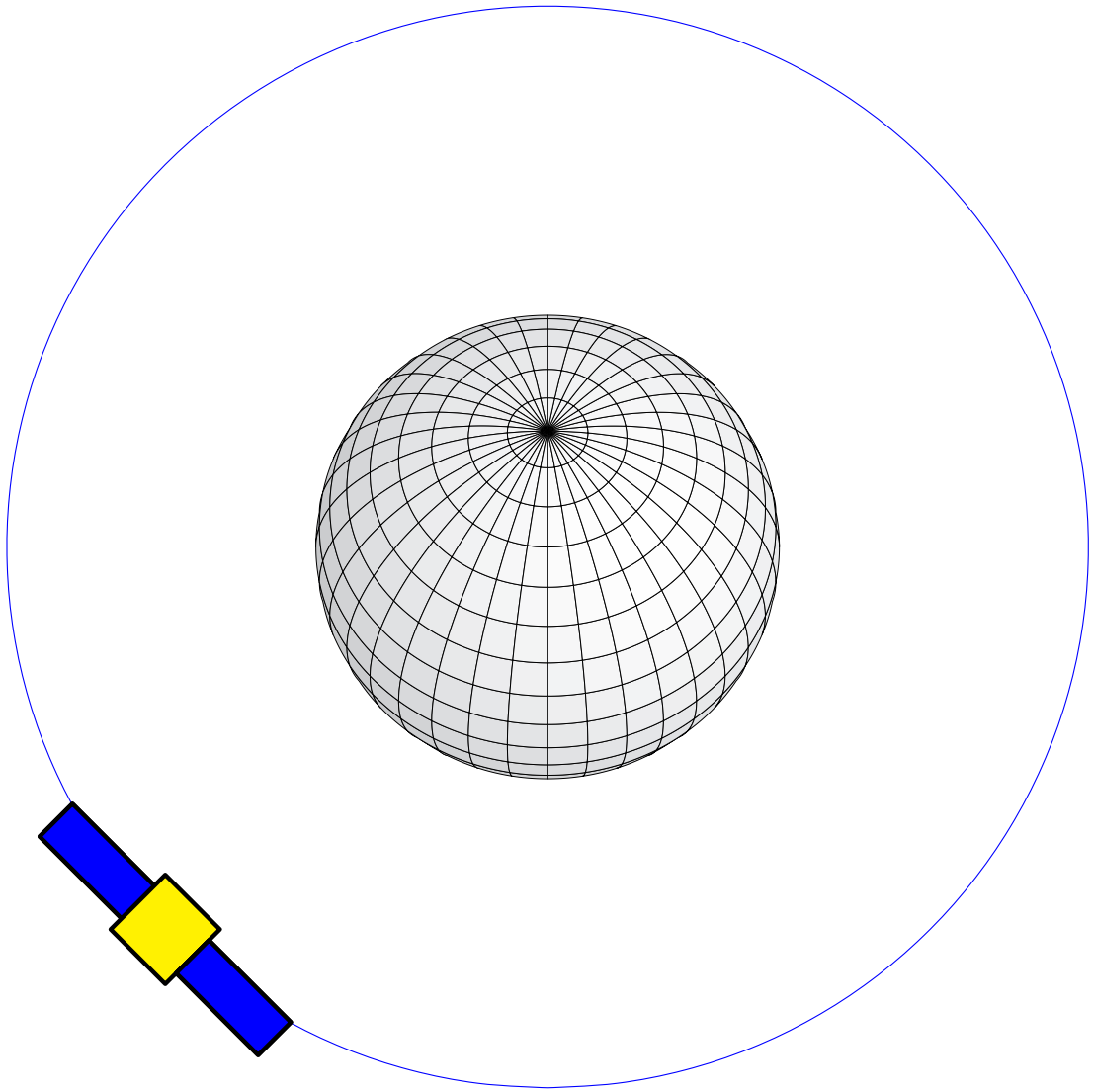

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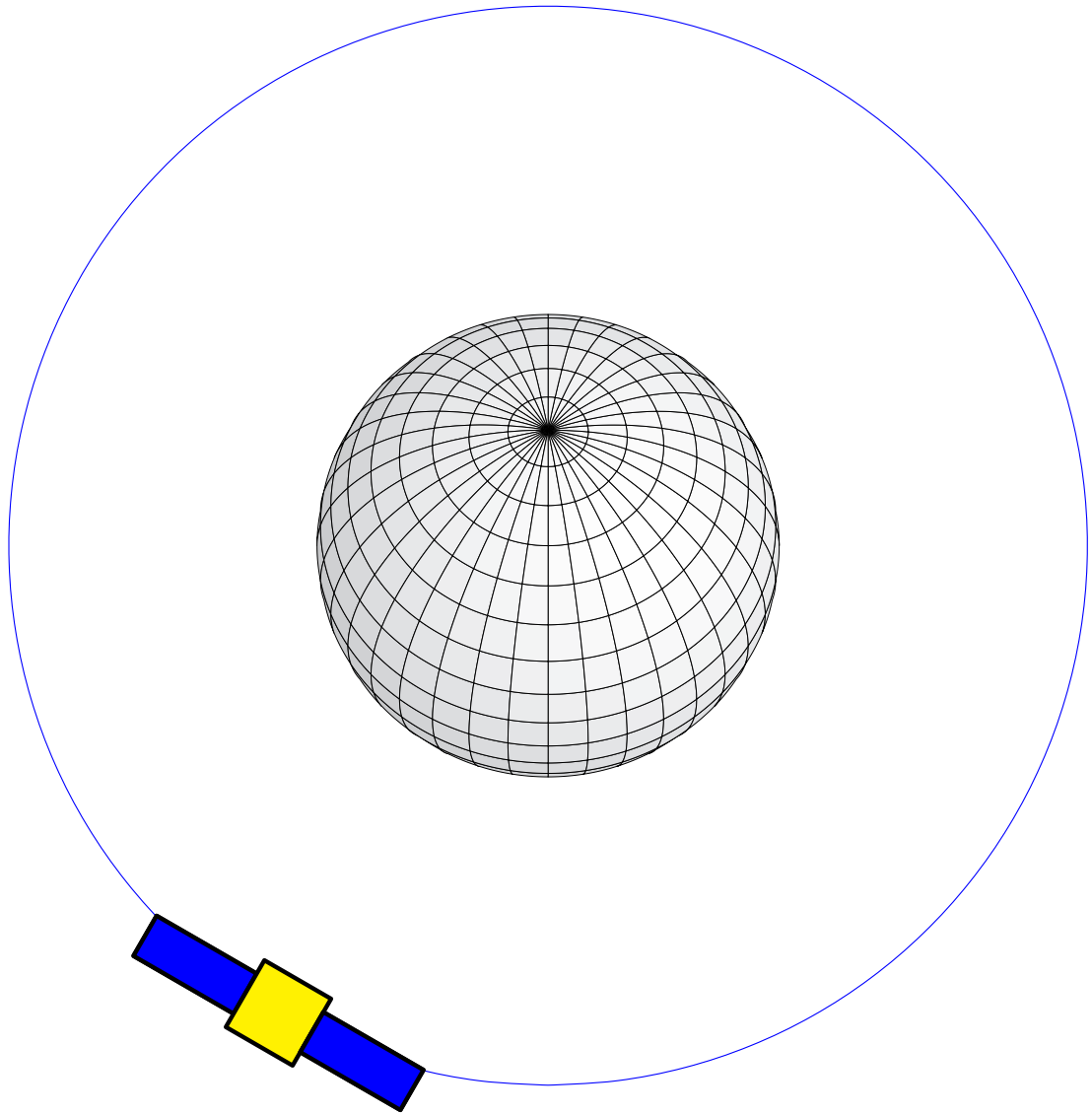

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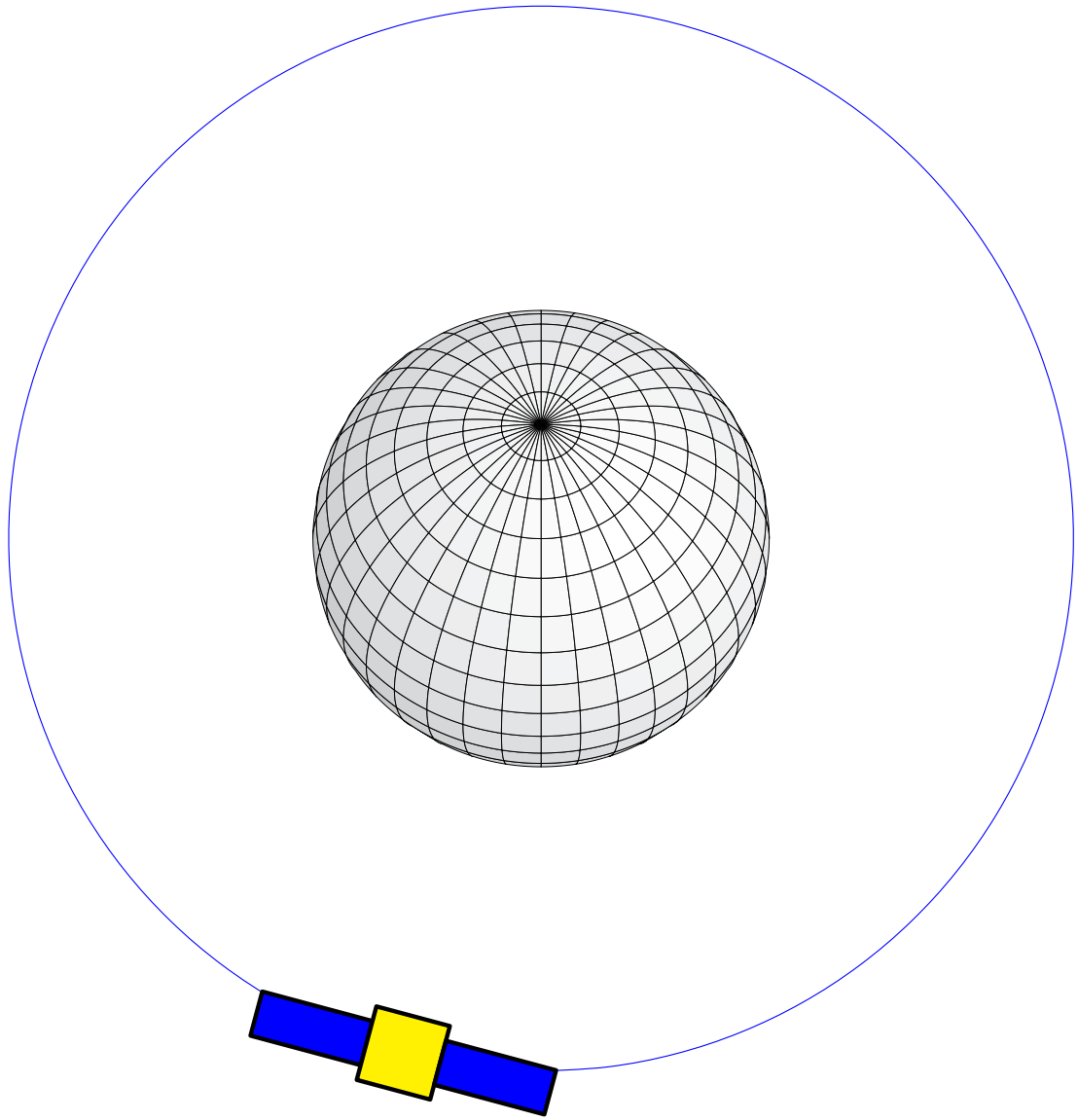

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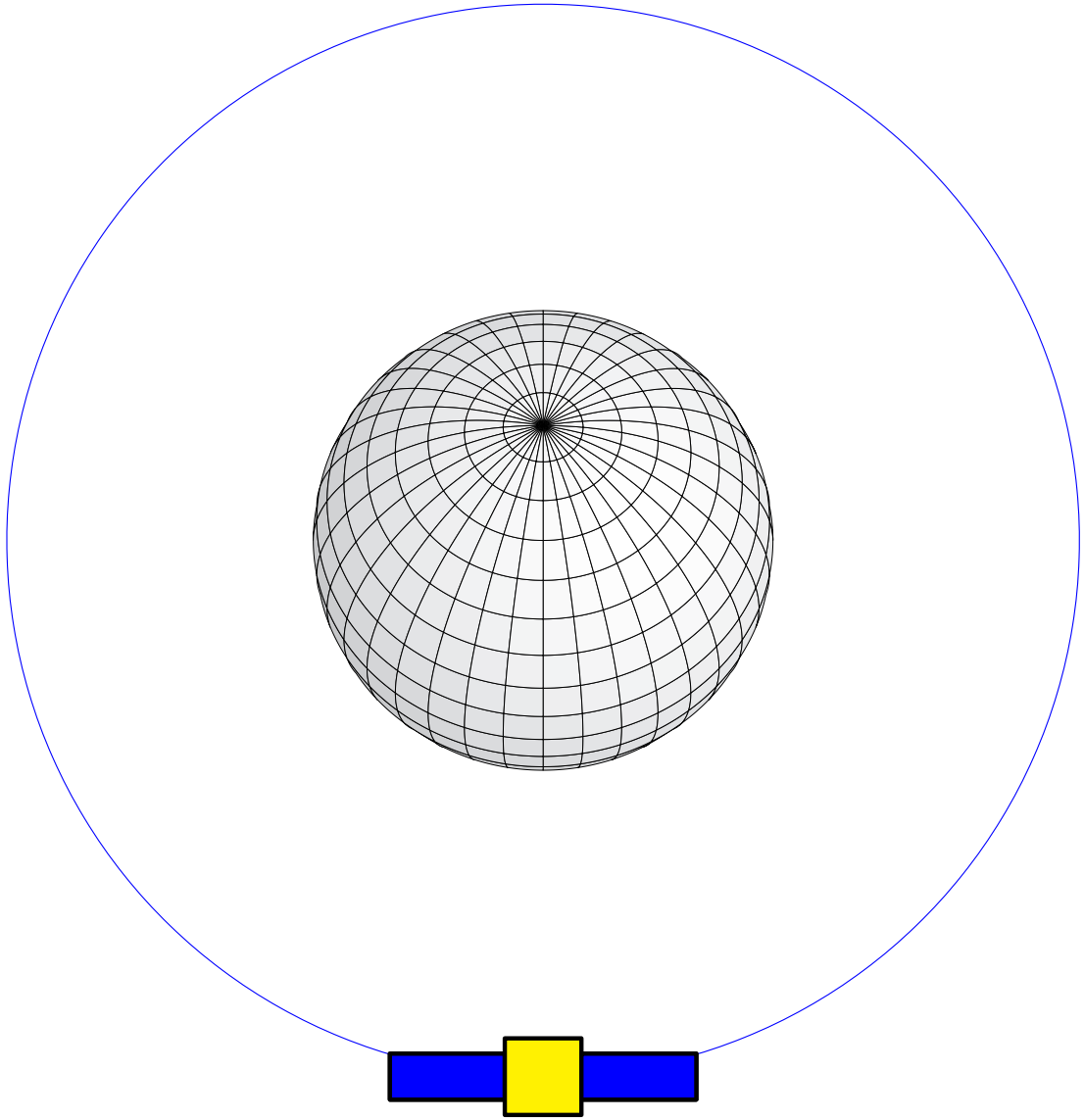

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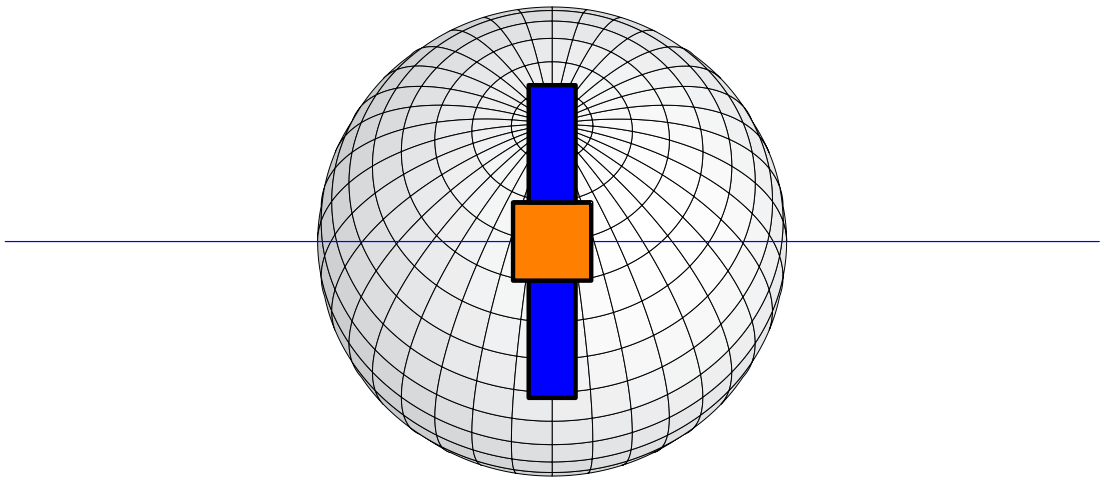

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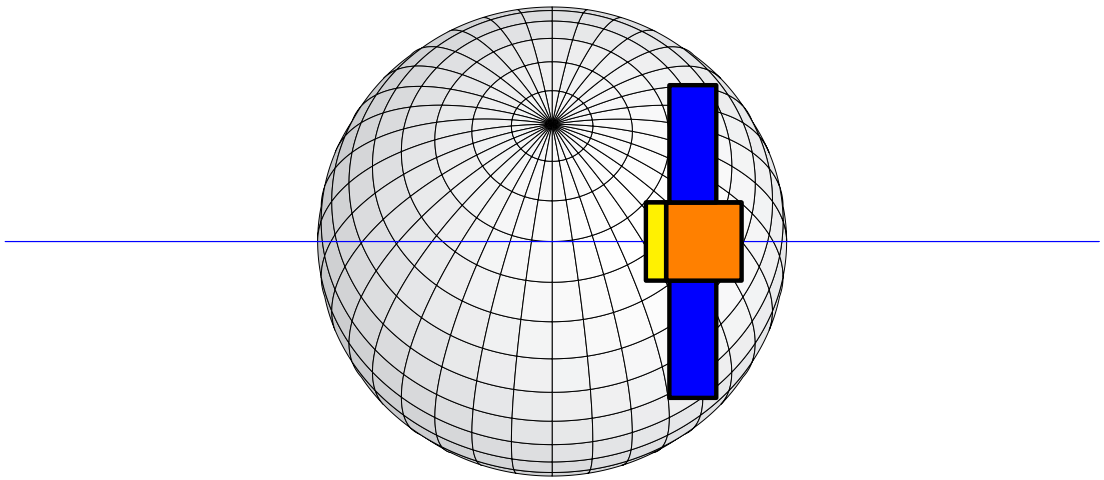

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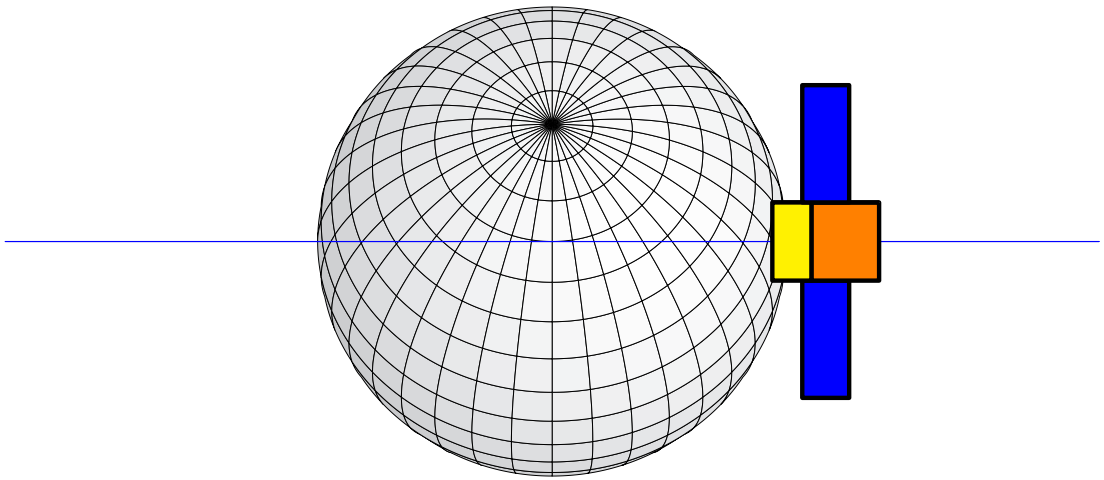

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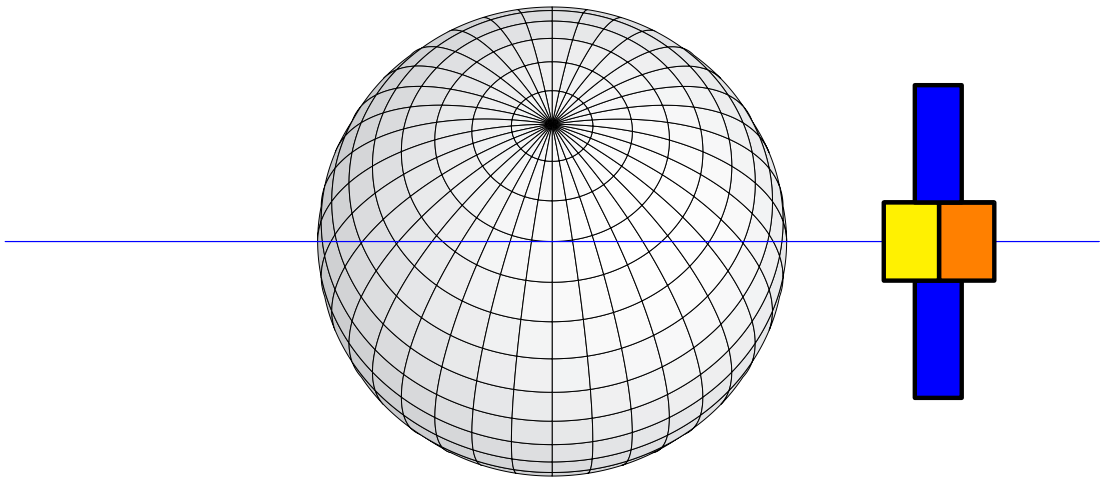

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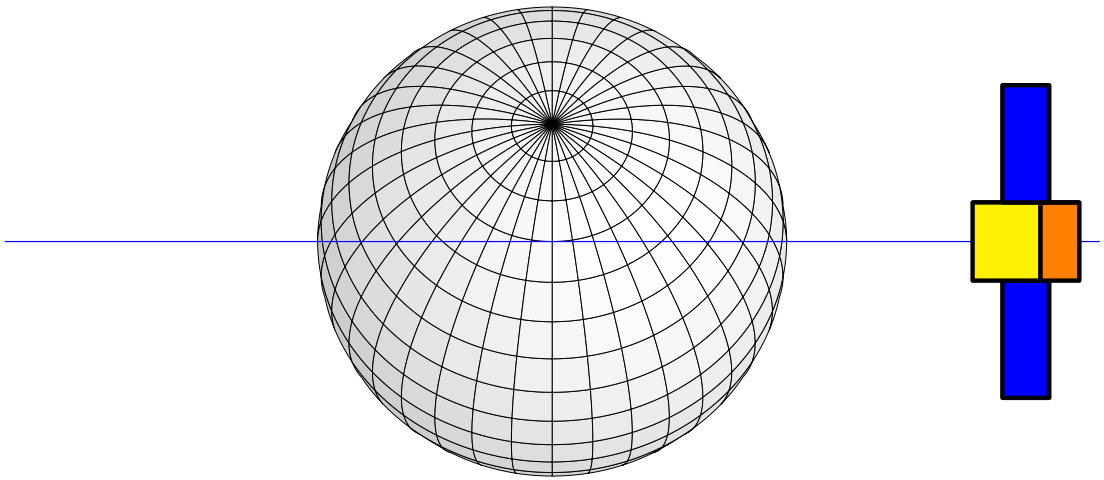

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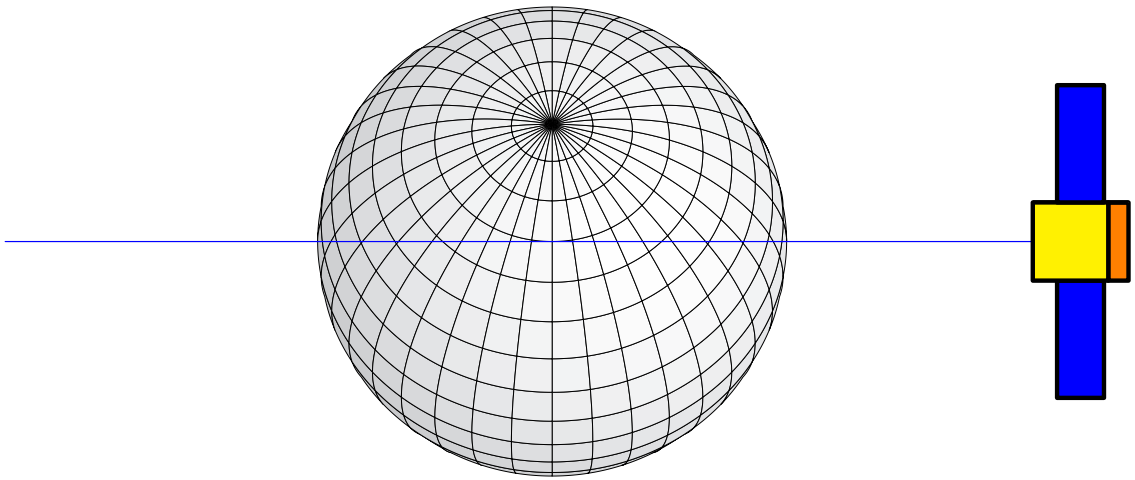

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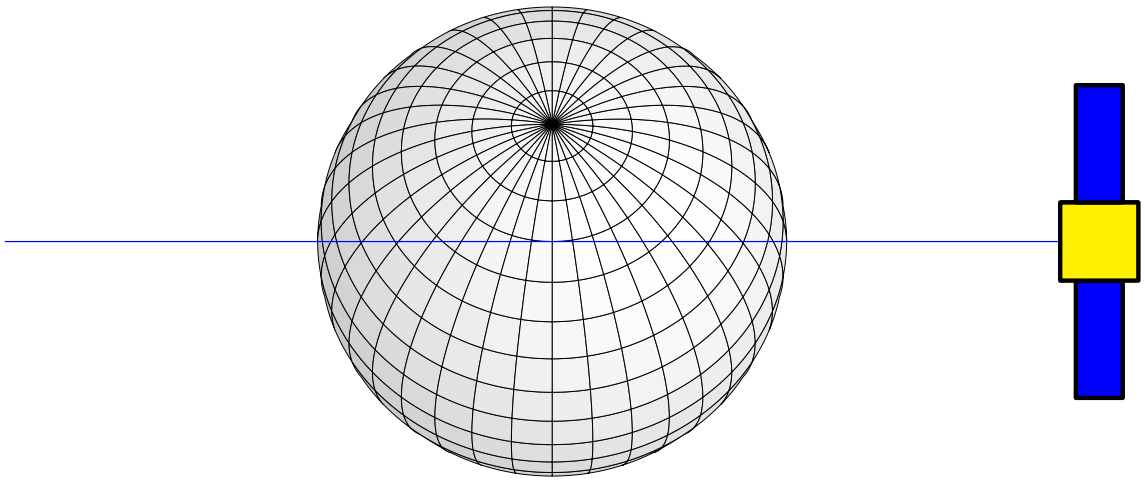

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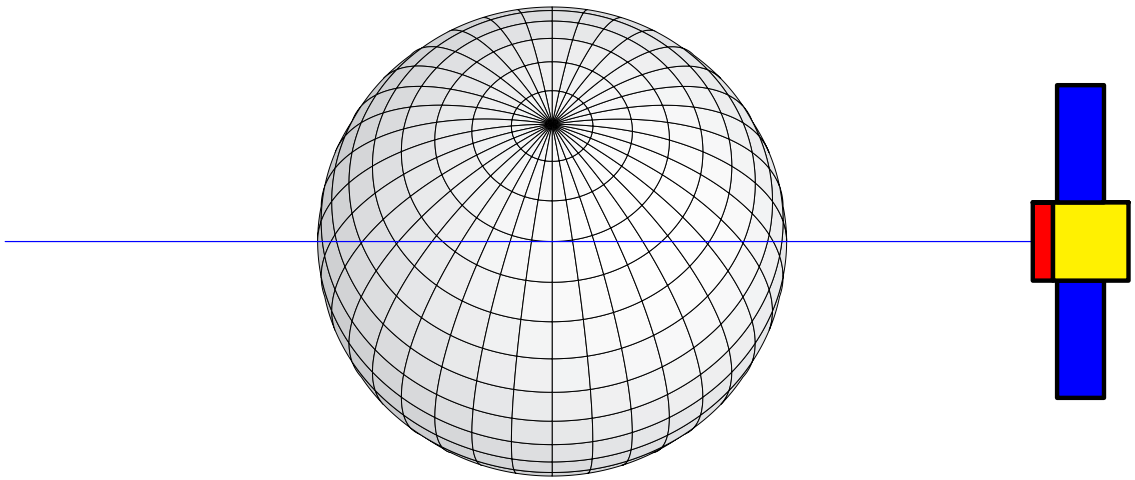

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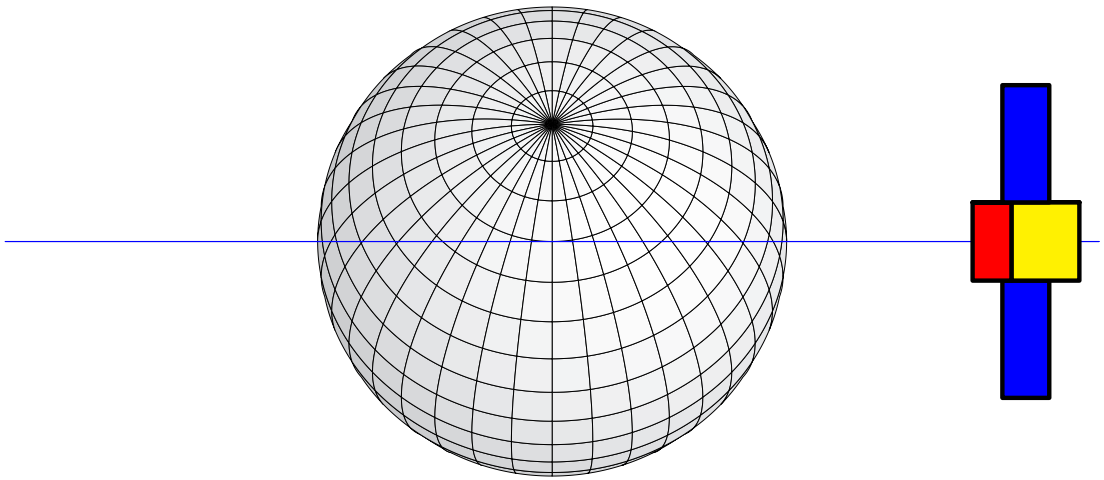

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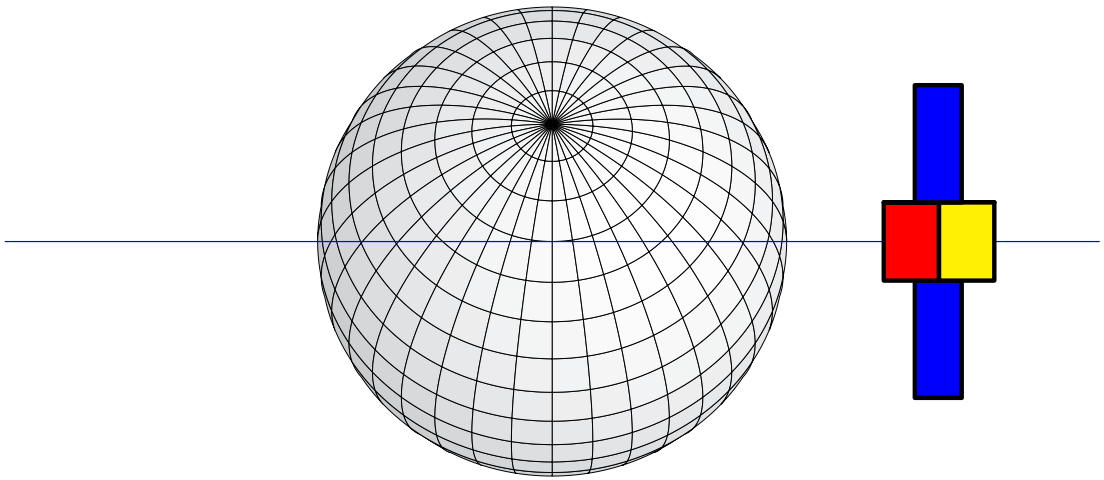

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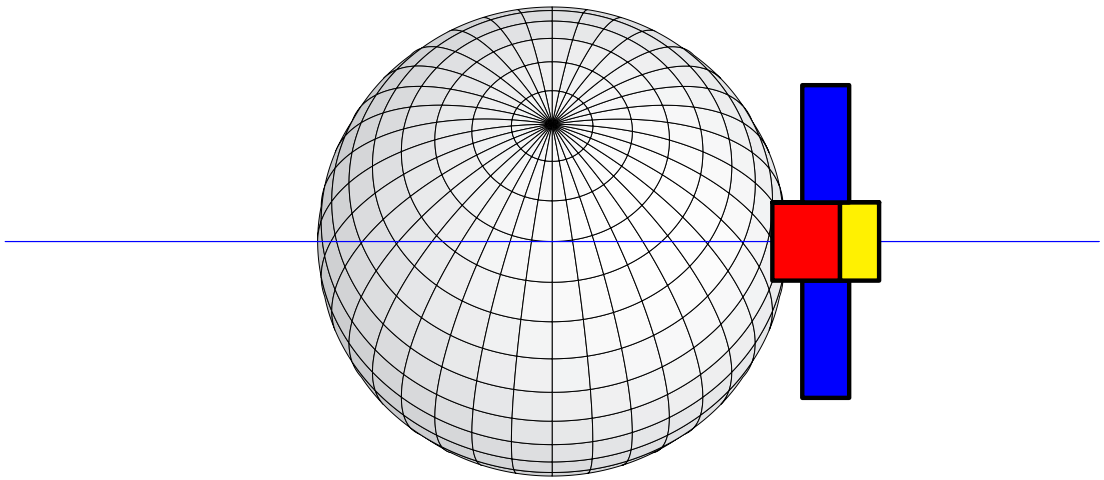

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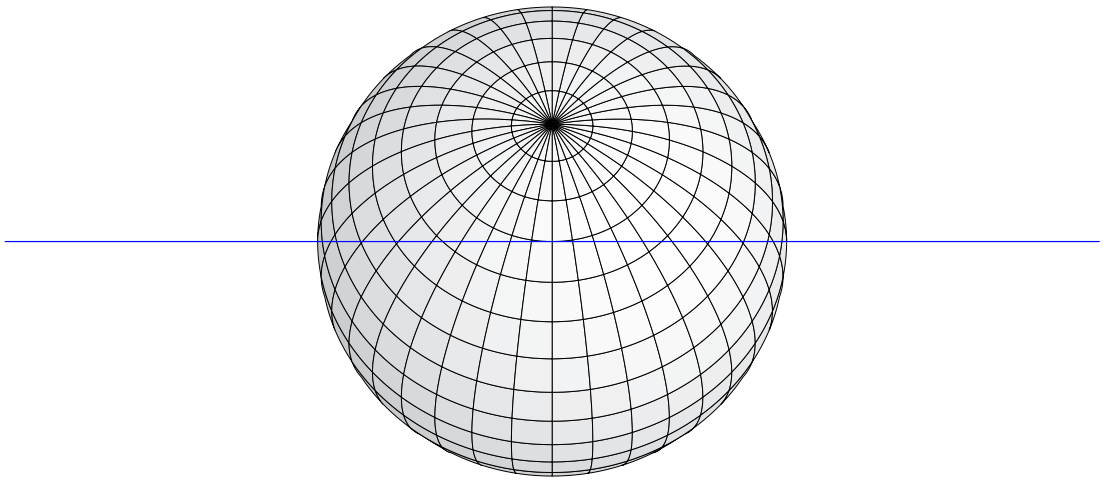

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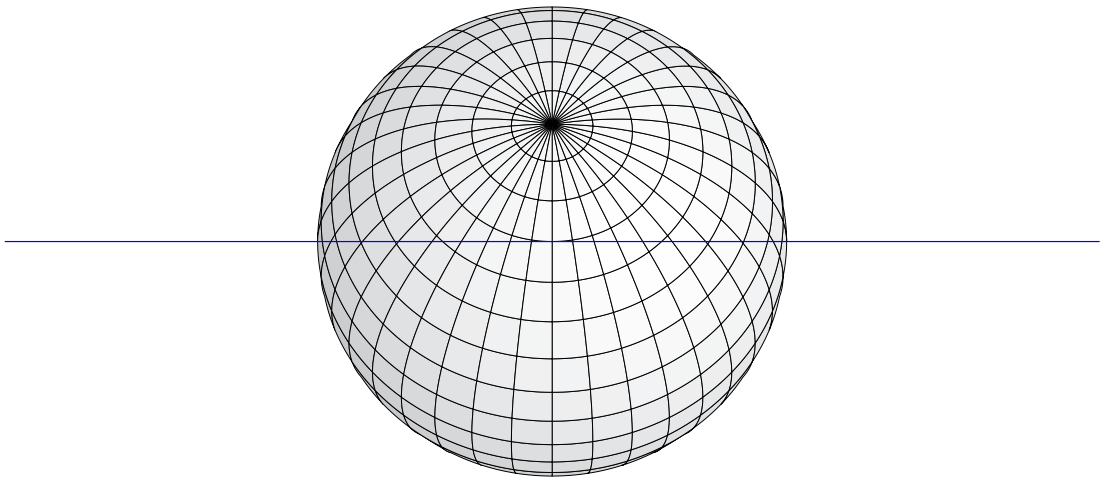

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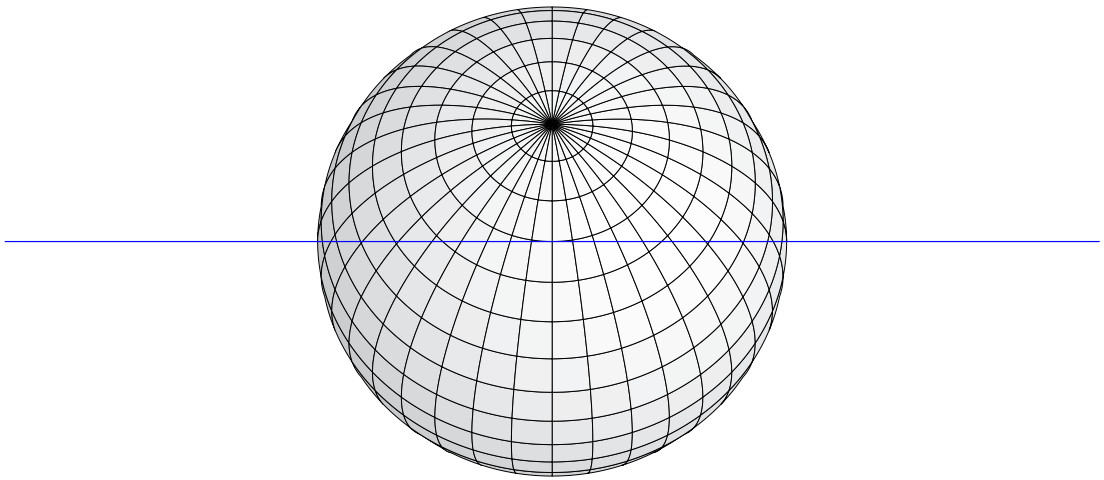

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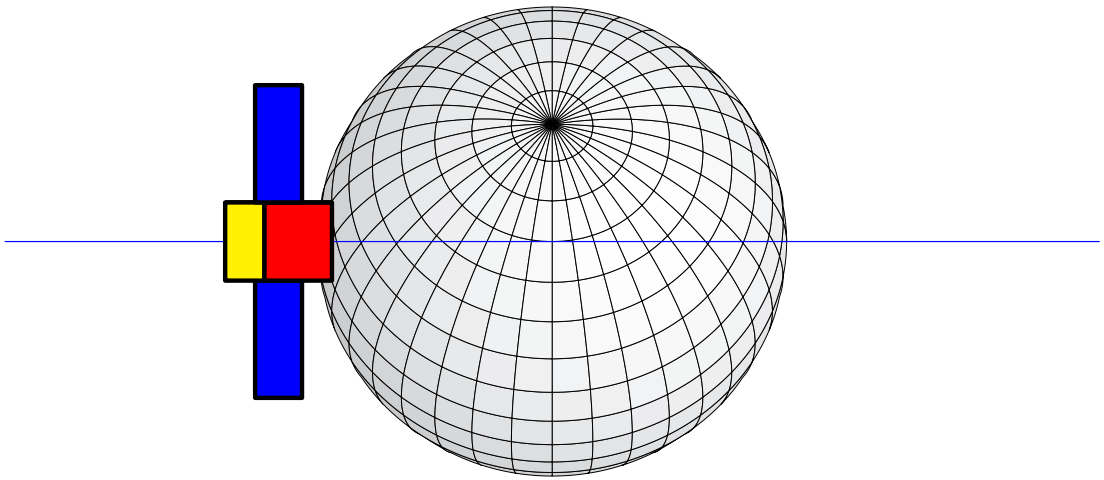

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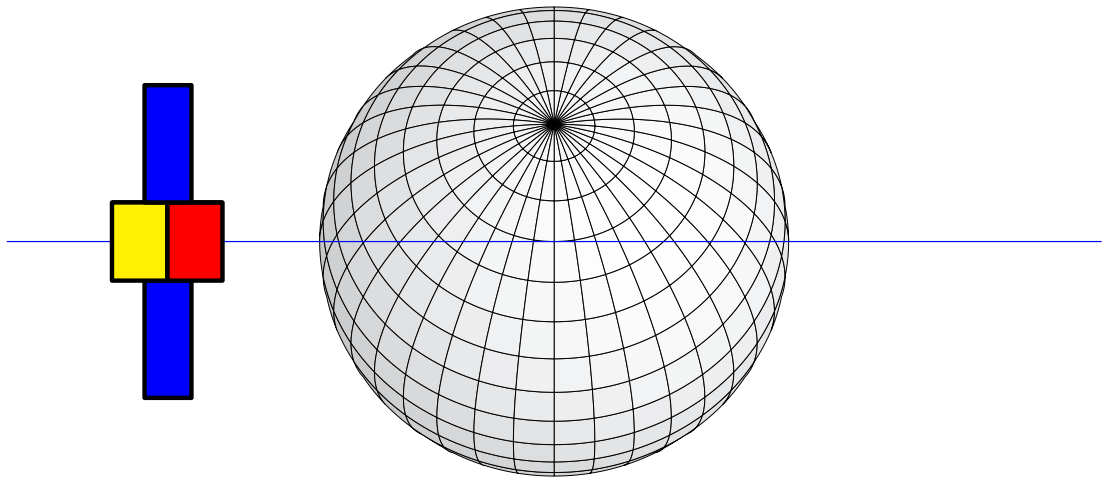

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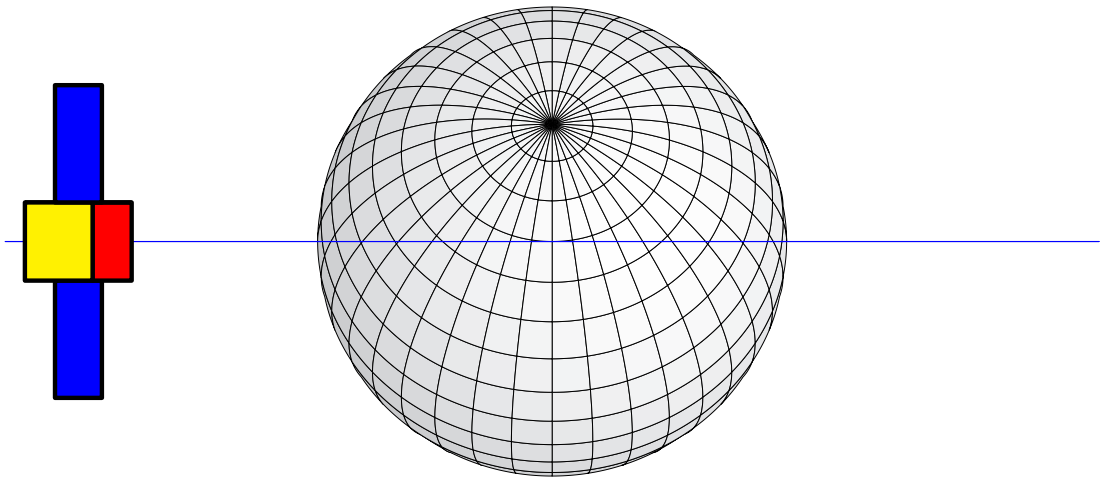

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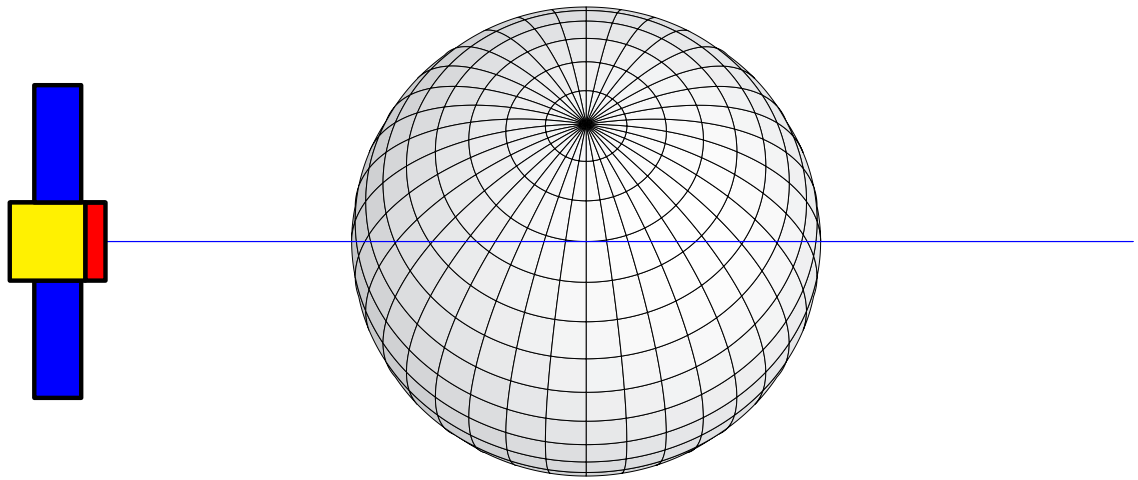

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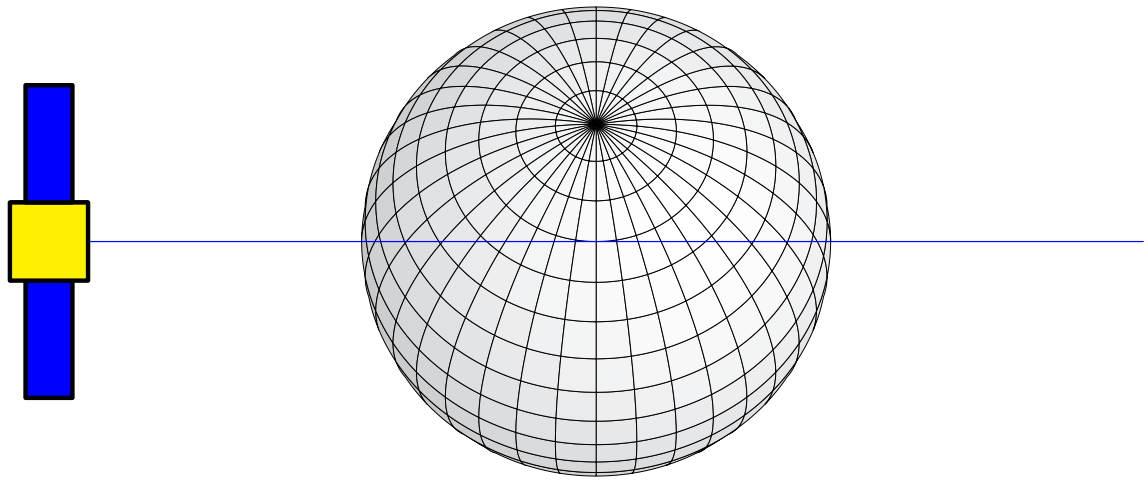

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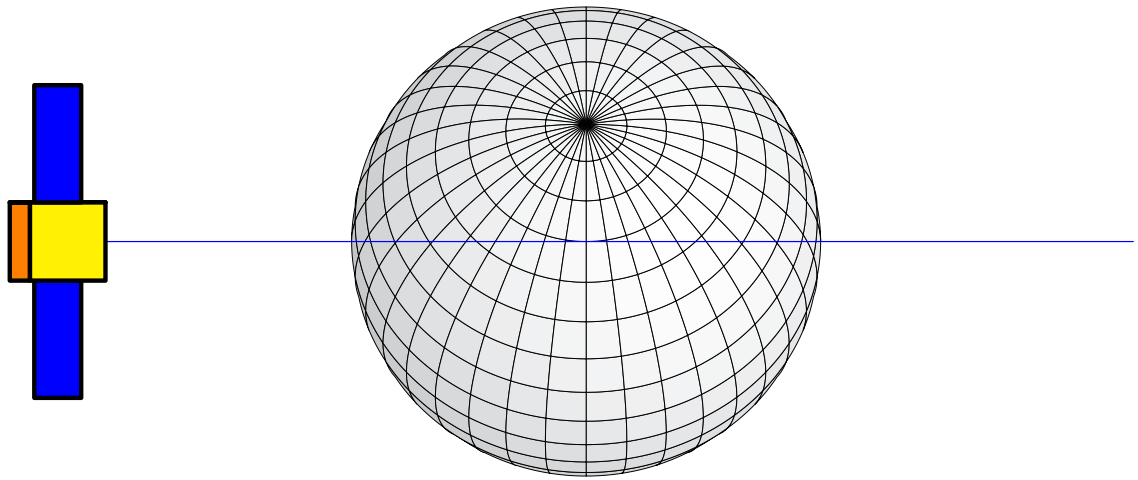

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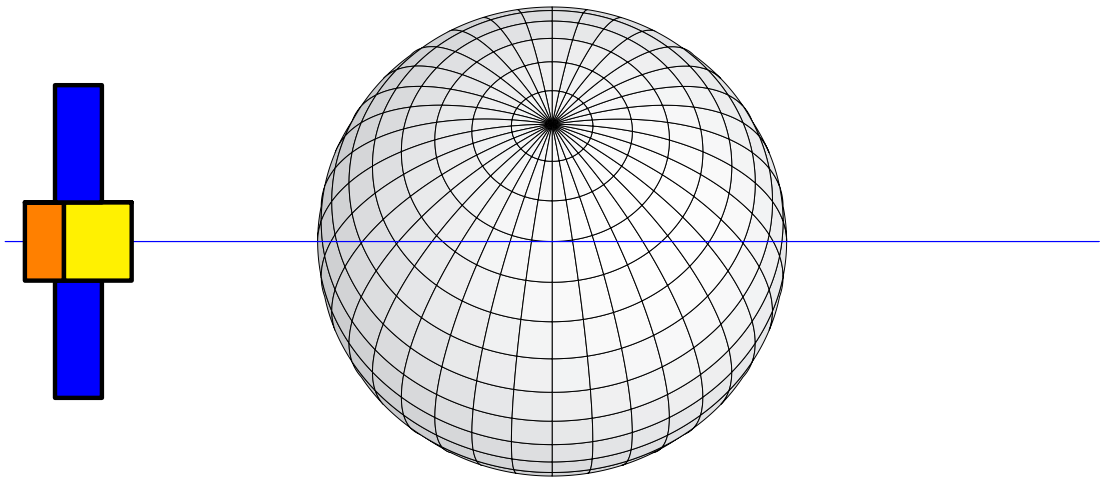

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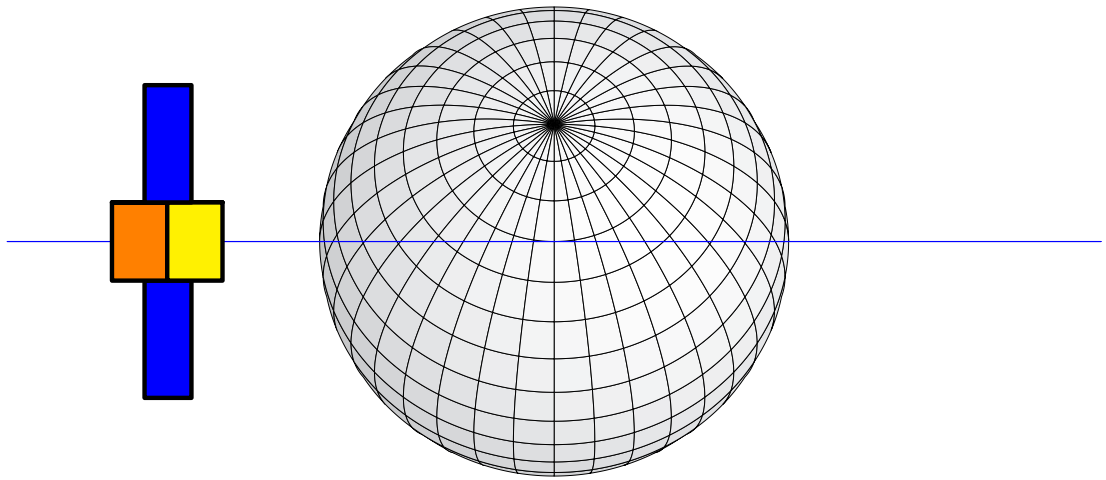

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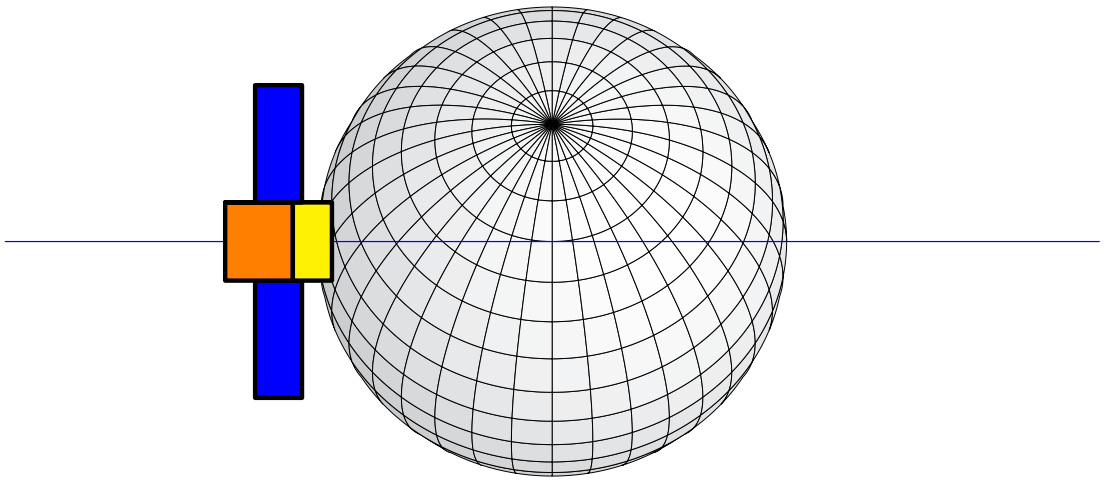

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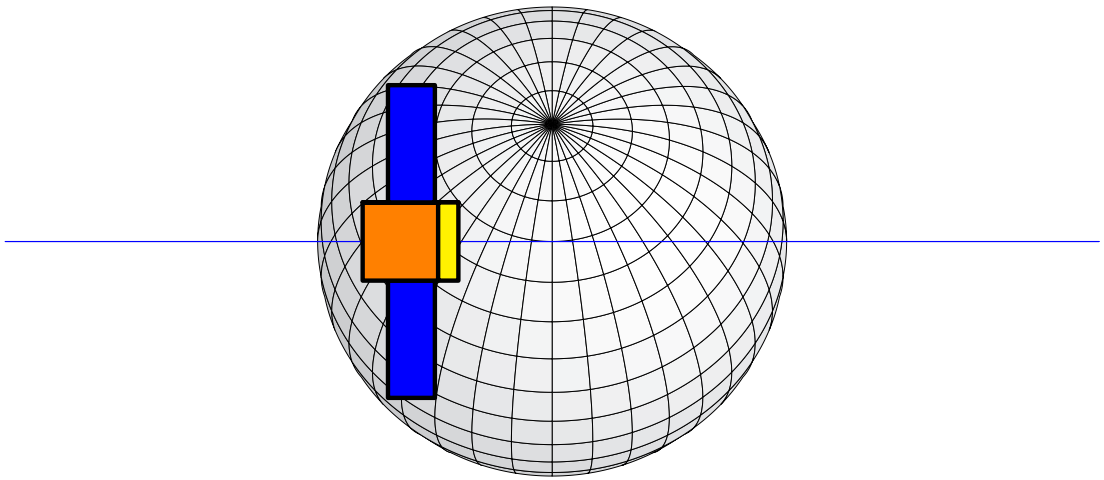

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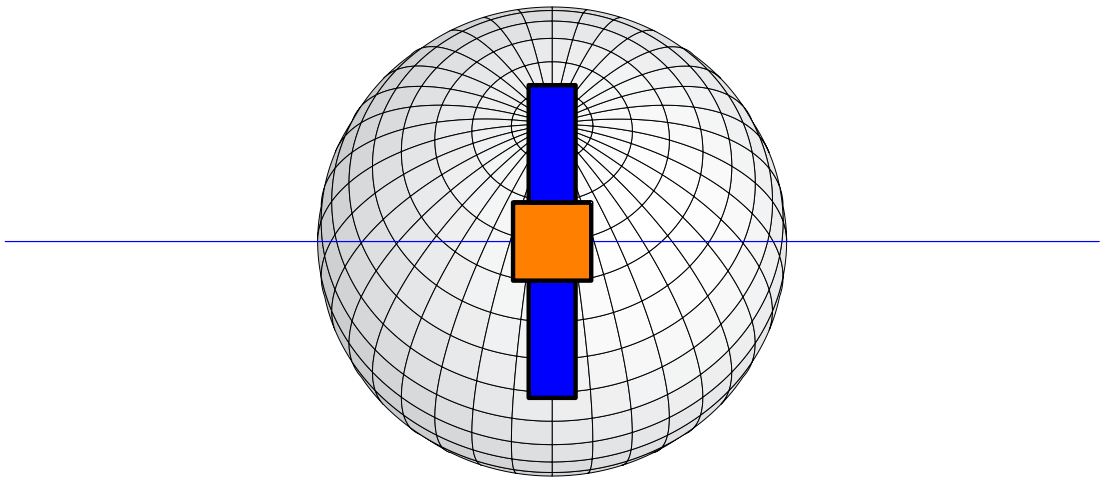

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Conclusions

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Observing the satellite from the Sun

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- If the Sun is perpenticular to the orbital plane no periodic solar radiation pressure perturbations are expected.
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Observing the satellite from the Sun

Conclusions

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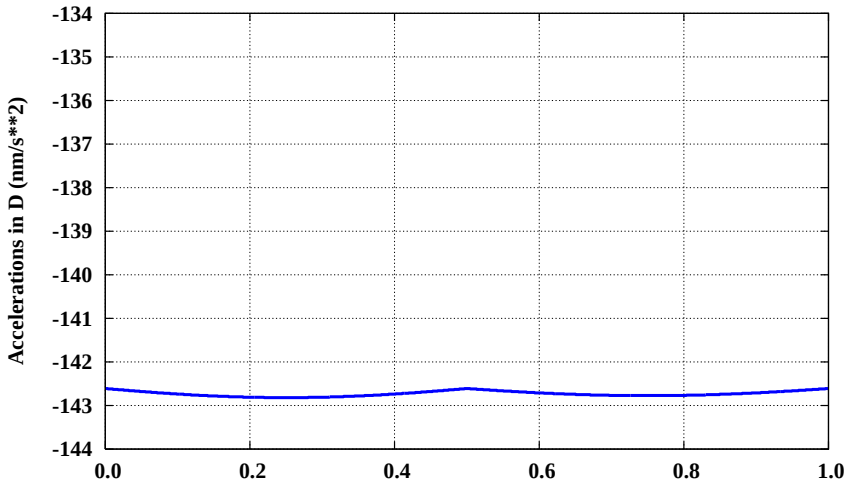
- If the Sun is perpenticular to the orbital plane no periodic solar radiation pressure perturbations are expected.
- If the Sun is located in the orbital plane a once–per–revolution signal is expected in the X–direction and a twice–per–revolution signal in the D–direction.
- These periodic signals are the more pronounced the more the satellite body deviates from a sphere
  (less for a cube – GPS – than a cylinder – GLONASS)

Solar radiation pressure from models

Accelerations derived for GLONASS satellites from a boxwing model[1]

D component



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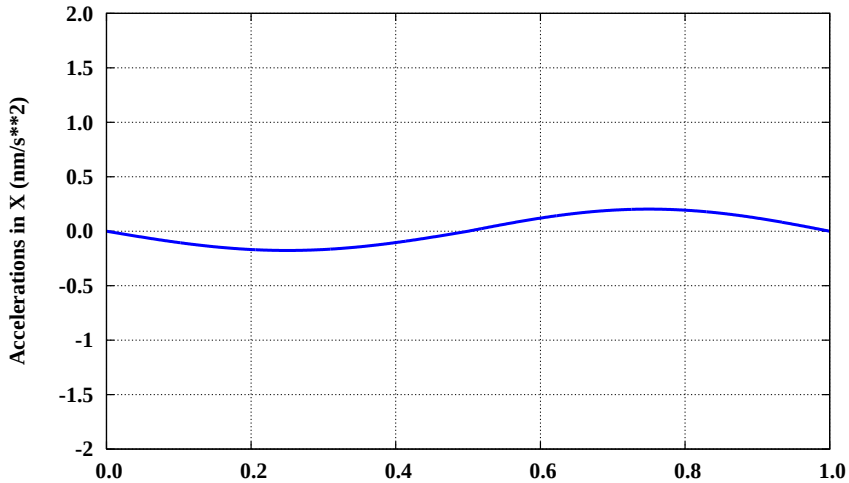

Computed for $\beta = 88°$

[1] as proposed by Carlos Rodriguez–Solano for the IGS based on Ziebart (2001)

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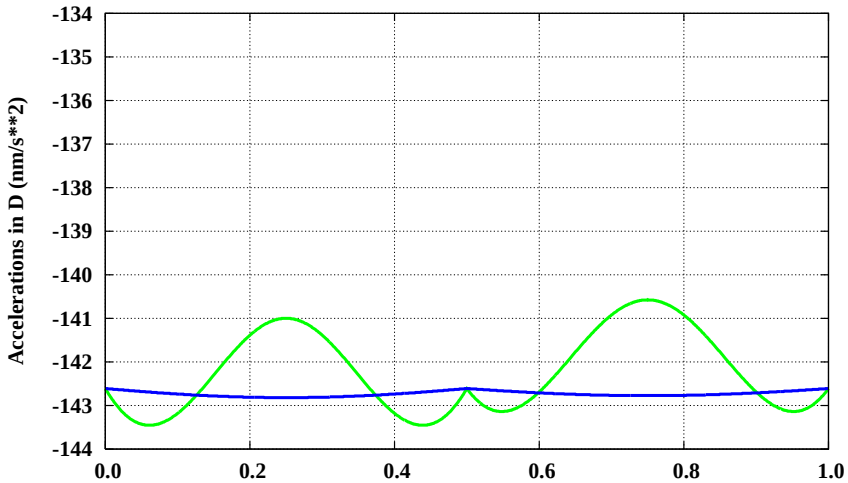

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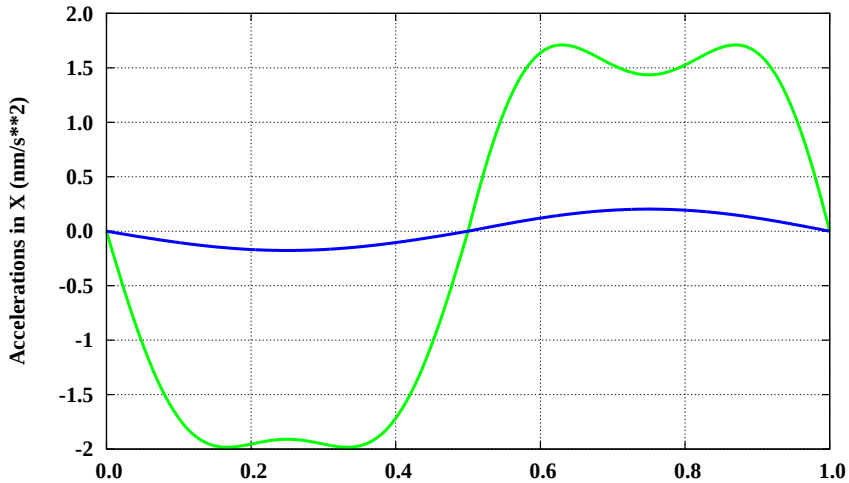

Computed for $\beta = 45°$ $\beta = 88°$

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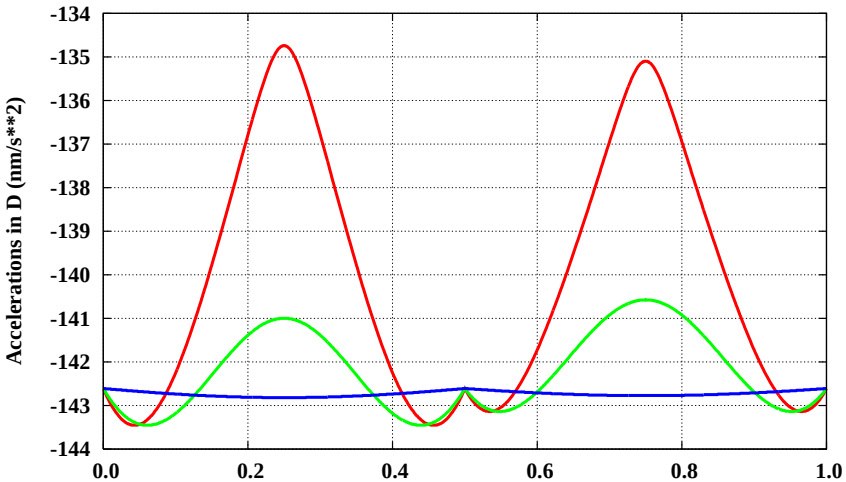
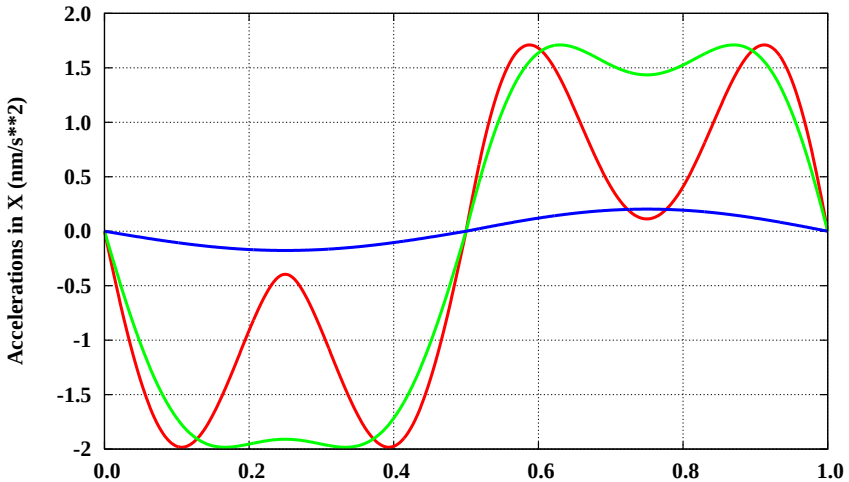
Accelerations derived for GLONASS satellites from a boxwing model[1]

D component



X component



Computed for $\beta = 10°$ $\beta = 45°$ $\beta = 88°$

[1] as proposed by Carlos Rodriguez–Solano for the IGS based on Ziebart (2001)

Solar radiation pressure from models

Accelerations derived for GLONASS satellites from a boxwing model[1]

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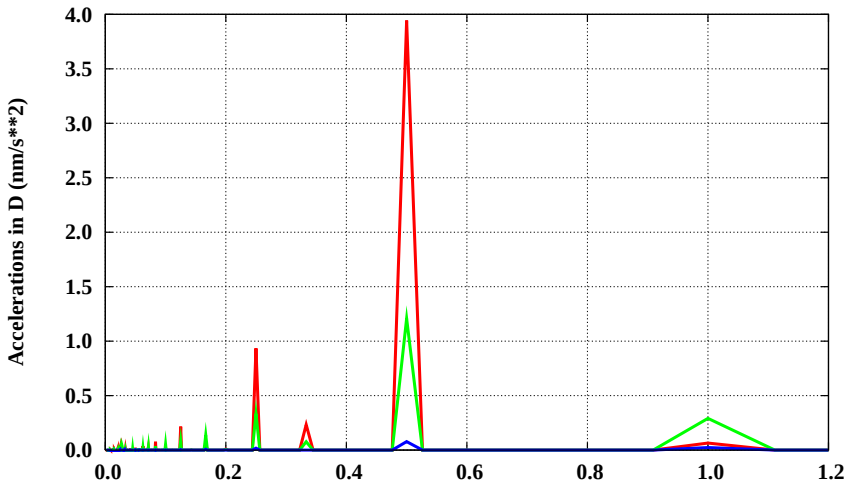
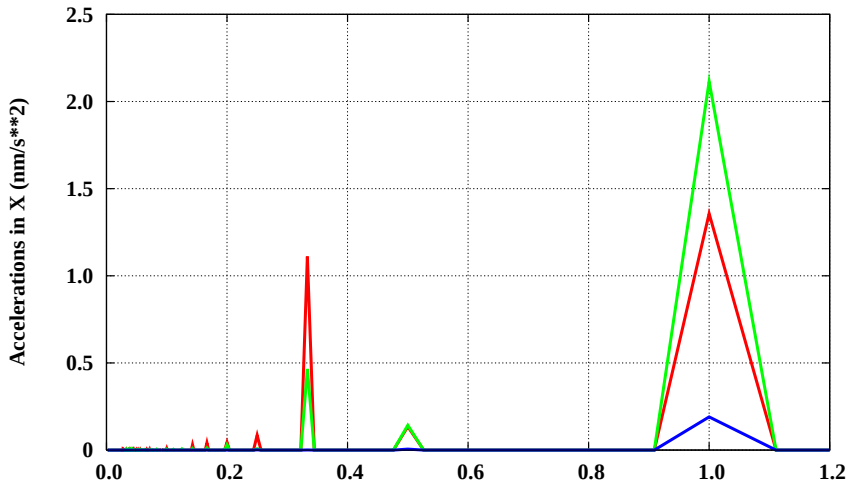


X component



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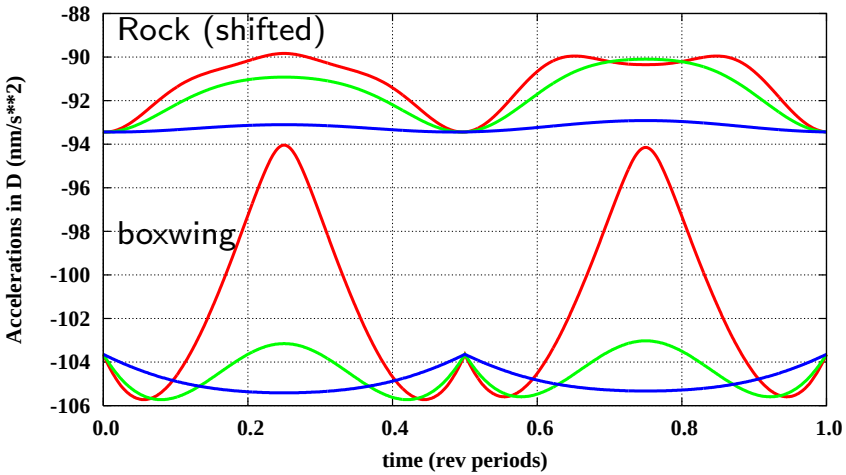
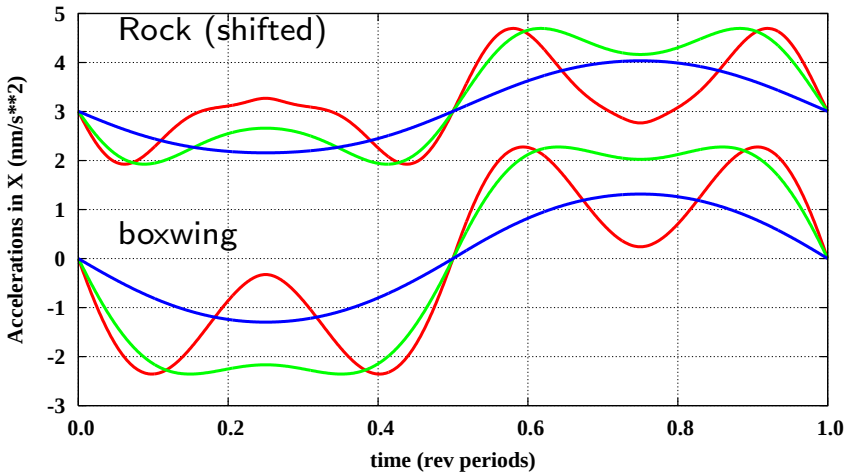
Solar radiation pressure from models

Accelerations derived for GPS (Block IIA) satellites from a boxwing[2] and Rock-S[3] model

D component



X component



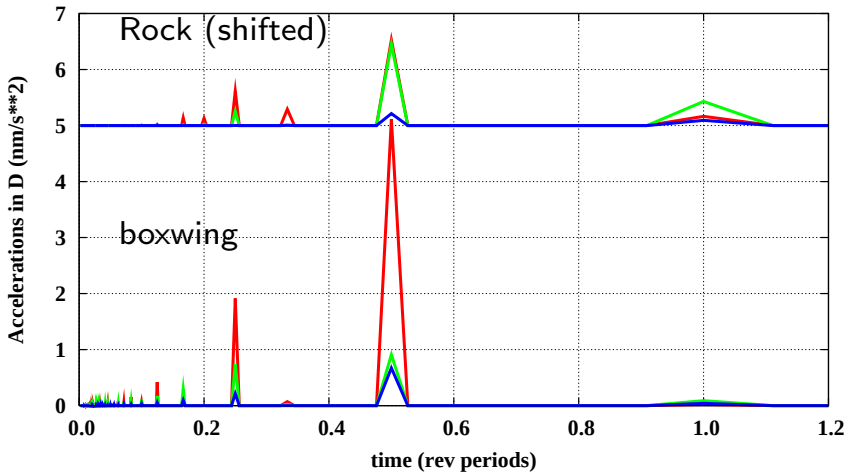
Computed for $\beta = 10°$ $\beta = 45°$ $\beta = 78°$

[2] as proposed by Carlos Rodriguez–Solano based on Fliegel et al. (1992)
[3] Fliegel et al. (1992)

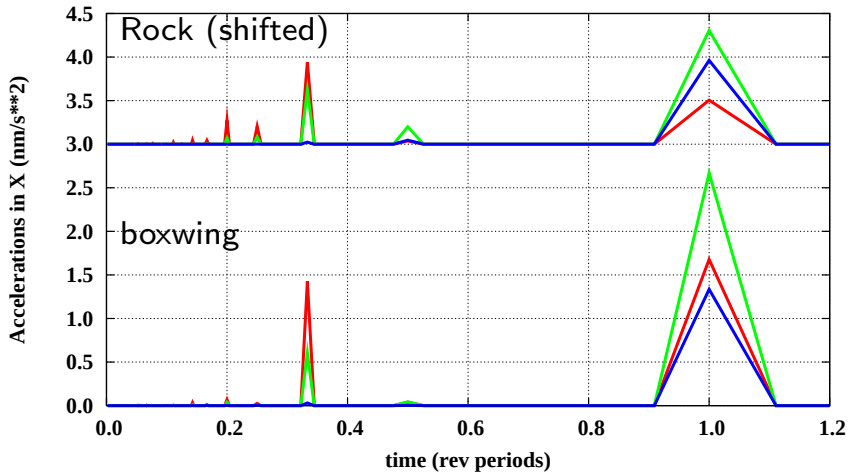
Solar radiation pressure from models

Accelerations derived for GPS (Block IIA) satellites from a boxwing[2] and Rock-S[3] model

D component



X component



Computed for $\beta = 10°$ $\beta = 45°$ $\beta = 78°$

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Conclusions

- A Sun–fixed argument for the periodic terms is necessary to obtain interpretable series of these parameters:

$$u' = u_{sat} - u_{Sun}$$

Solar radiation pressure from models

Conclusions

- A Sun–fixed argument for the periodic terms is necessary to obtain interpretable series of these parameters:

$$u' = u_{sat} - u_{Sun}$$

- Solar radiation pressure for satellites flying according to the previously mentioned models can be represented by:

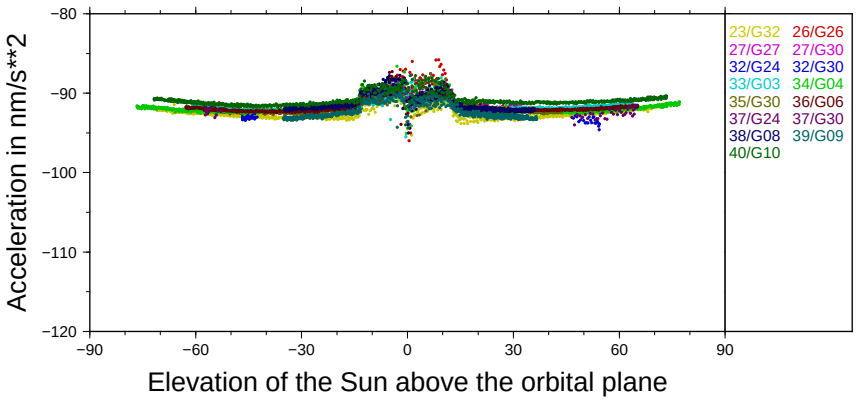
$$\begin{aligned} D &= D_0 + D_2 \cos(2u') + D_4 \cos(4u') + \ldots \\ Y &= (Y_0) \\ X &= X_1 \cos(1u') + X_3 \cos(3u') + \ldots \end{aligned}$$

$Y_0 \neq 0$ if the satellite is flying "missaligned" with a Y–bias (e.g., GPS, except for Block IIF).

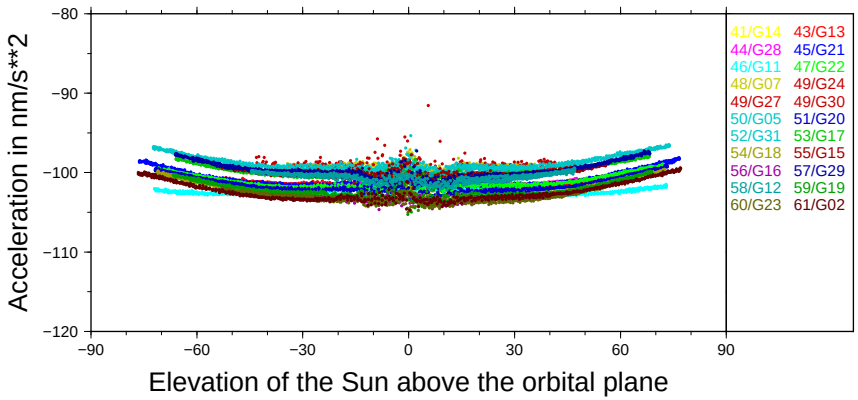
Estimated solar radiation pressure

Component: D_0

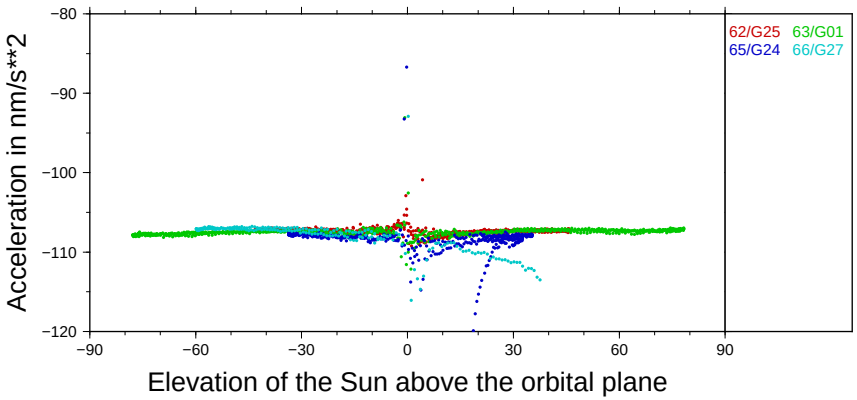
GPS Block IIA



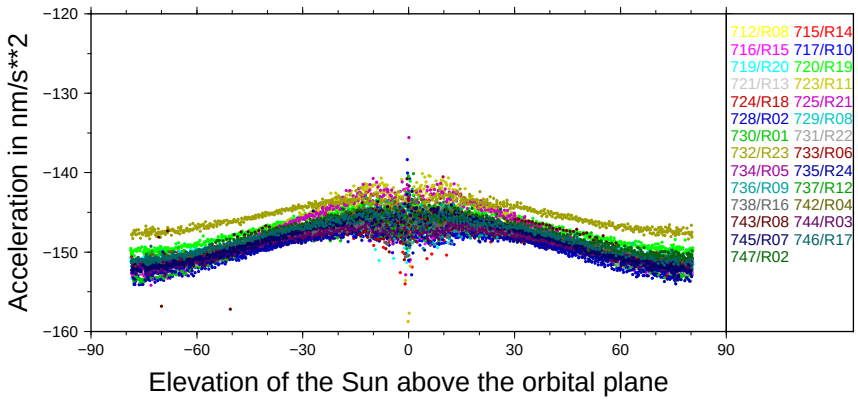
GPS Block IIR



GPS Block IIF



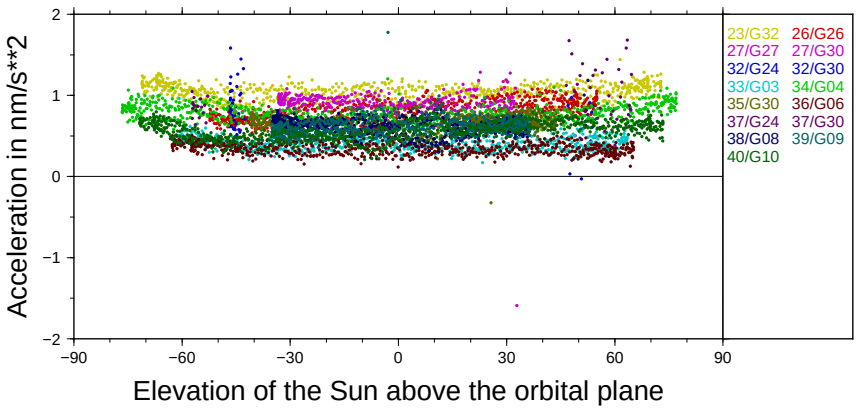
GLONASS–M



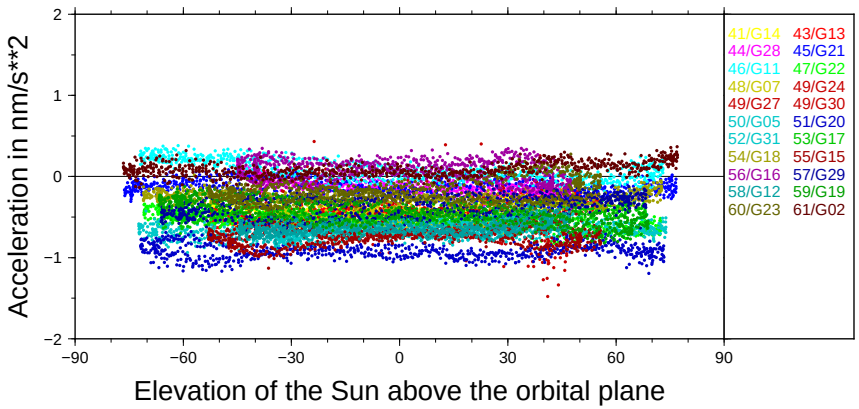
Estimated solar radiation pressure

Component: Y_0 (small scale)

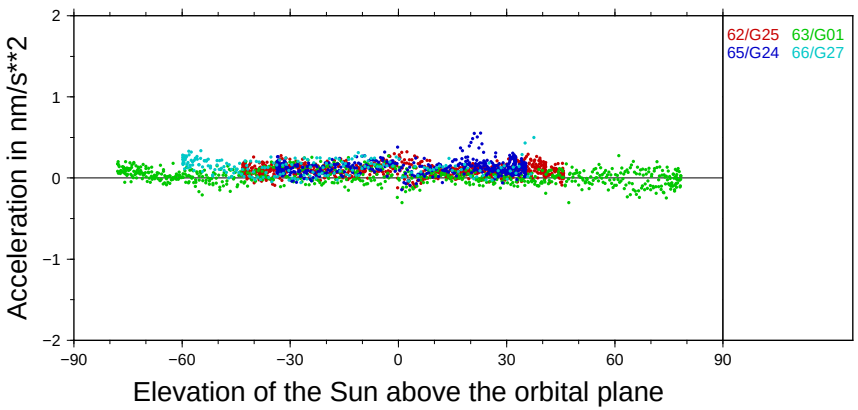
GPS Block IIA



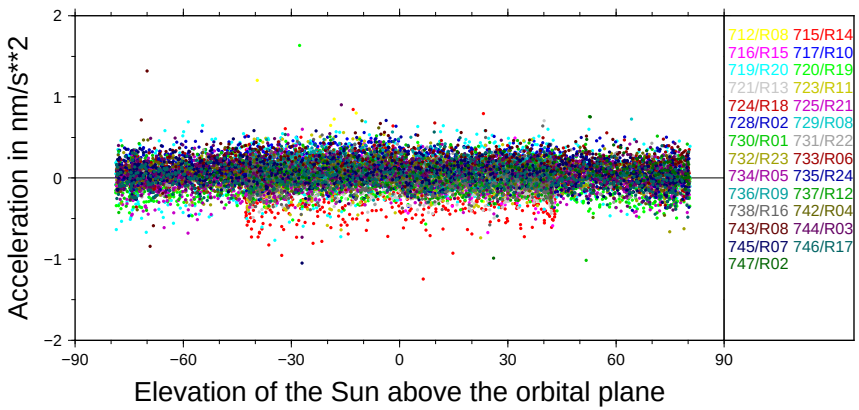
GPS Block IIR



GPS Block IIF



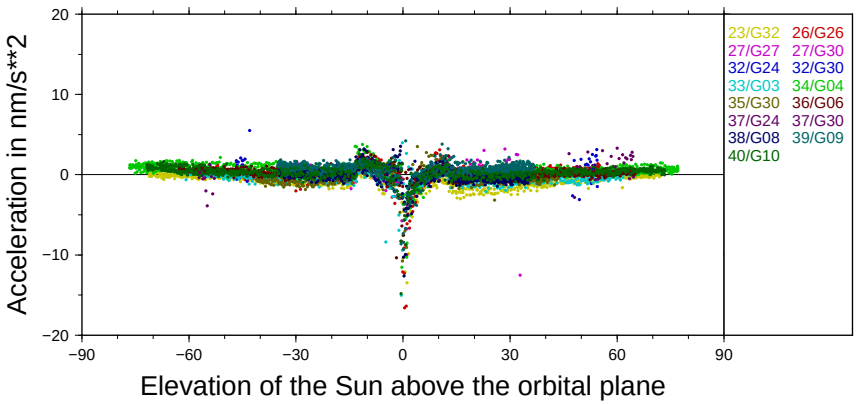
GLONASS–M



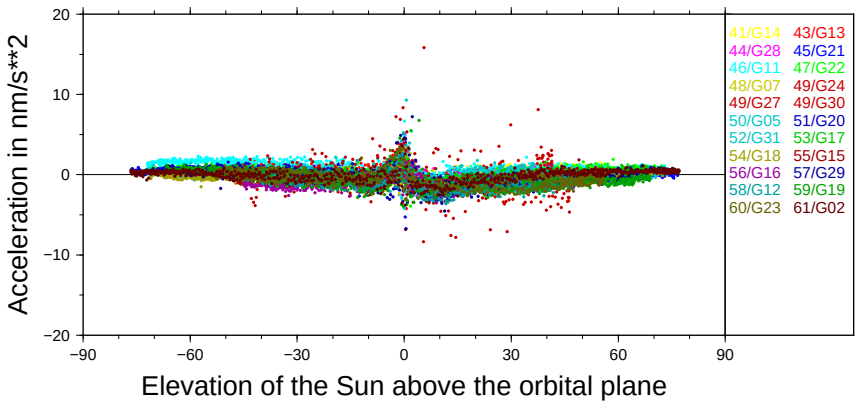
Estimated solar radiation pressure

Component: $X_1 \cdot \cos(1u')$

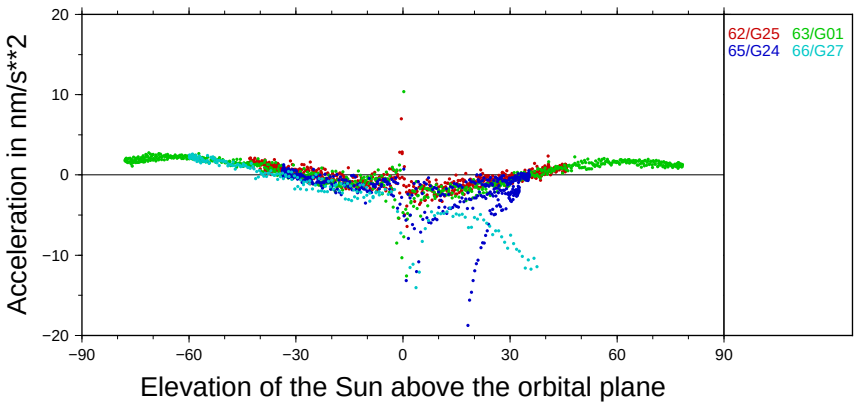
GPS Block IIA



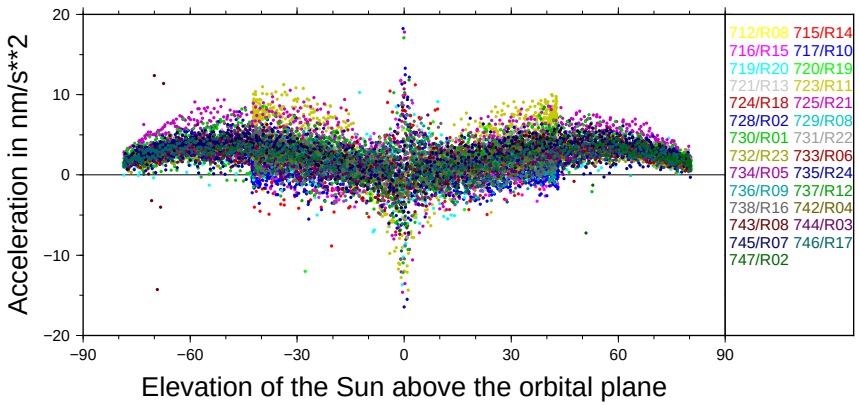
GPS Block IIR



GPS Block IIF



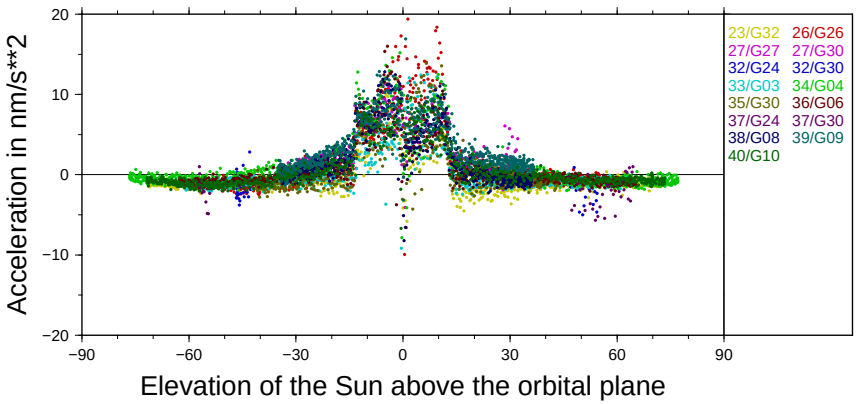
GLONASS–M



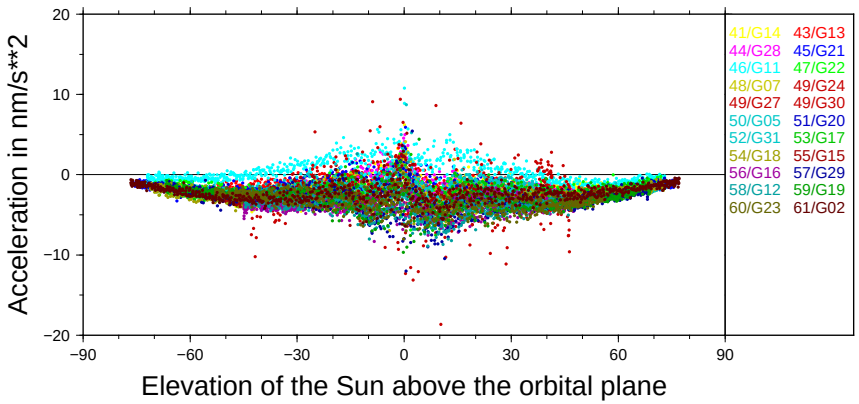
Estimated solar radiation pressure

Component: $D_2 \cdot \cos(2u')$

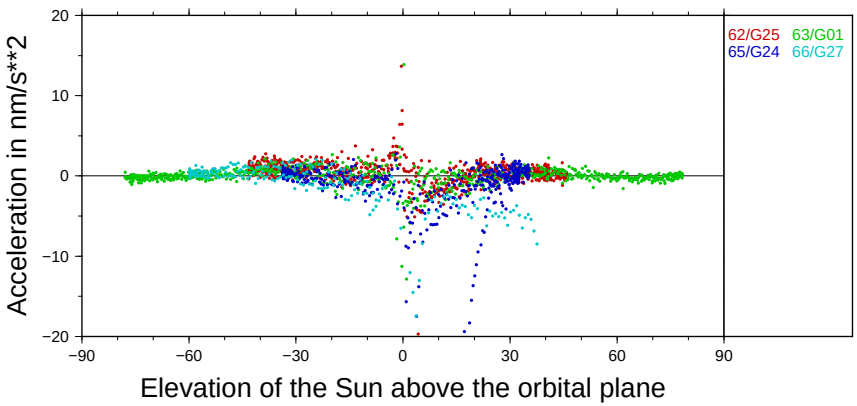
GPS Block IIA



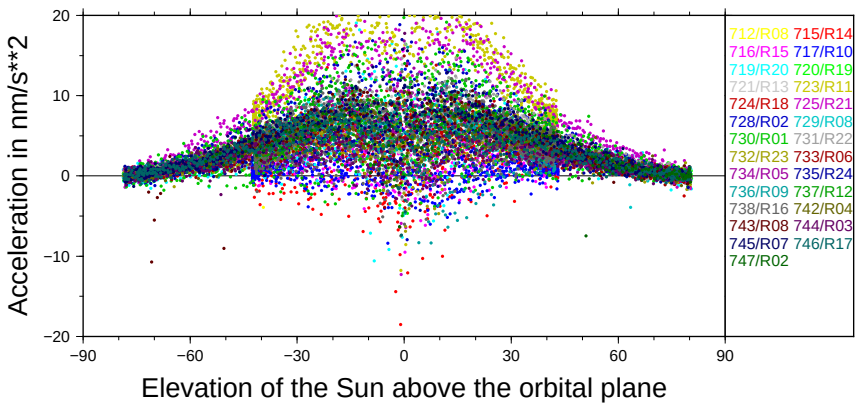
GPS Block IIR



GPS Block IIF



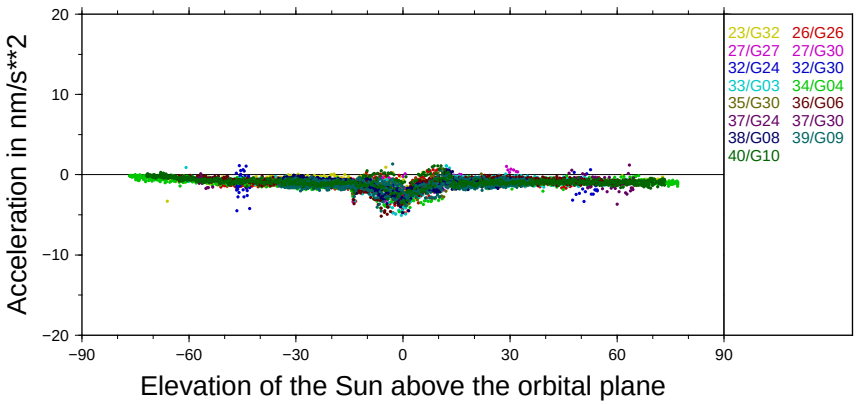
GLONASS–M



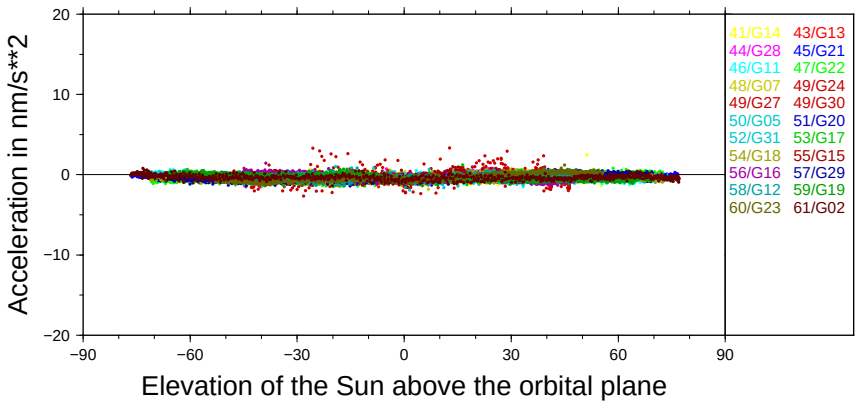
Estimated solar radiation pressure

Component: $X_1 \cdot \sin(1u')$

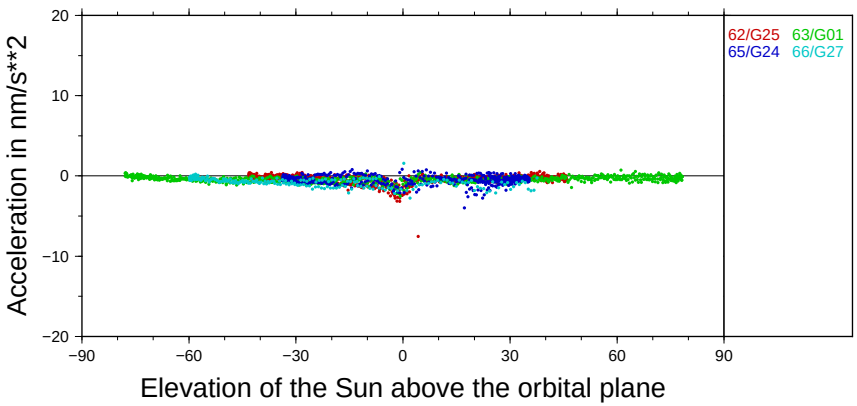
GPS Block IIA



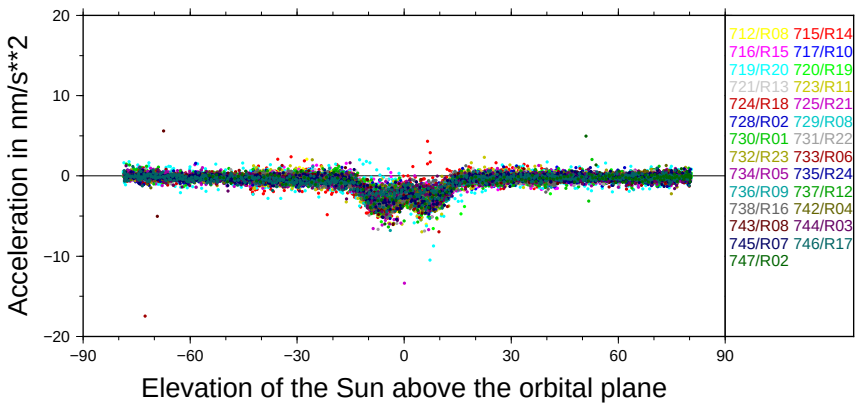
GPS Block IIR



GPS Block IIF



GLONASS–M



Estimated solar radiation pressure

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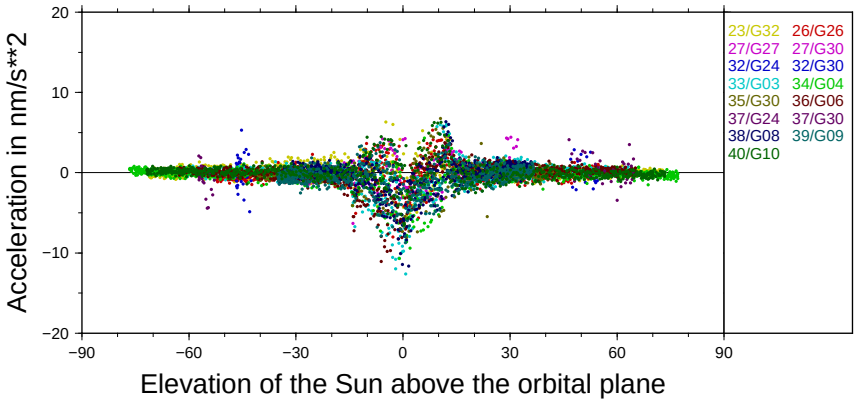
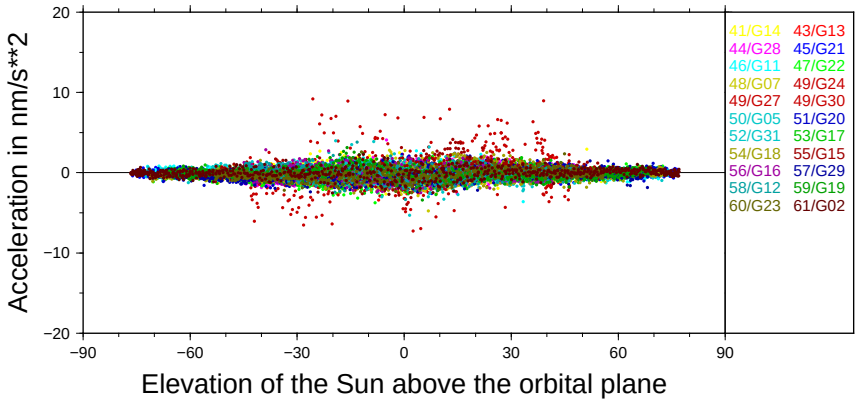
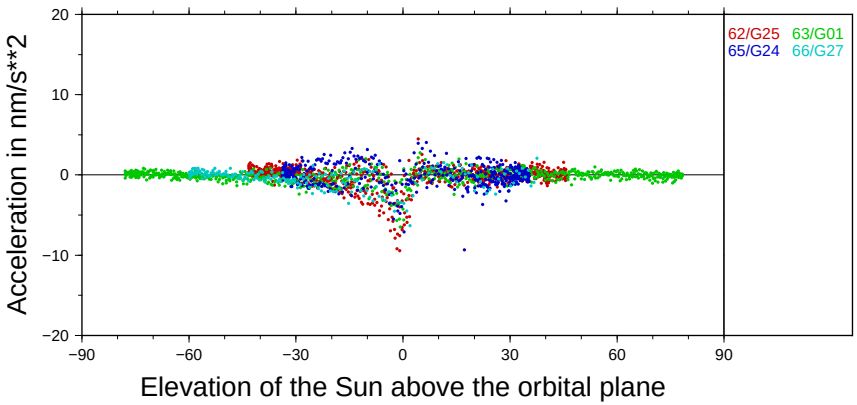
GPS Block IIA



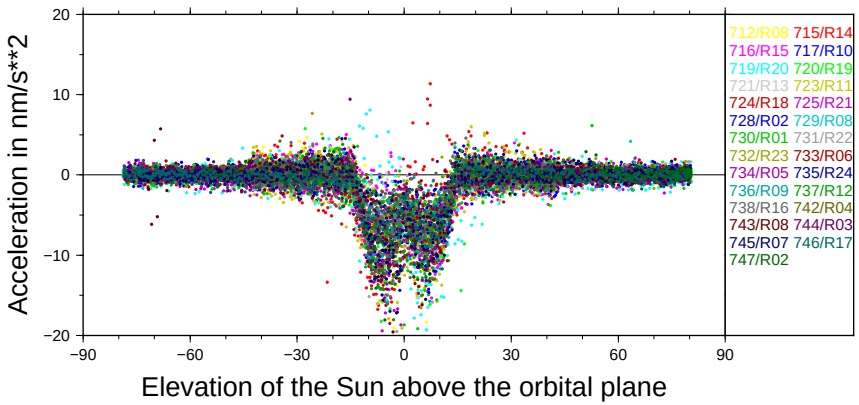
GPS Block IIR



GPS Block IIF

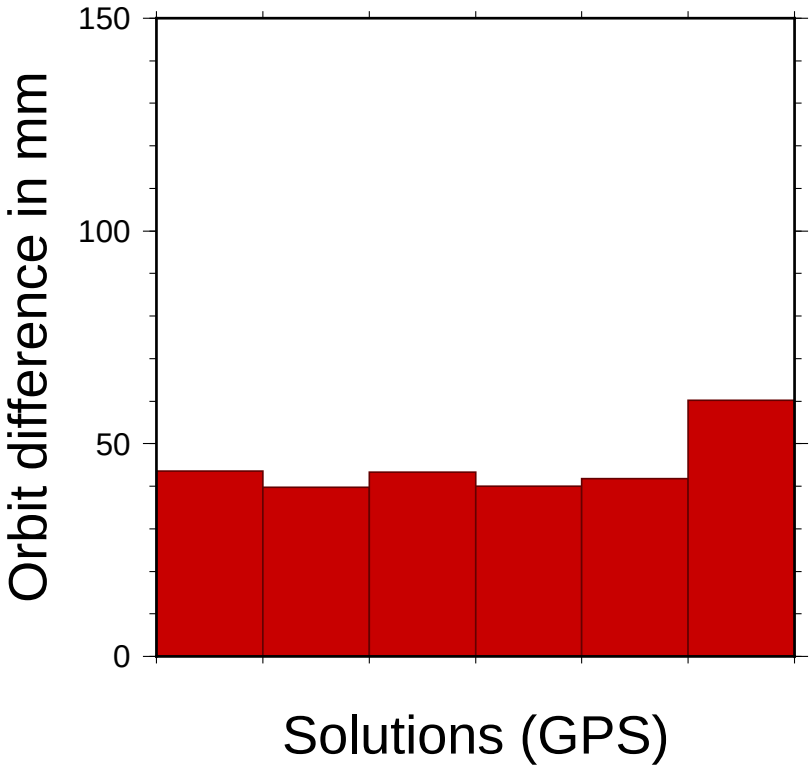


GLONASS–M



Impact on the GNSS Satellite orbits

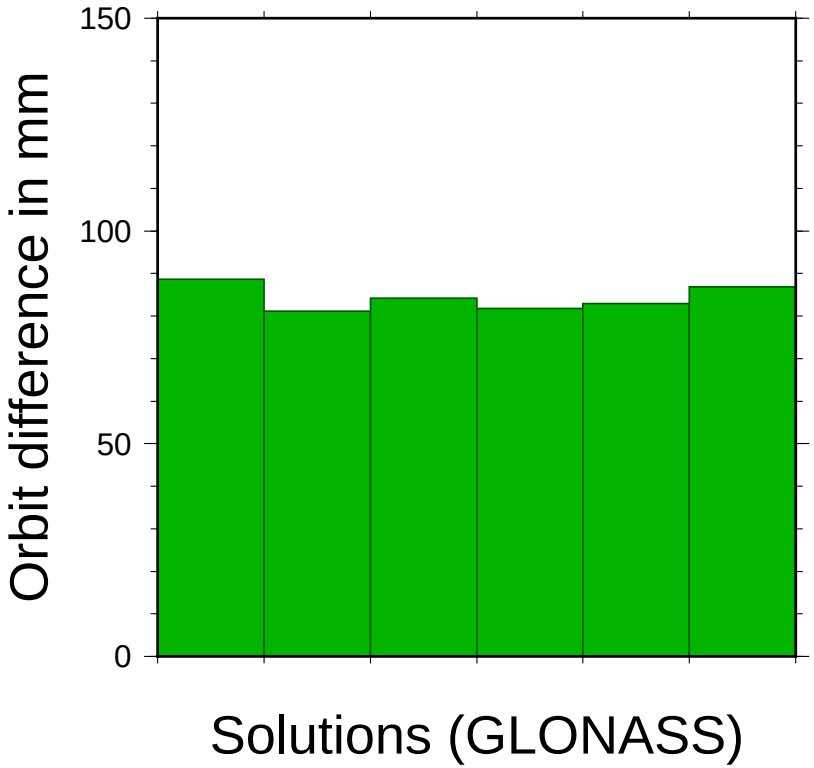
Orbit overlaps from one–day solutions (mean over all components)



Components of the orbit model:

X

D



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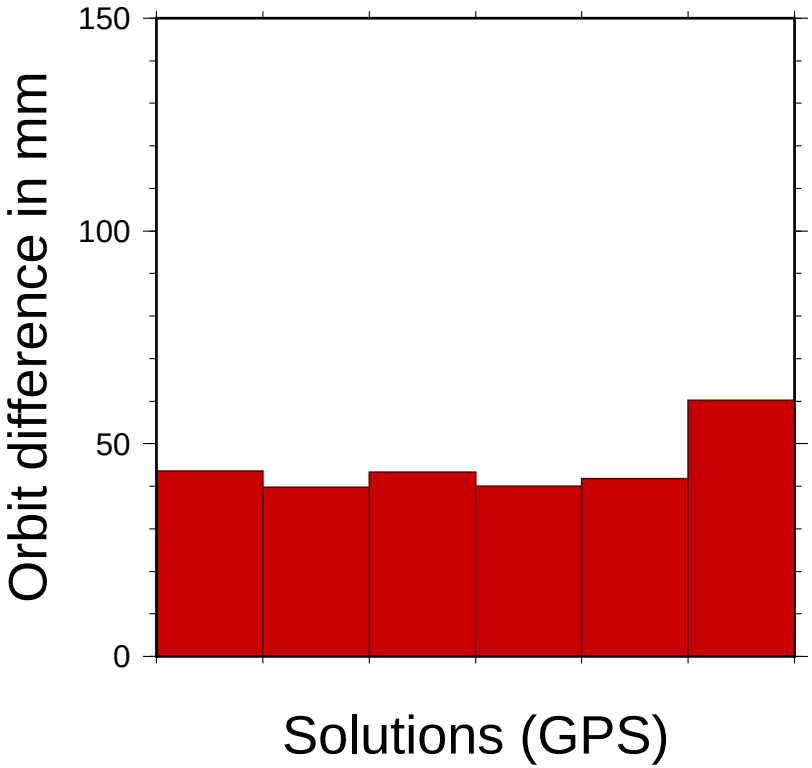
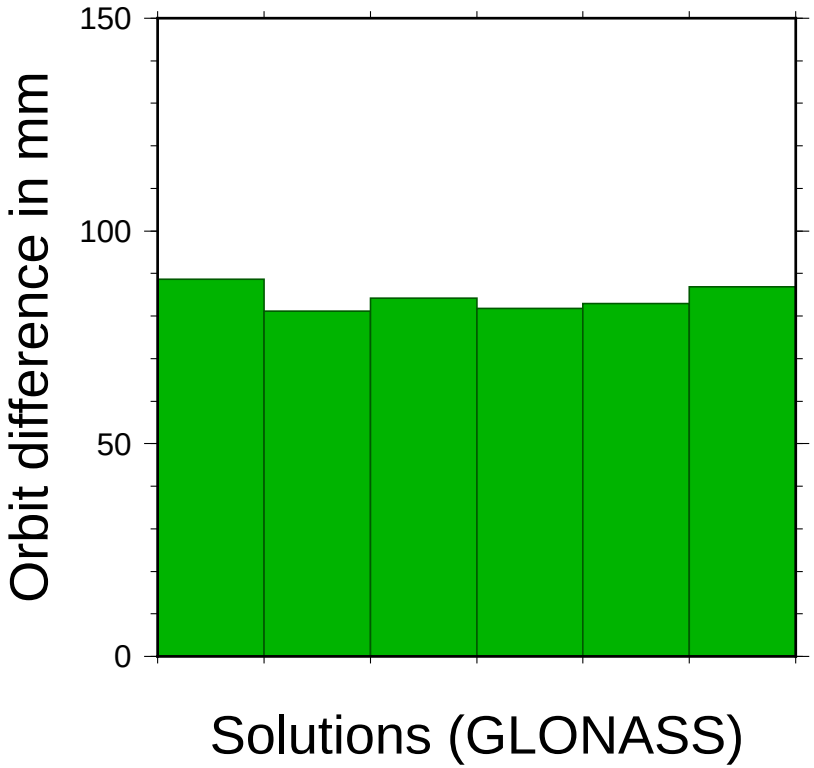


Components of the orbit model:

X $1u'$

D –



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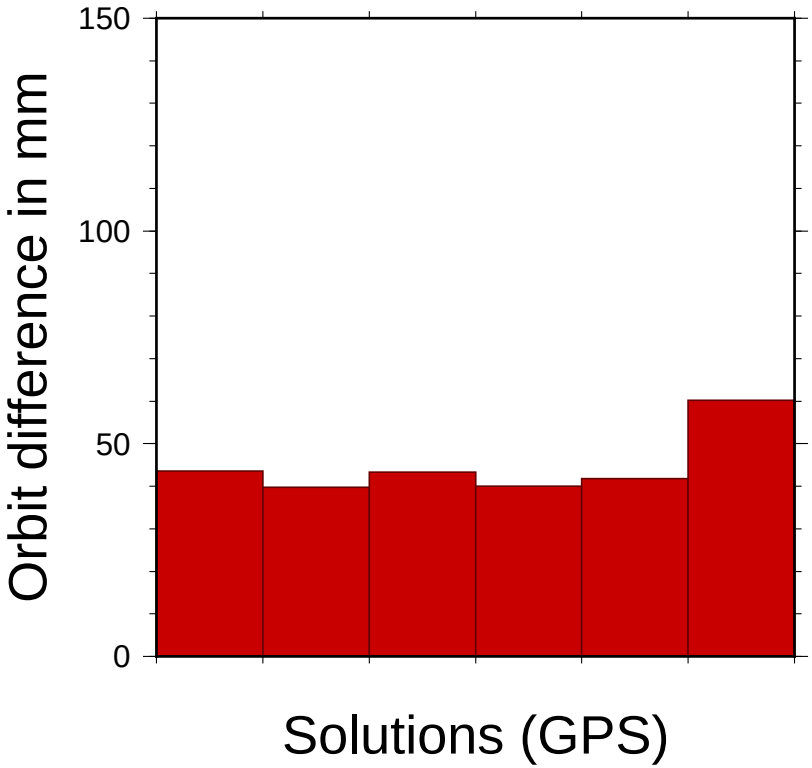
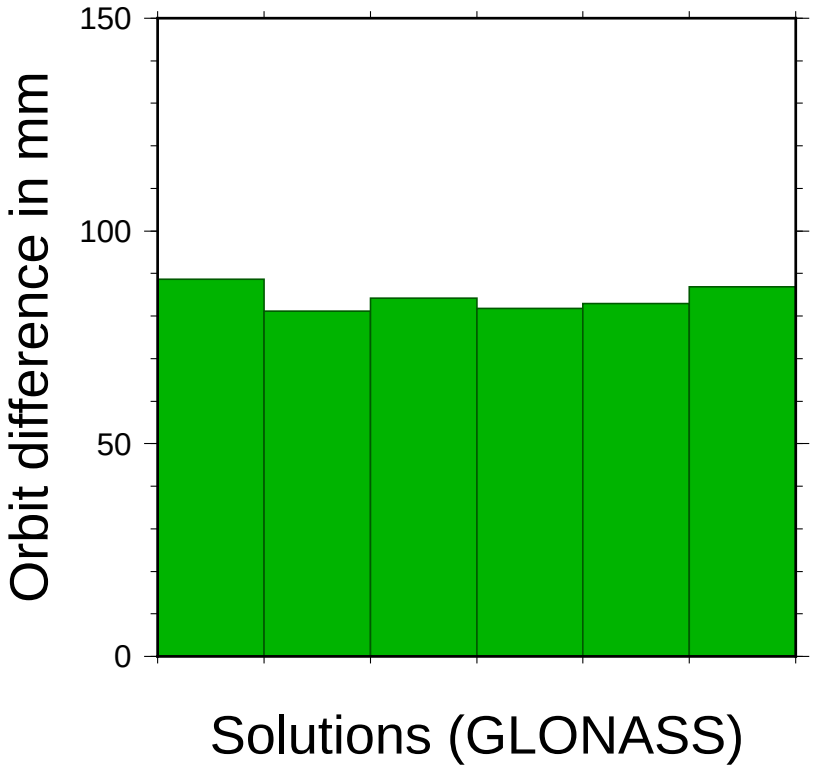


Components of the orbit model:

X	$1u'$	$1u'$
D	–	$2u'$



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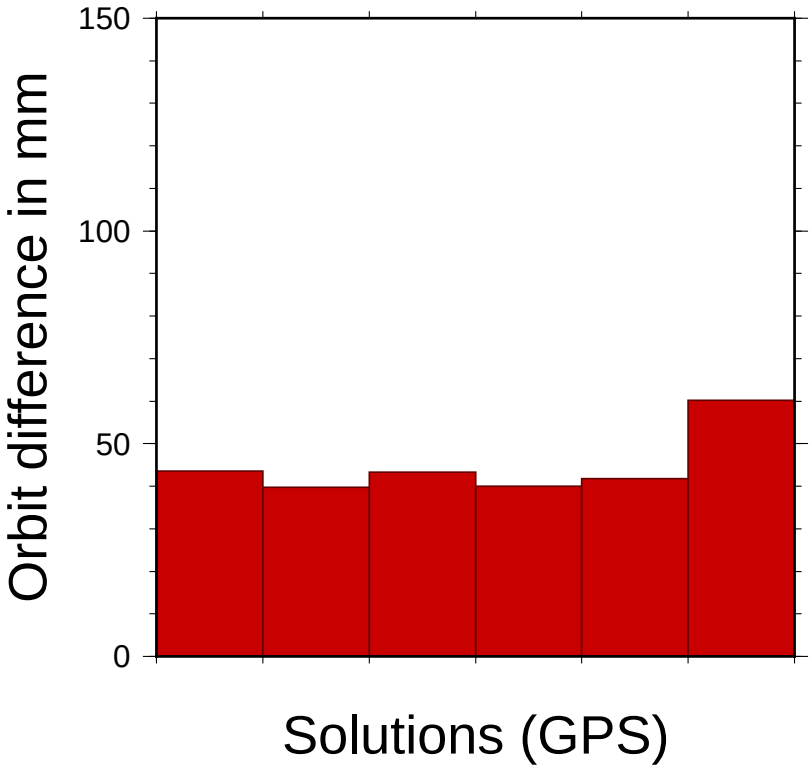
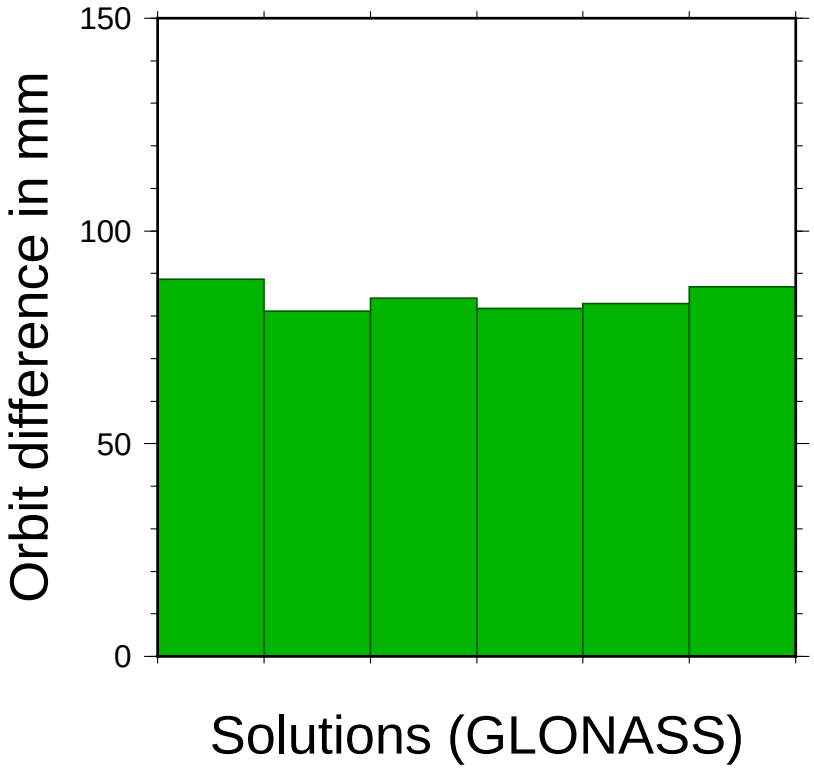


Components of the orbit model:

X	$1u'$	$1u'$	–
D	–	$2u'$	$2u'$



Components of the orbit model:

X	$1u'$	$1u'$	–
D	–	$2u'$	$2u'$

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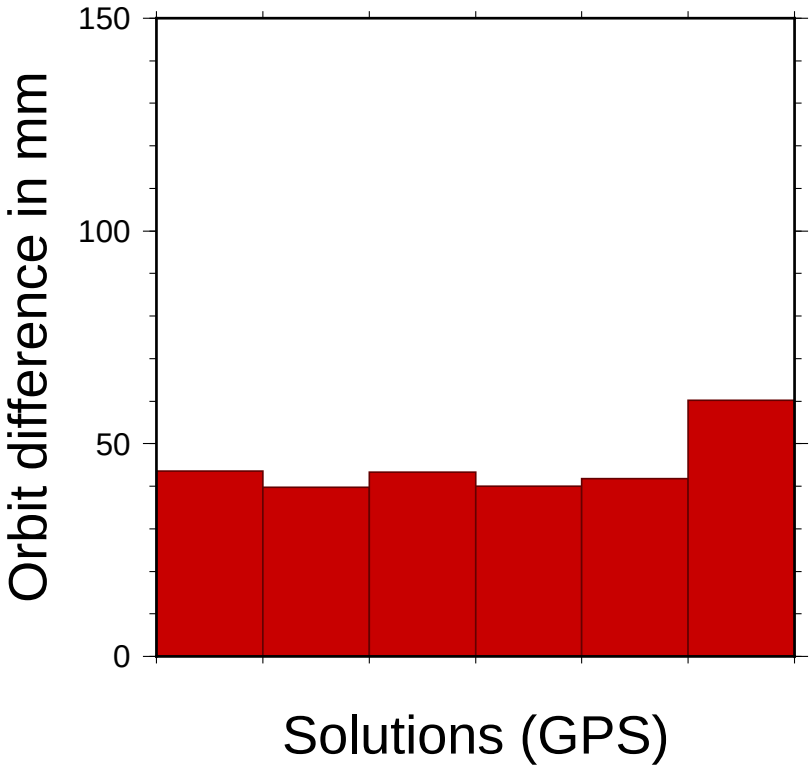
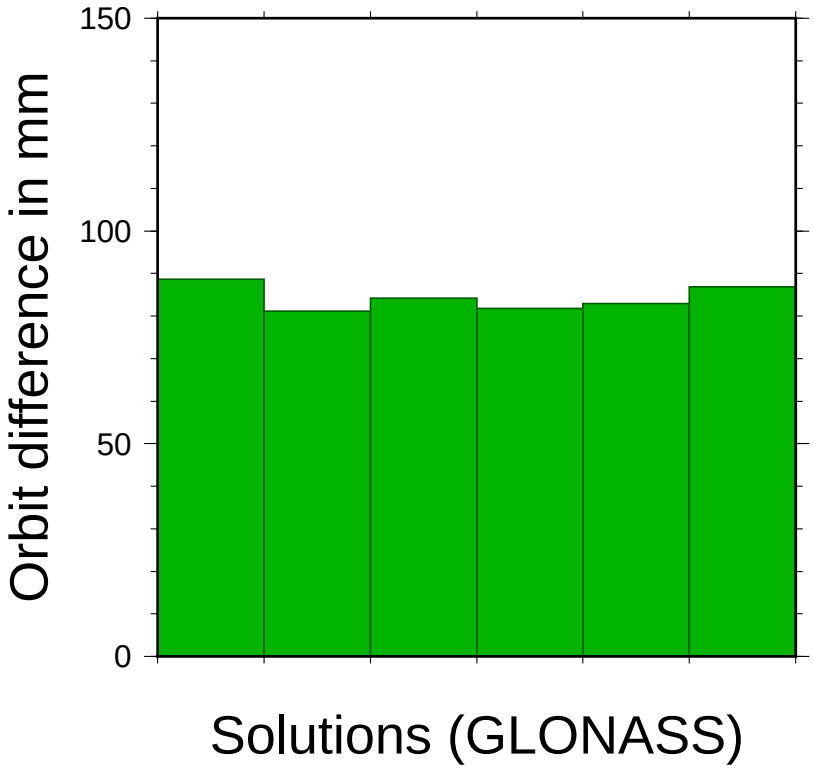


Components of the orbit model:

X	$1u'$	$1u'$	–	$1u'$
D	–	$2u'$	$2u'$	$2u'$
				$4u'$

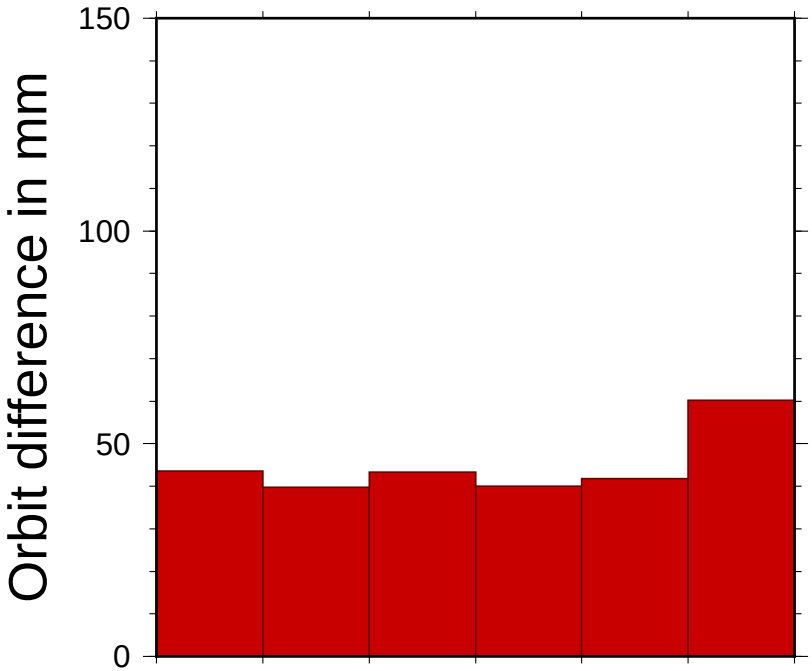


Components of the orbit model:

X	$1u'$	$1u'$	–	$1u'$
D	–	$2u'$	$2u'$	$2u'$
				$4u'$

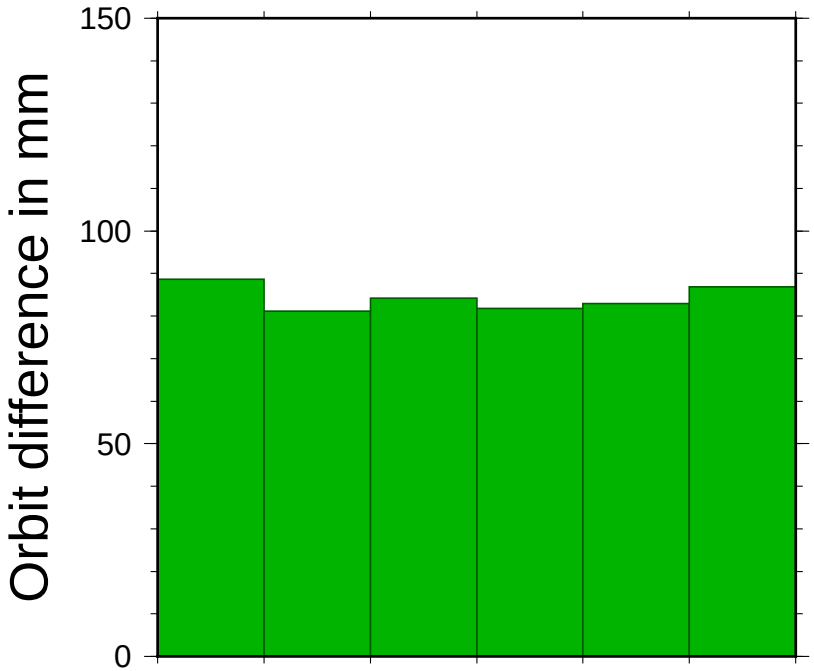
Impact on the GNSS Satellite orbits

Orbit overlaps from one–day solutions (mean over all components)



Components of the orbit model:

X	$1u'$	$1u'$	–	$1u'$	$1u'$
					$3u'$
D	–	$2u'$	$2u'$	$2u'$	$2u'$
				$4u'$	



Components of the orbit model:

X	$1u'$	$1u'$	–	$1u'$	$1u'$
					$3u'$
D	–	$2u'$	$2u'$	$2u'$	$2u'$
				$4u'$	

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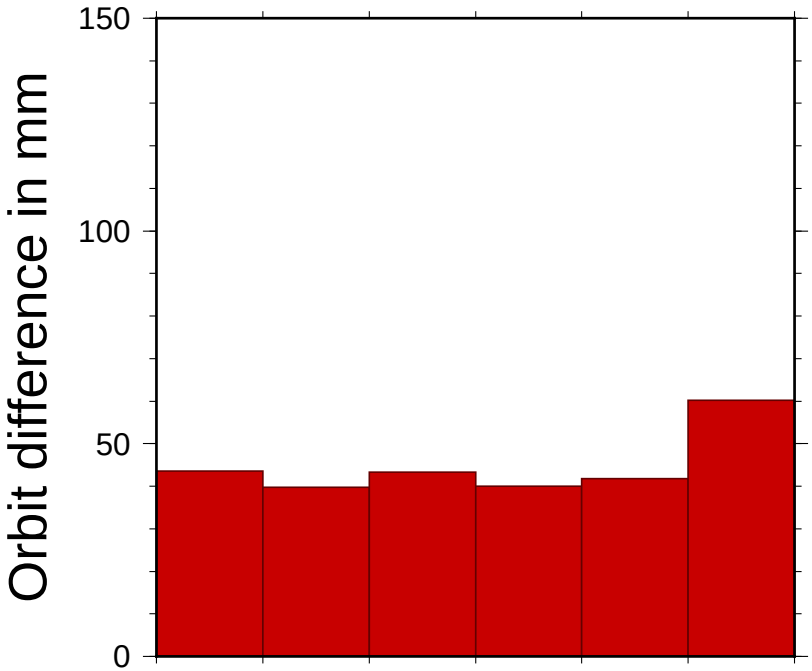
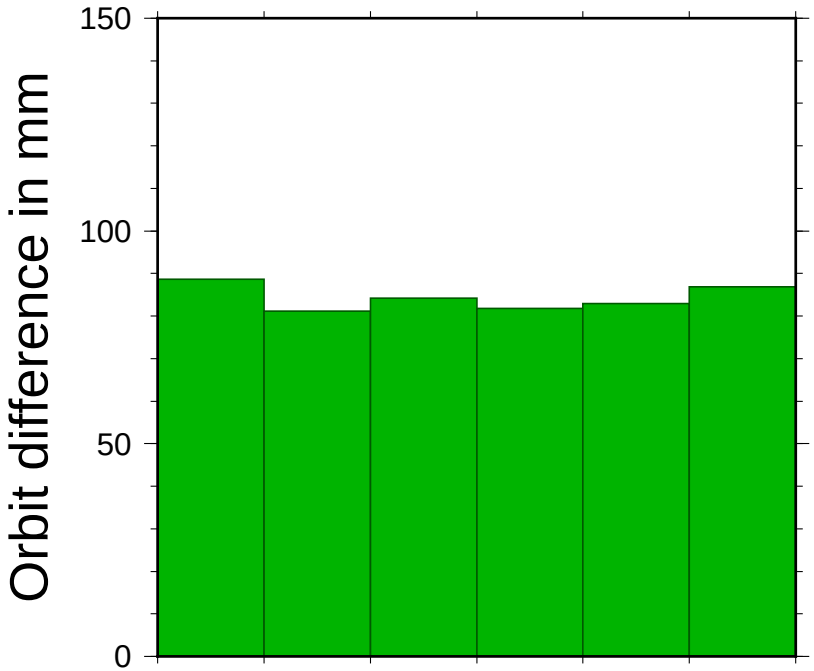
Orbit overlaps from one–day solutions (mean over all components)



Components of the orbit model:

X	$1u'$	$1u'$	–	$1u'$	$1u'$	$1u'$
					$3u'$	$3u'$
D	–	$2u'$	$2u'$	$2u'$	$2u'$	$2u'$
				$4u'$		(cos)



Components of the orbit model:

X	$1u'$	$1u'$	–	$1u'$	$1u'$	$1u'$
					$3u'$	$3u'$
D	–	$2u'$	$2u'$	$2u'$	$2u'$	$2u'$
				$4u'$		(cos)

Conclusions

- The new definition of the angular argument ($u' = u_{sat} - u_{Sun}$ instead of u_{sat}) allows it to better interpret of estimated parameter series, e.g., w.r.t. the elevation of the Sun above the orbital plane.

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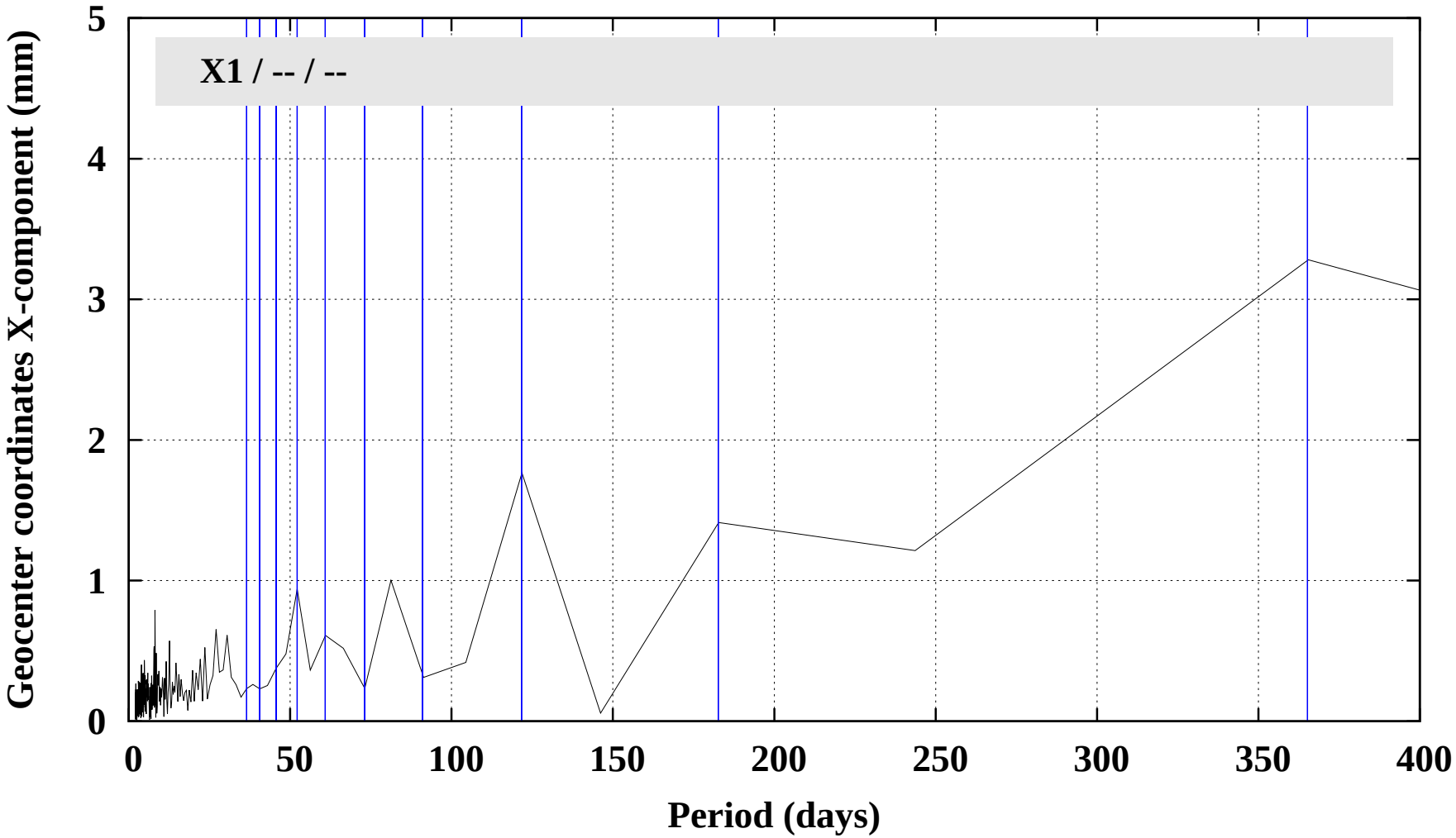
Conclusions

- The new definition of the angular argument ($u' = u_{sat} - u_{Sun}$ instead of u_{sat}) allows it to better interpret of estimated parameter series, e.g., w.r.t. the elevation of the Sun above the orbital plane.
- Adding twice–per–revolution terms in D-component improves the orbit solution.
- Even if the sin-terms are not necessary according to theory they are needed for representing real satellite trajectories.

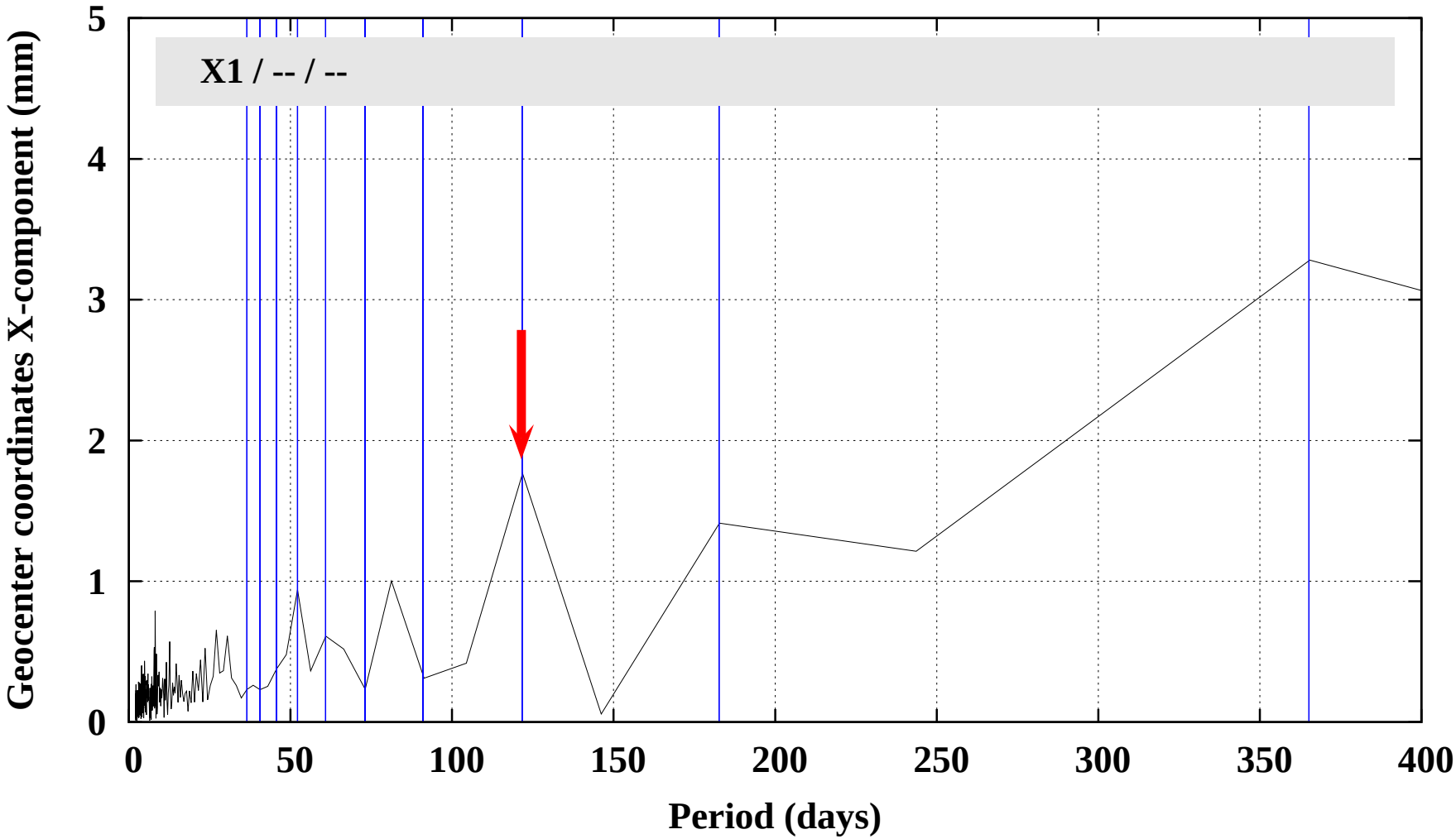
Impact on the Geocenter Estimates

Spectra from geocenter estimates: X component



Impact on the Geocenter Estimates

Spectra from geocenter estimates: X component



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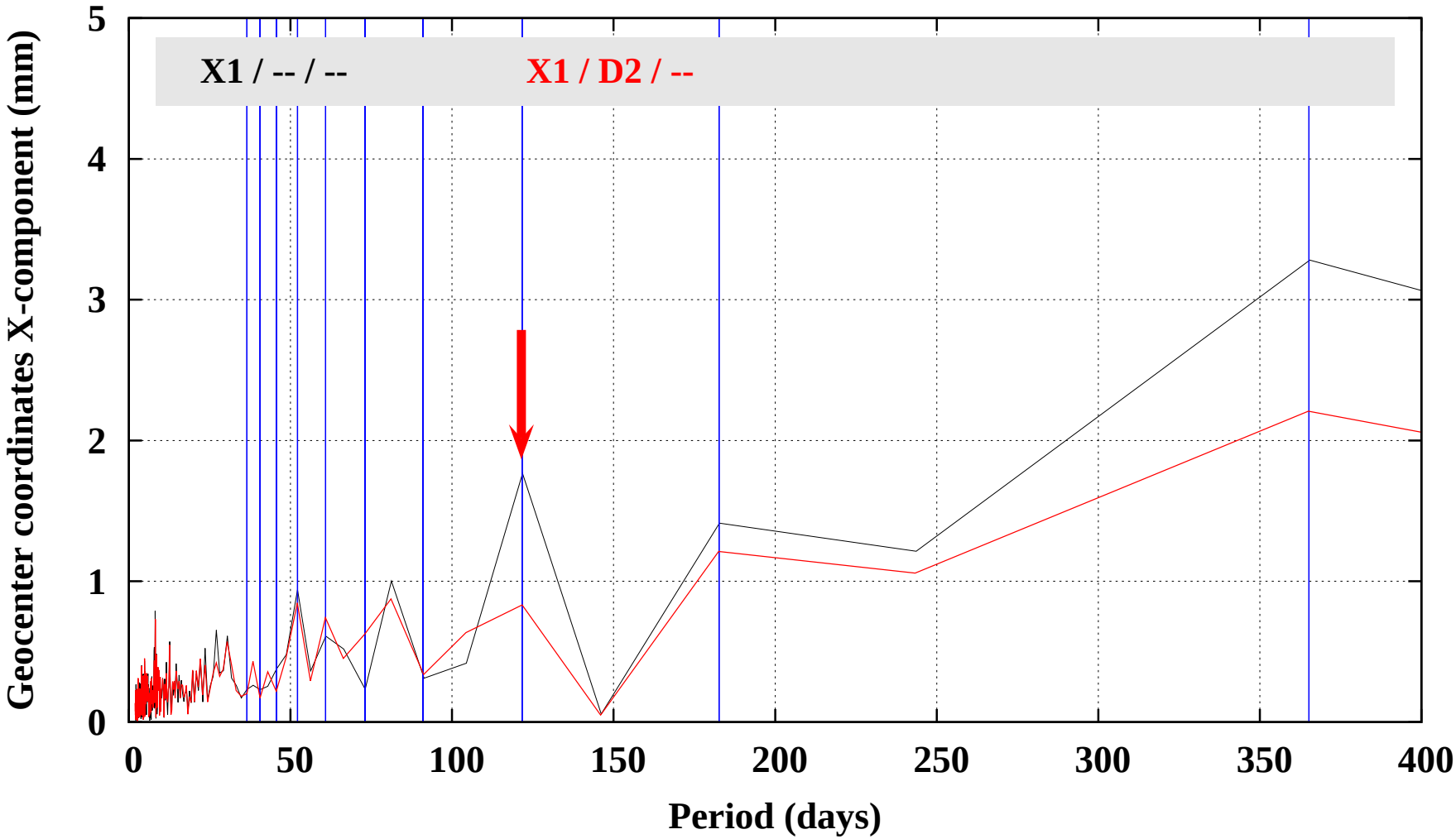

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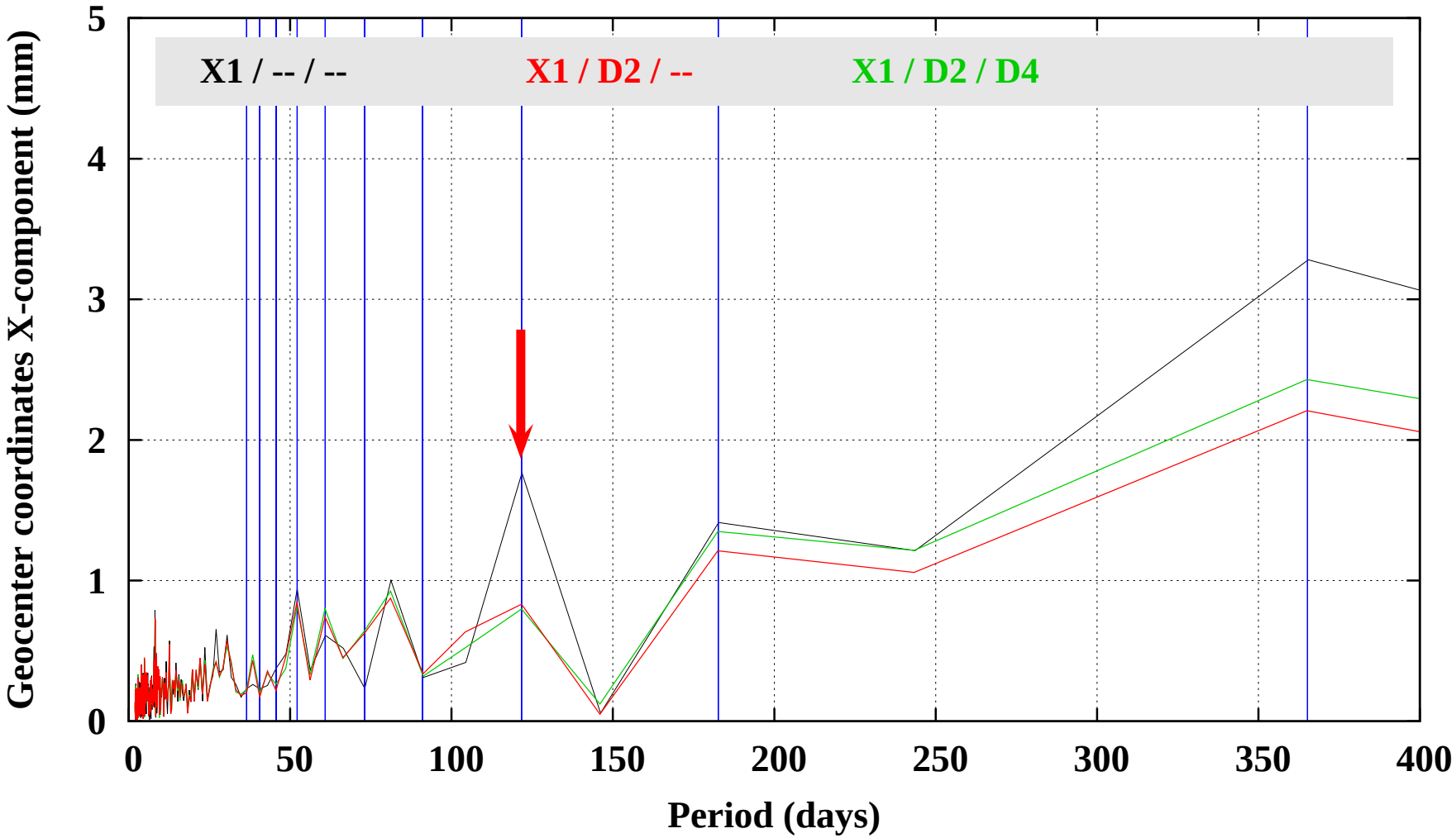

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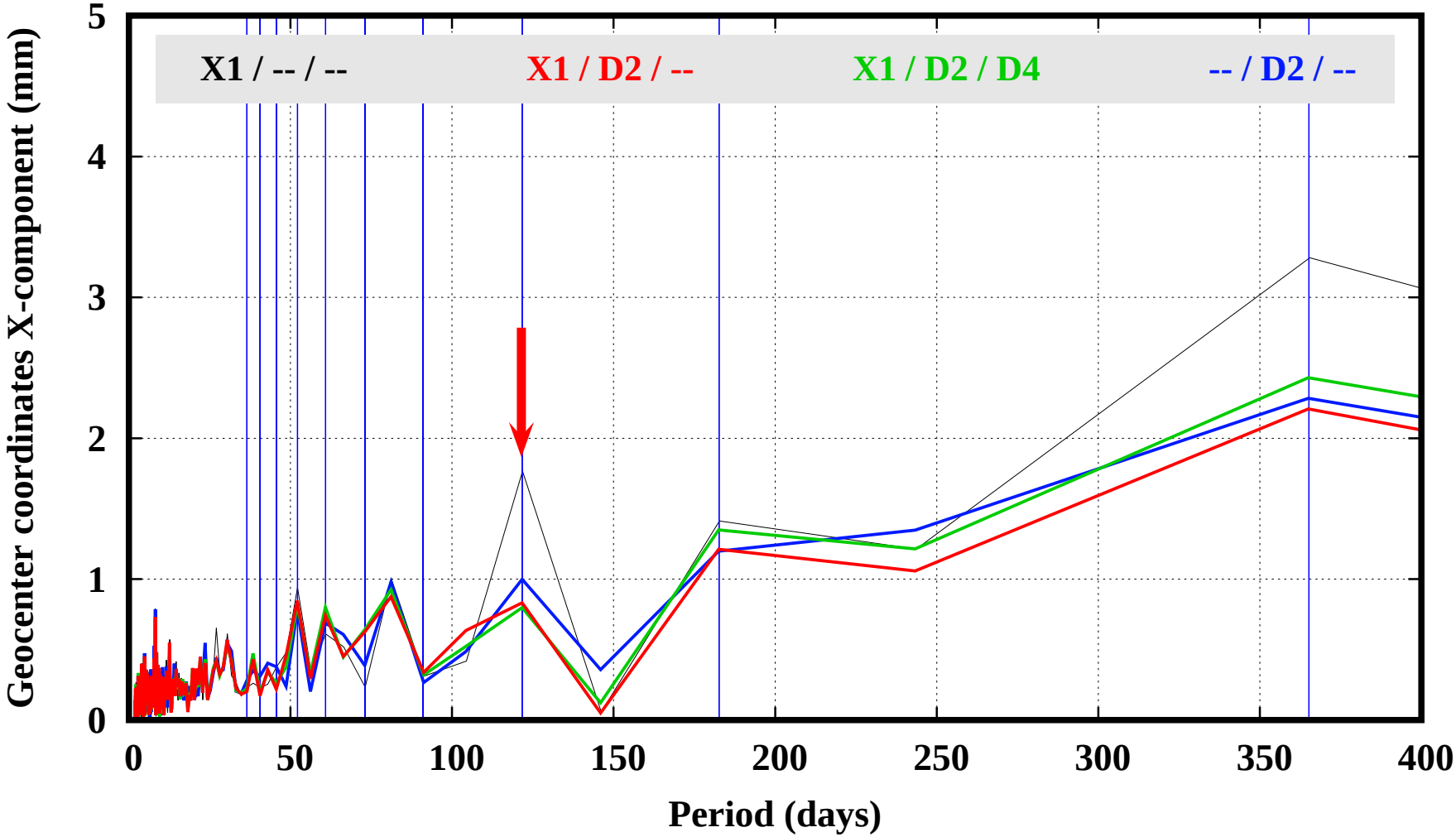

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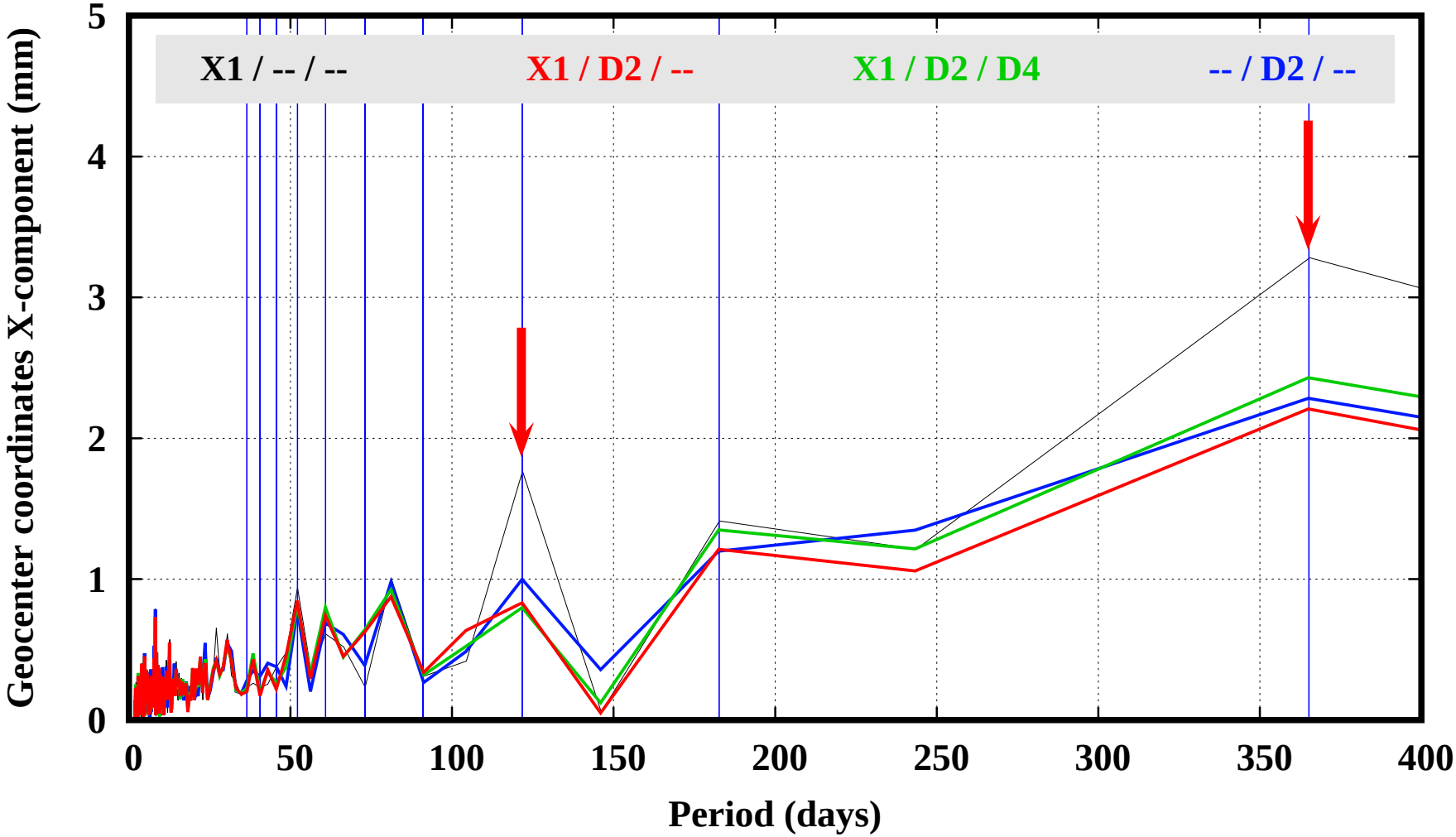

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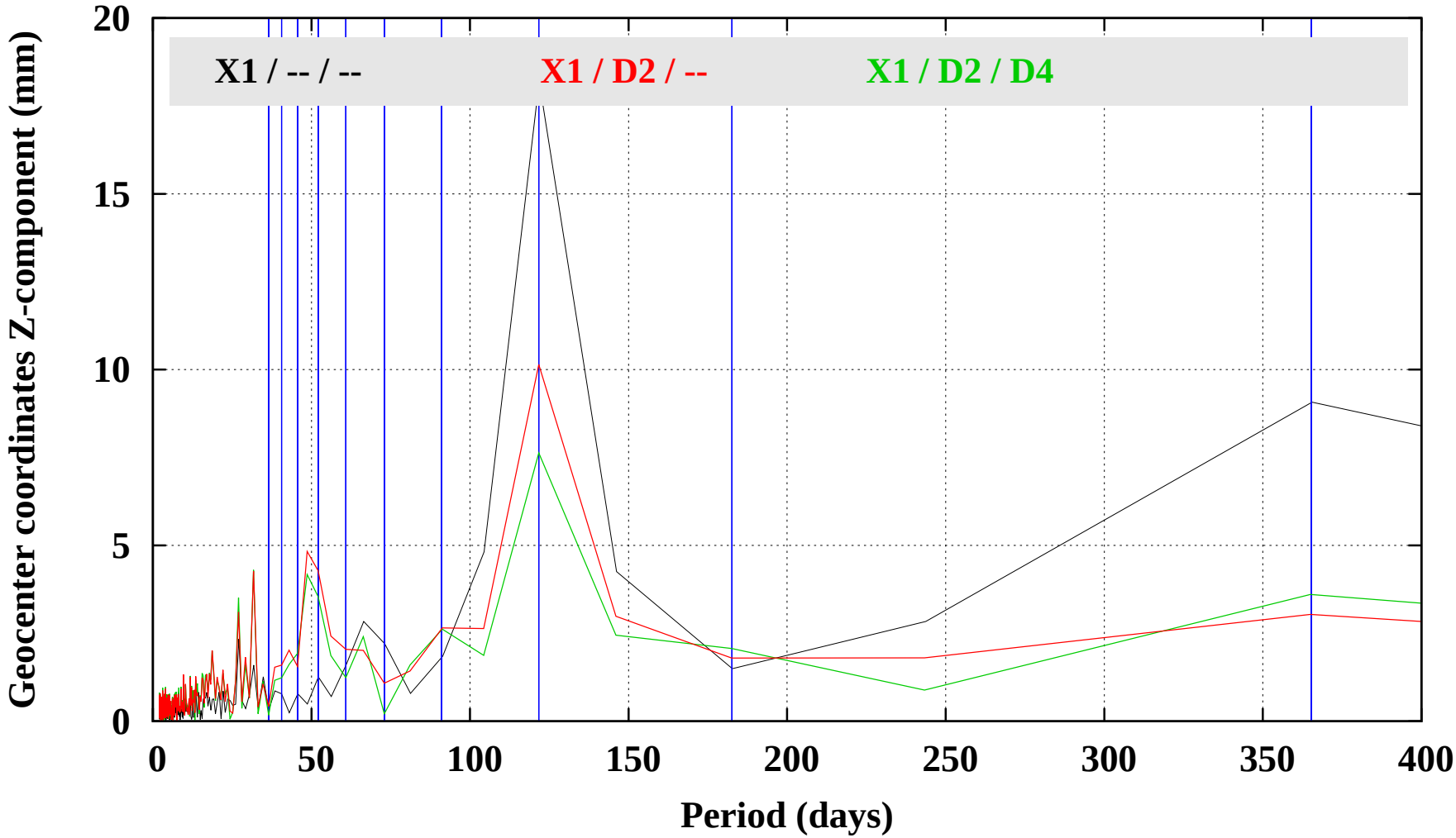
Spectra from geocenter estimates: Z component



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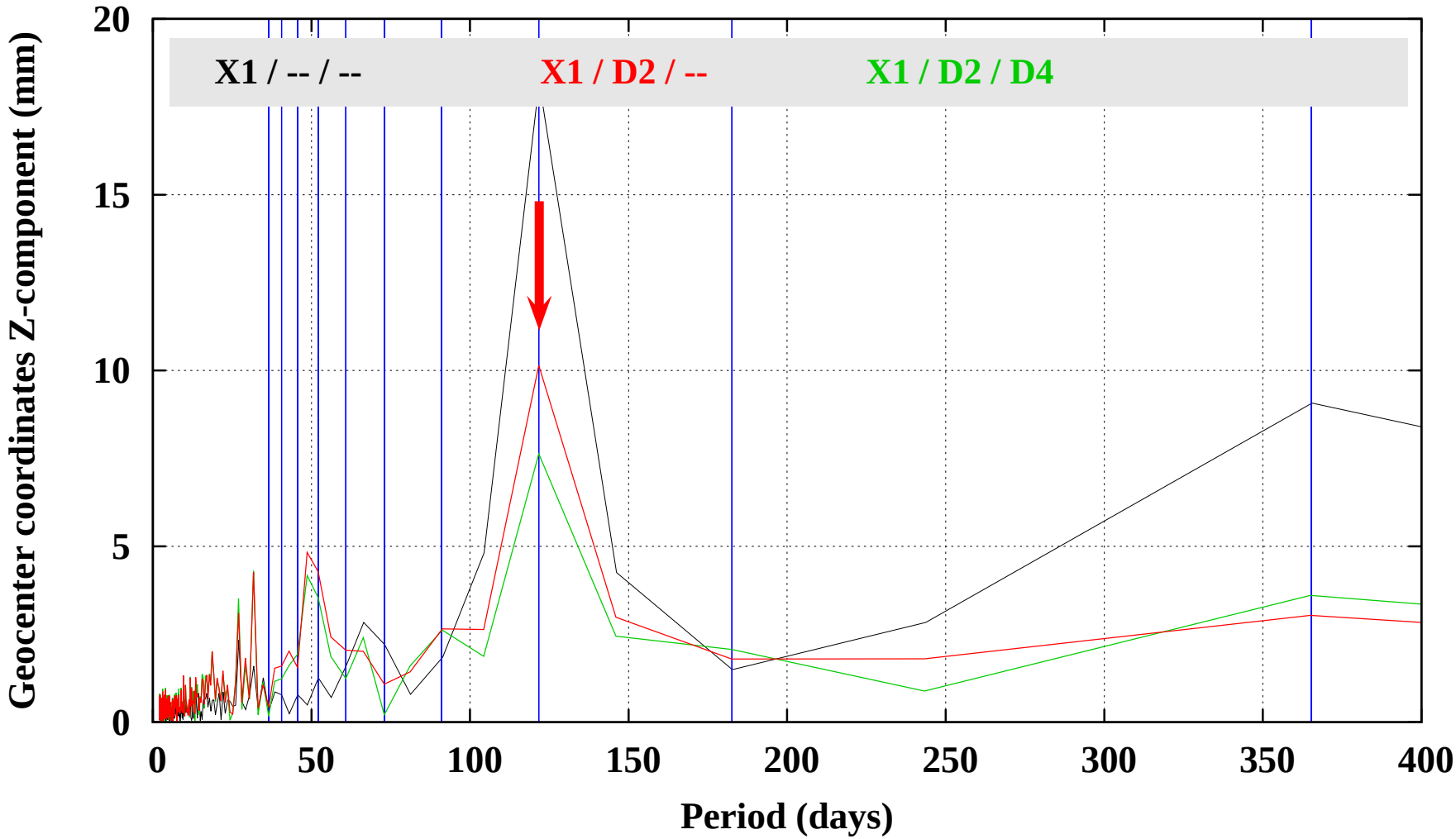
Spectra from geocenter estimates: Z component



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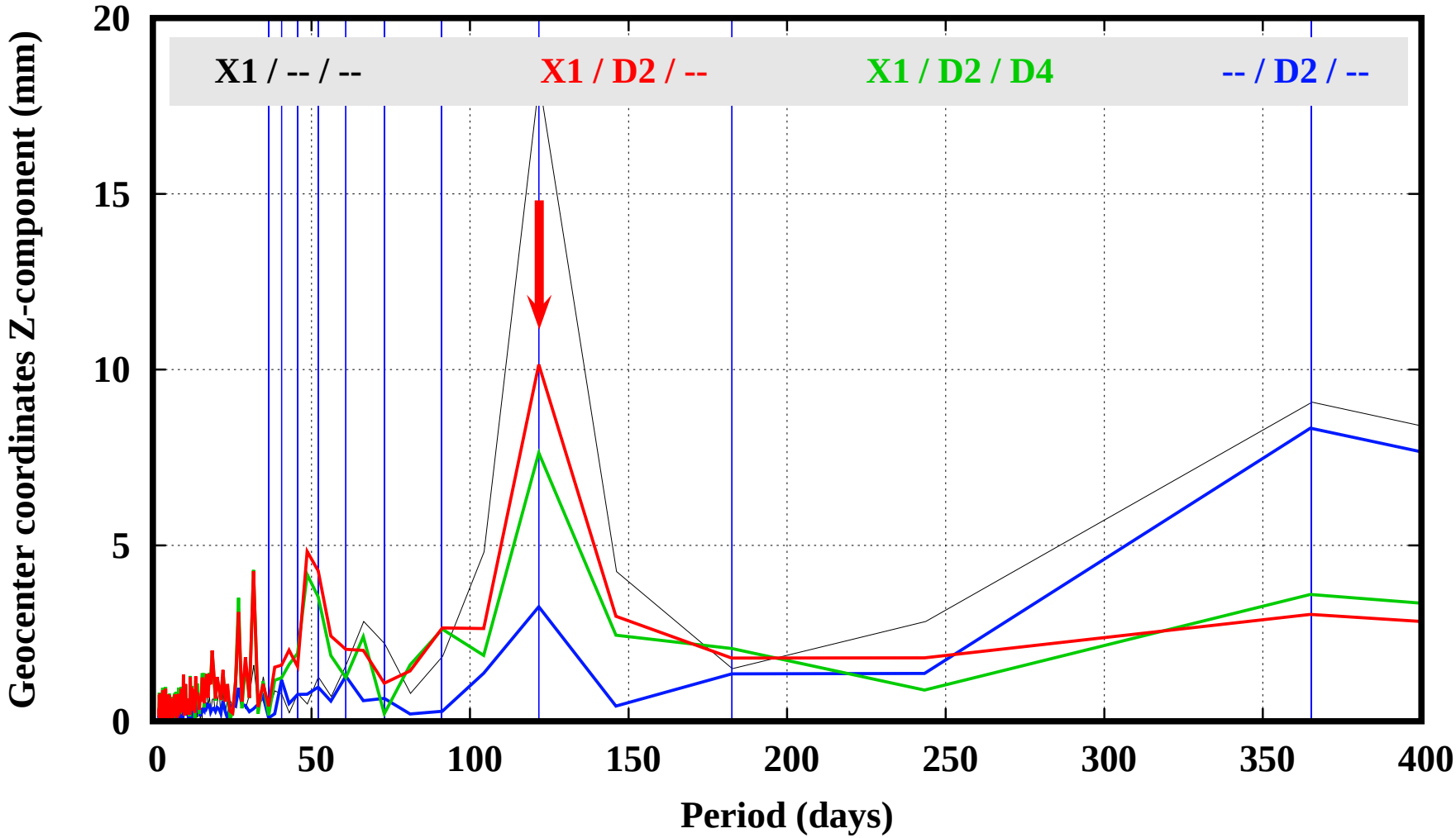
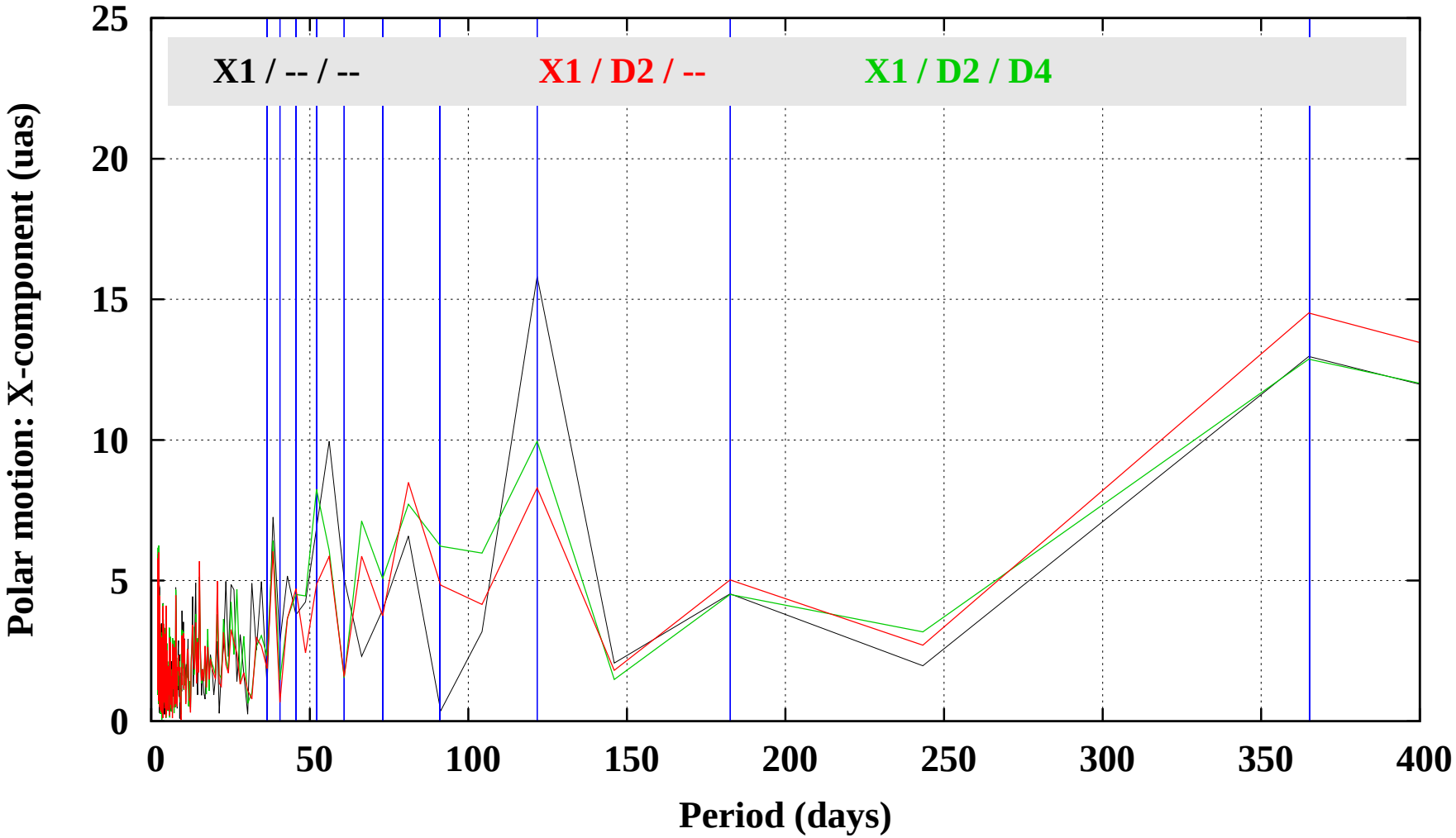


Impact on the Earth Rotation Parameters

Spectra from ERP solution: Polar motion – X



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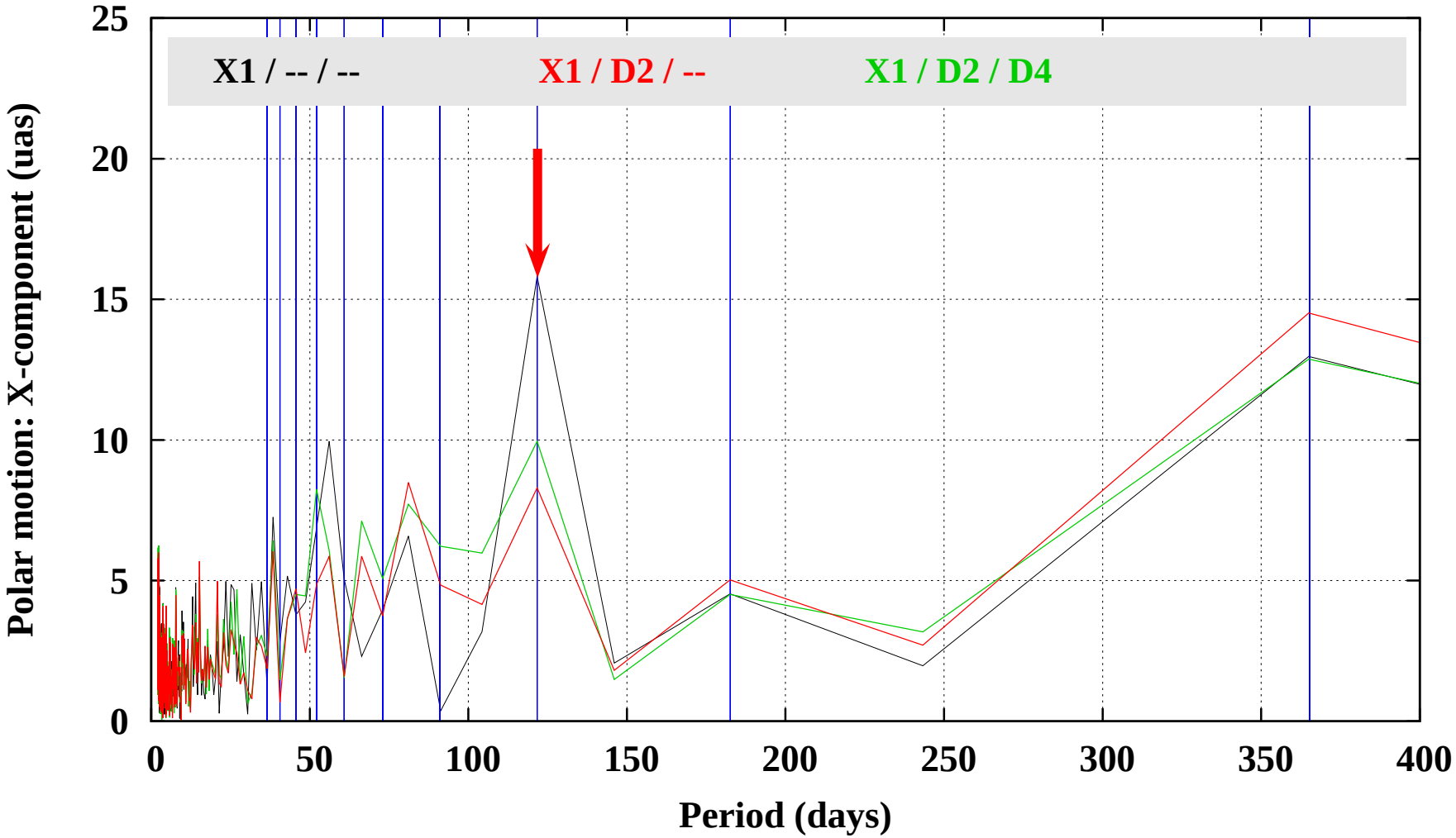

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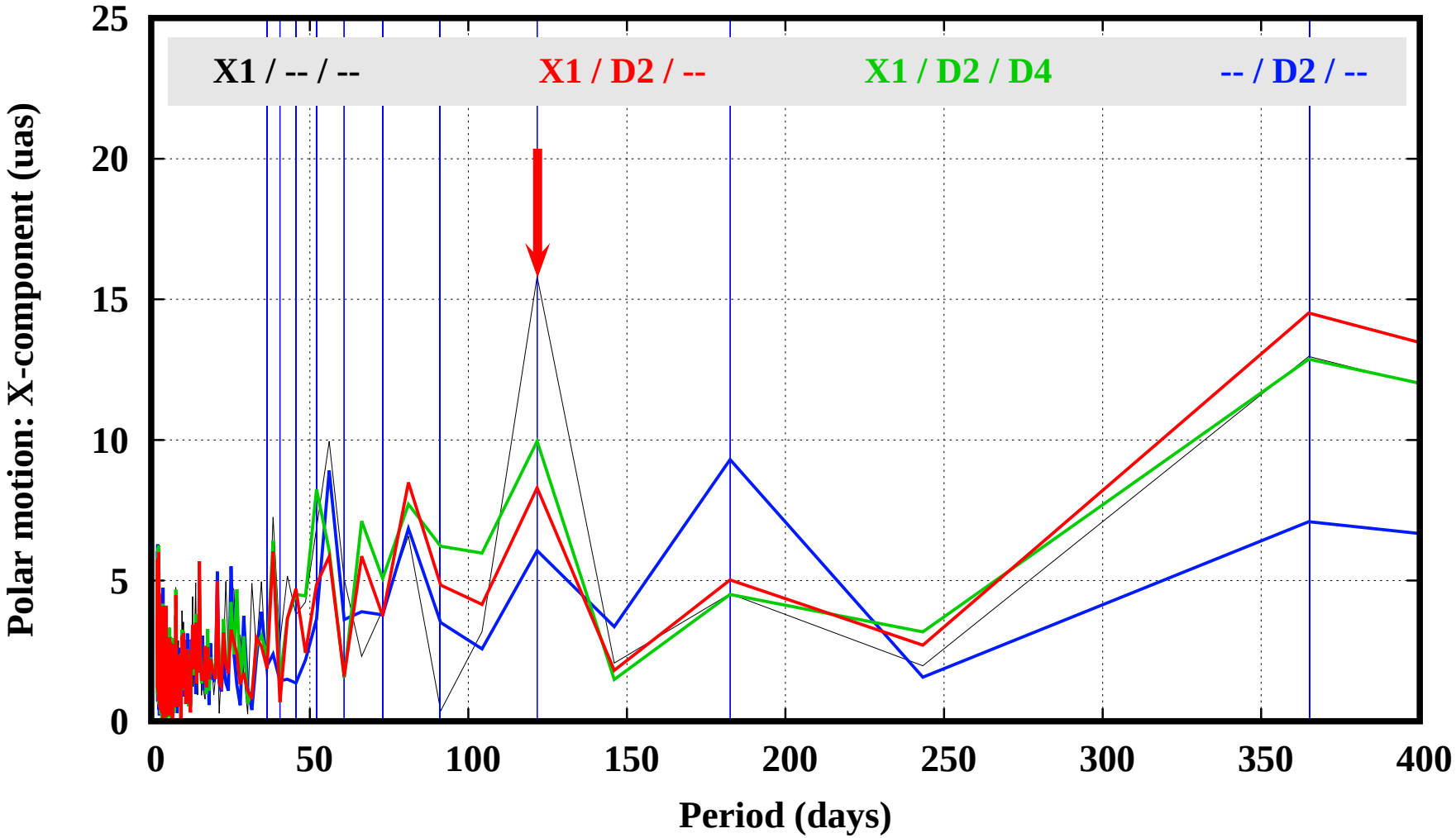

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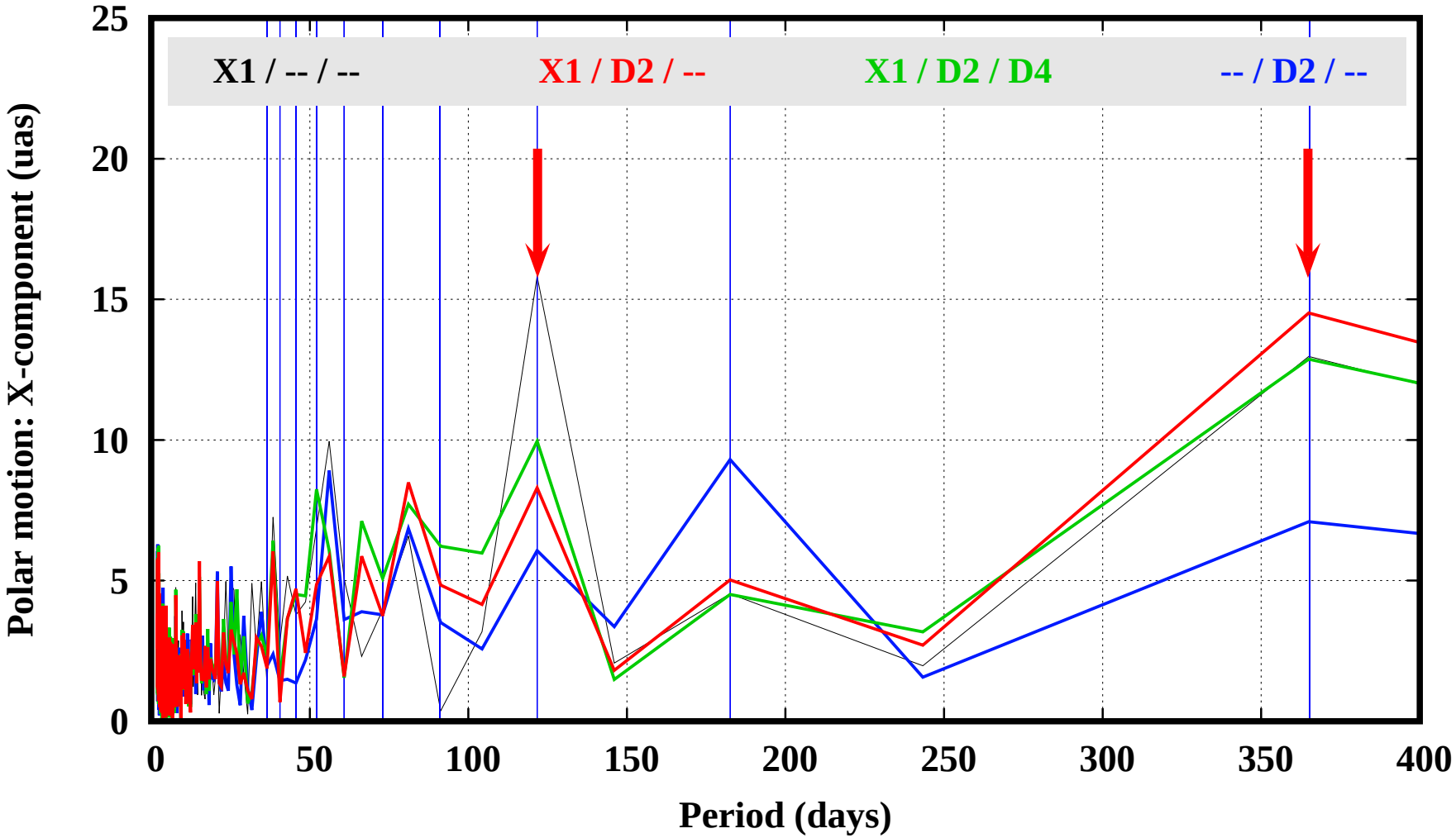

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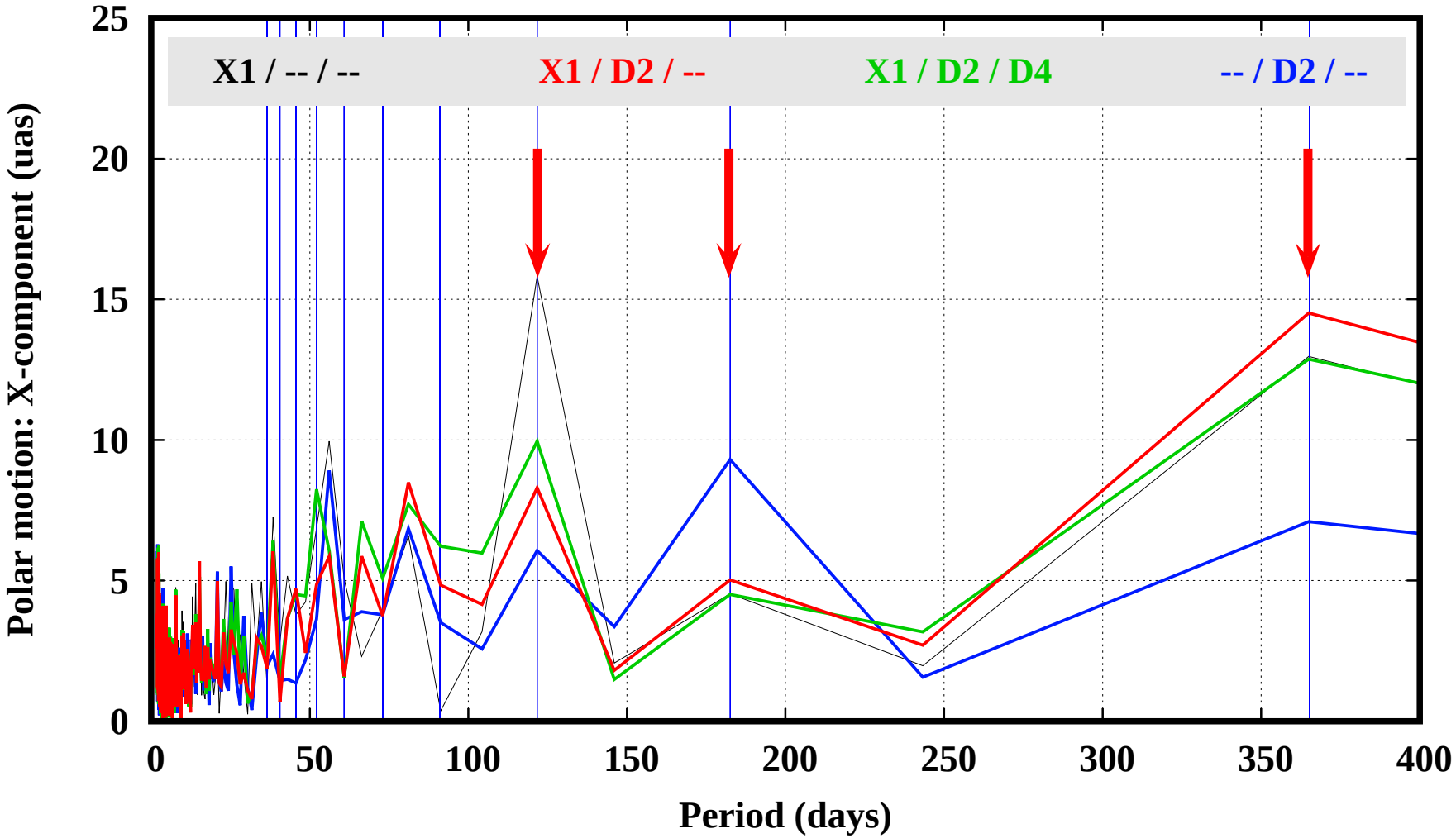

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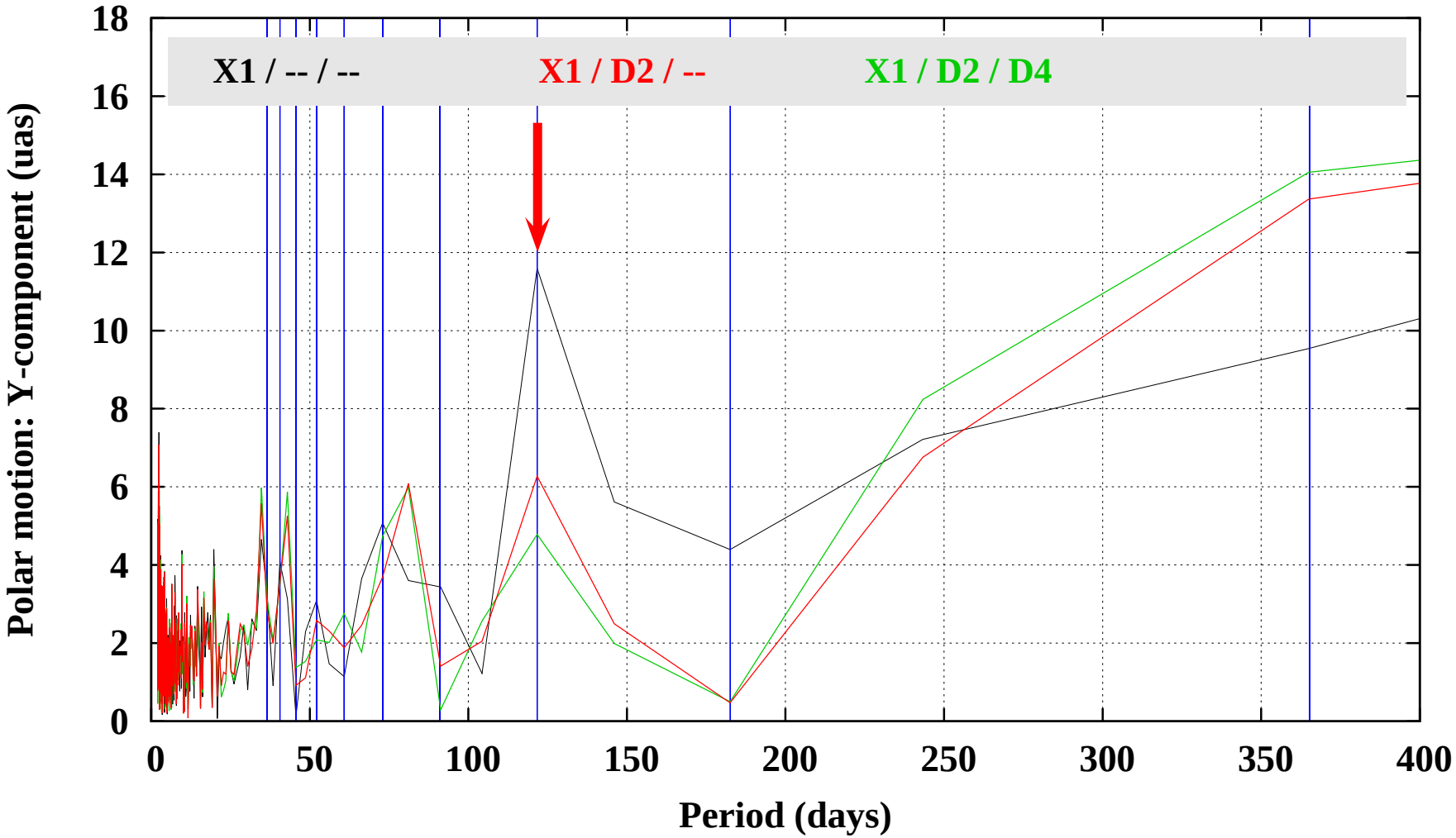

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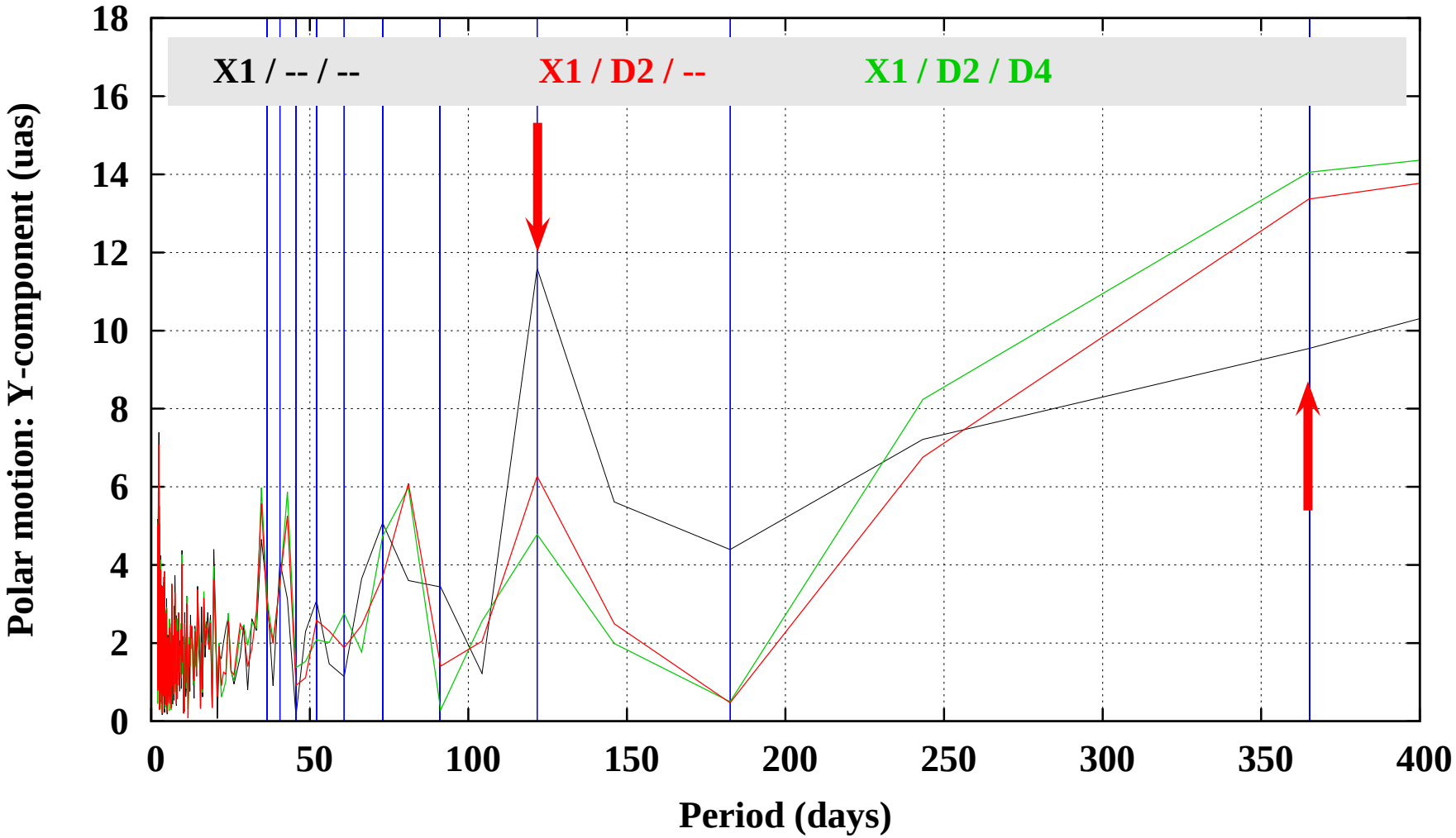

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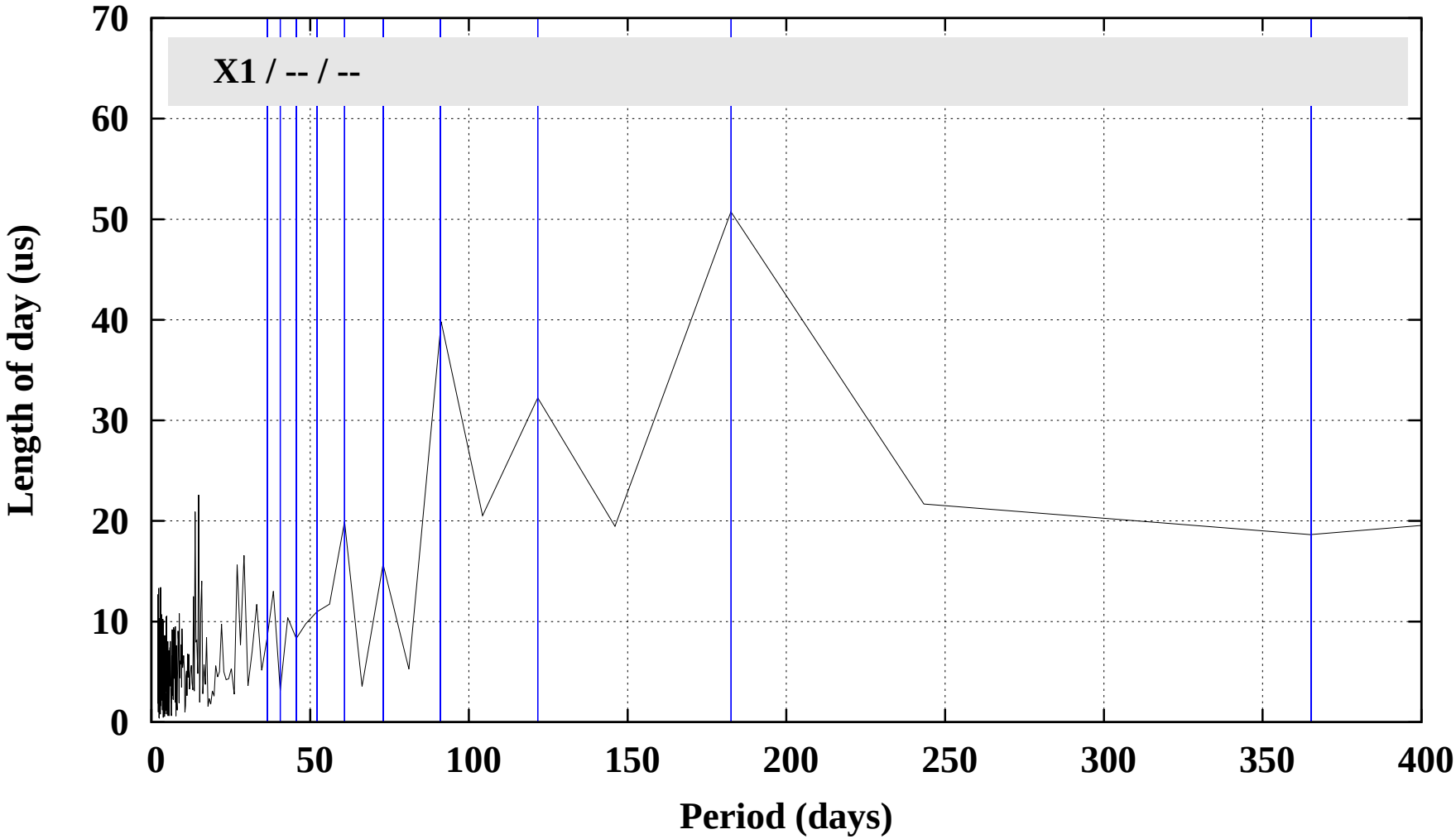
Spectra from ERP solution: length of day



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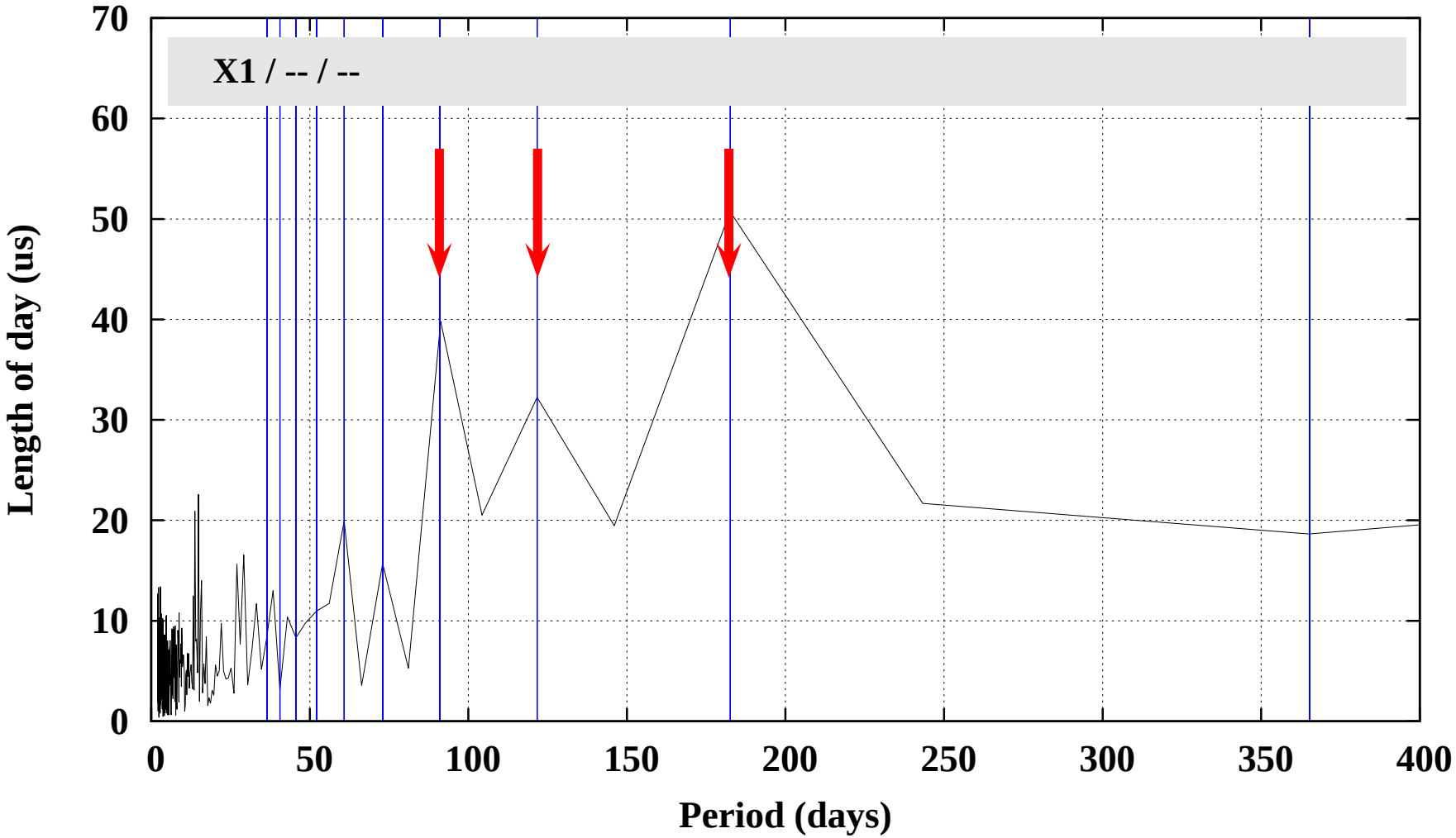

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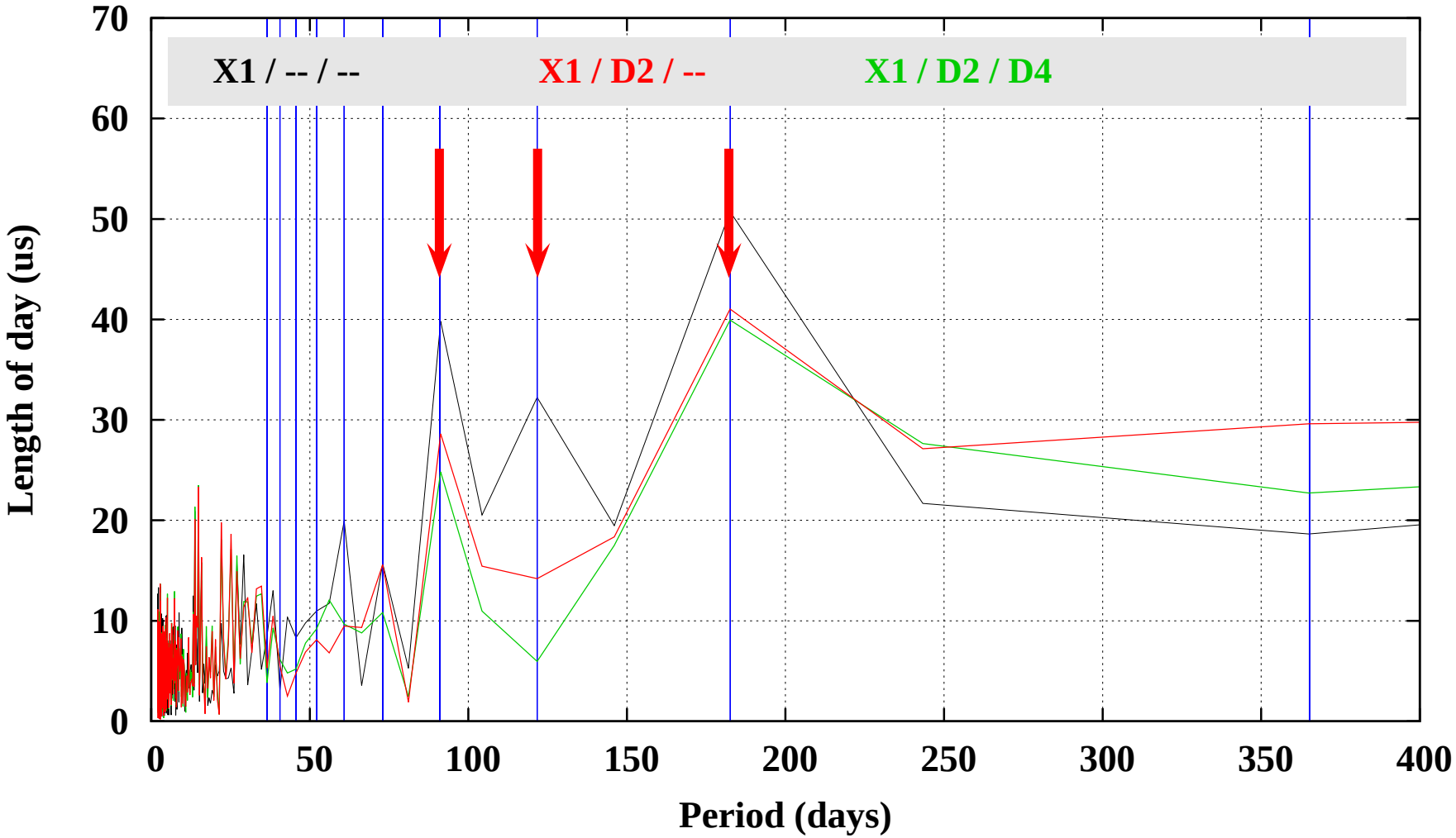

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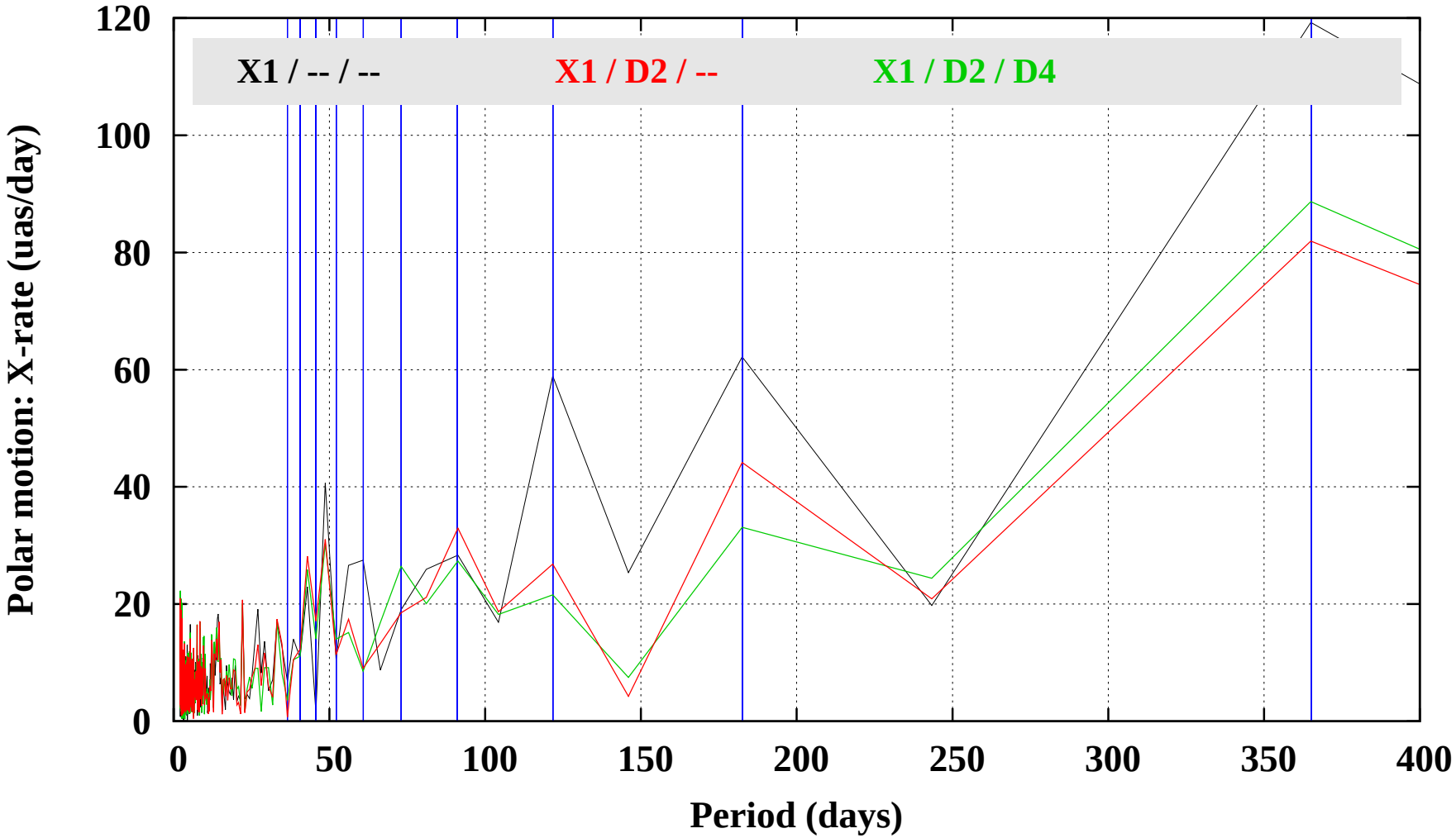

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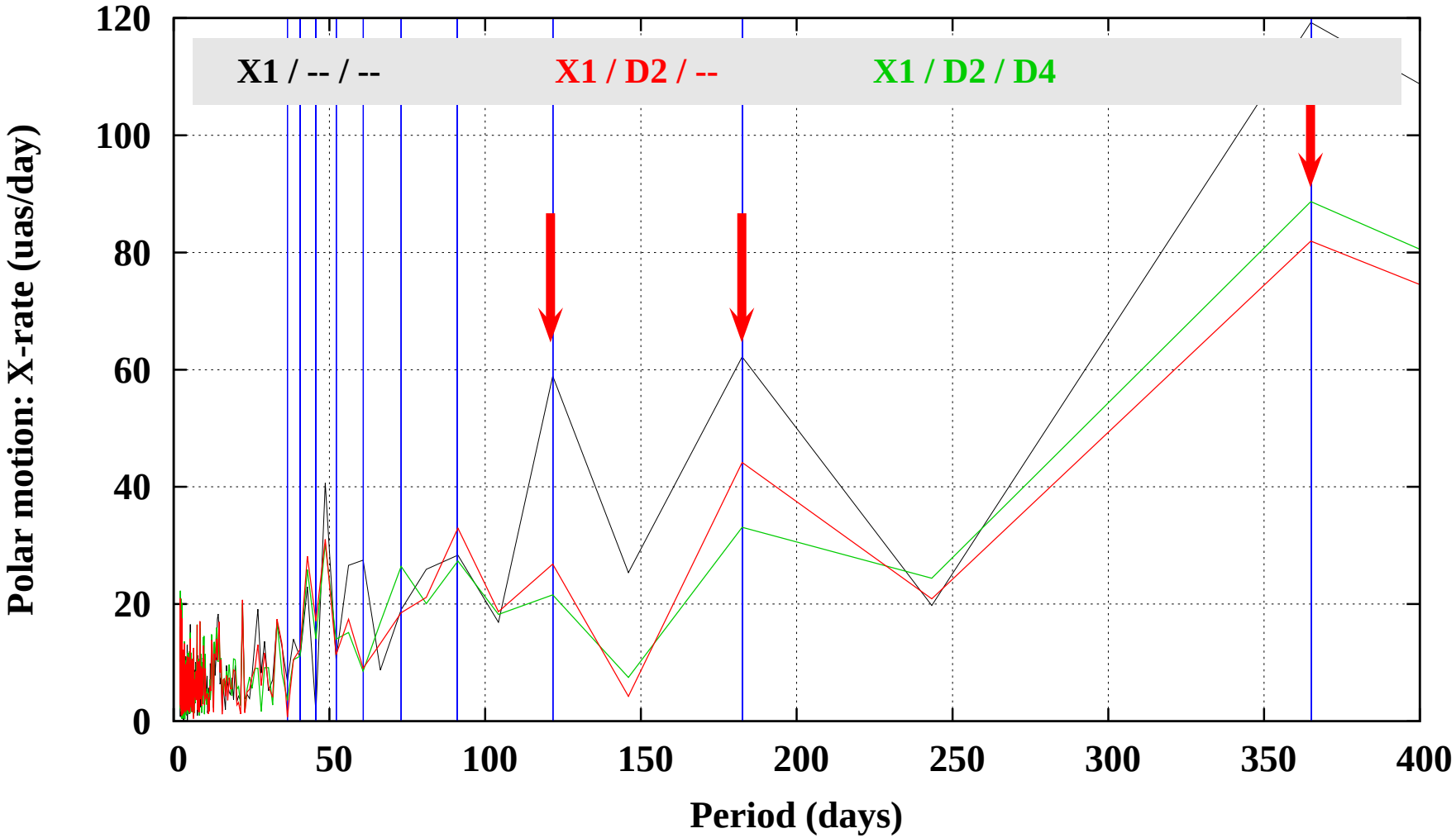

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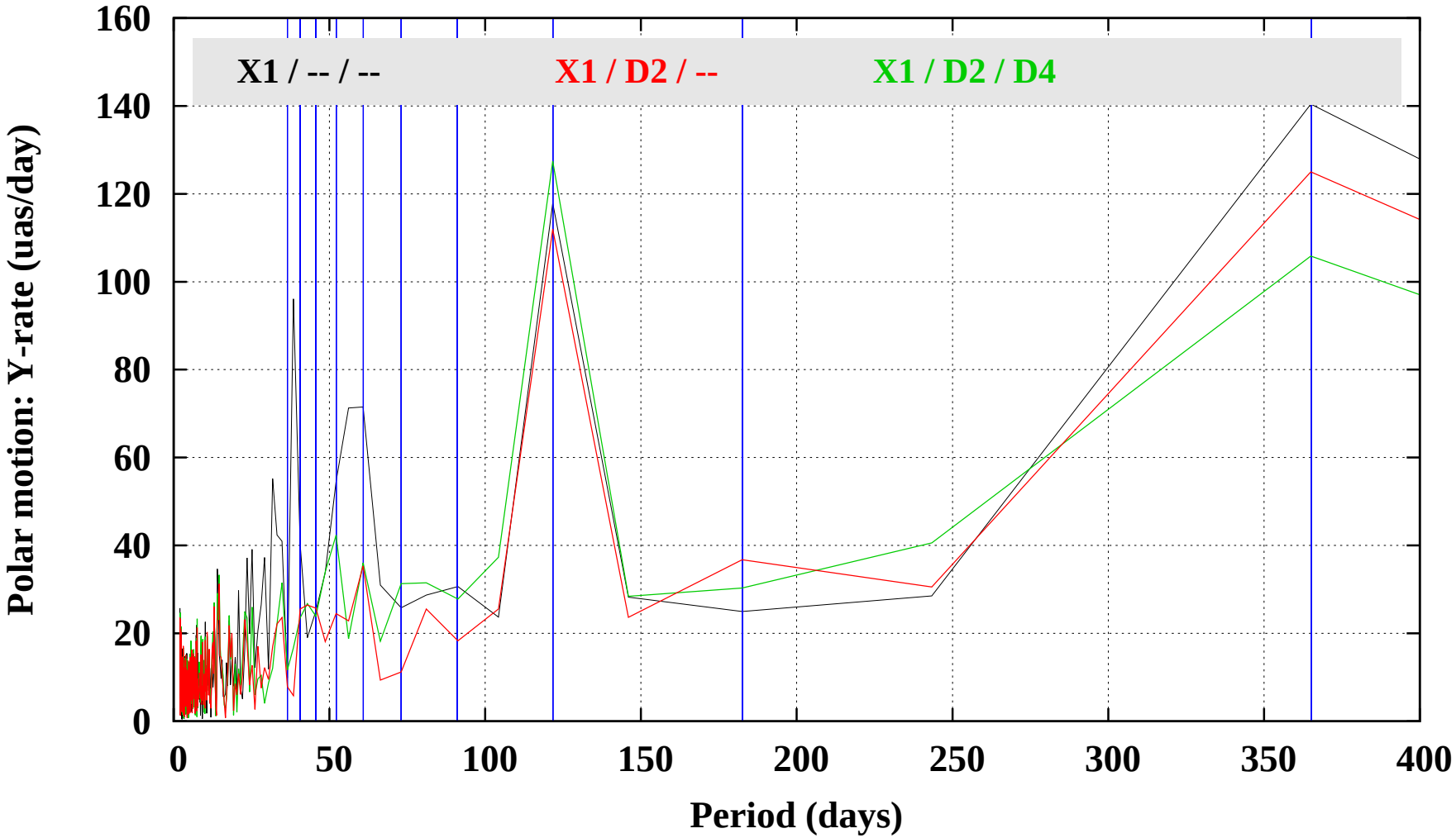

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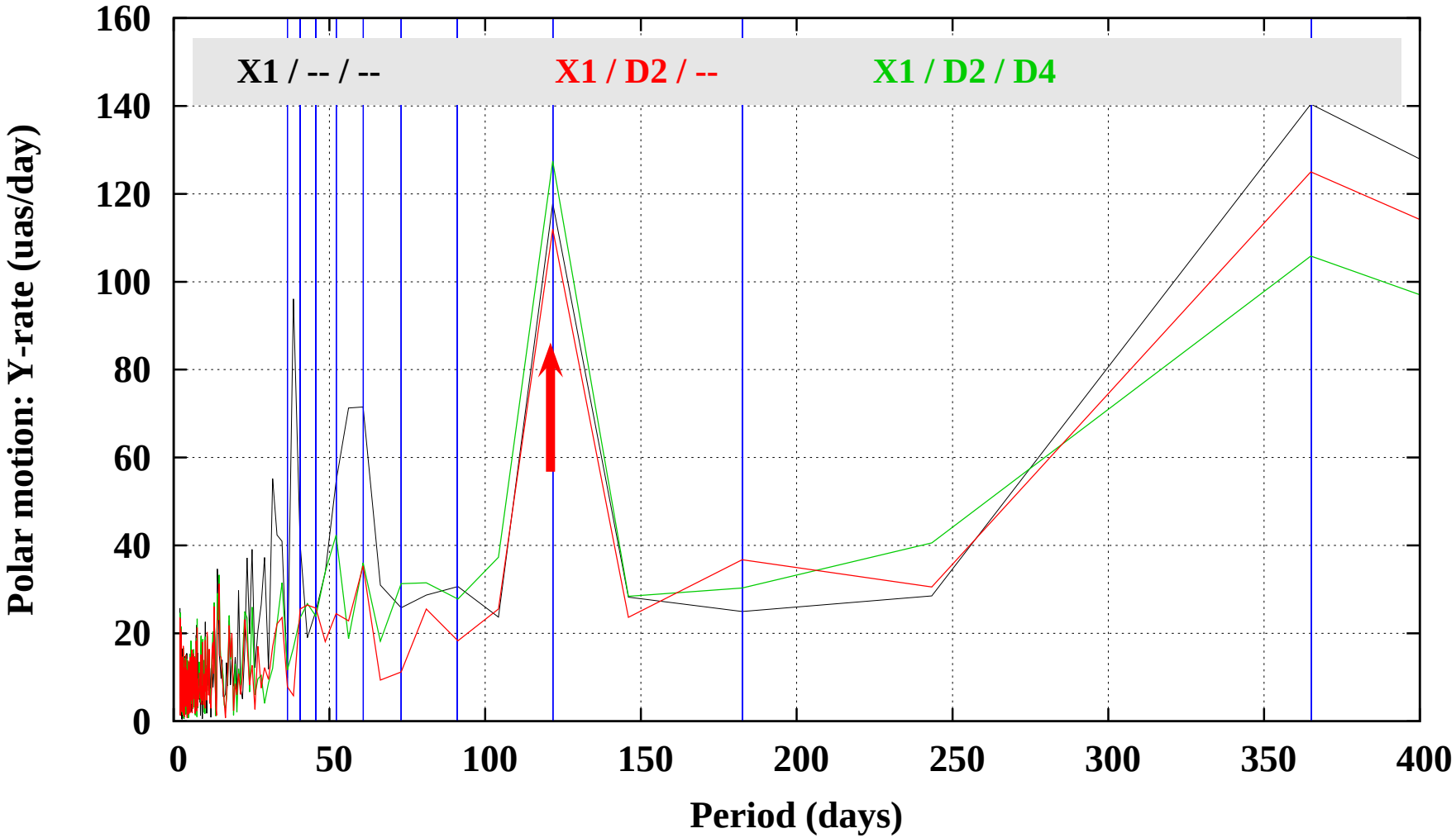

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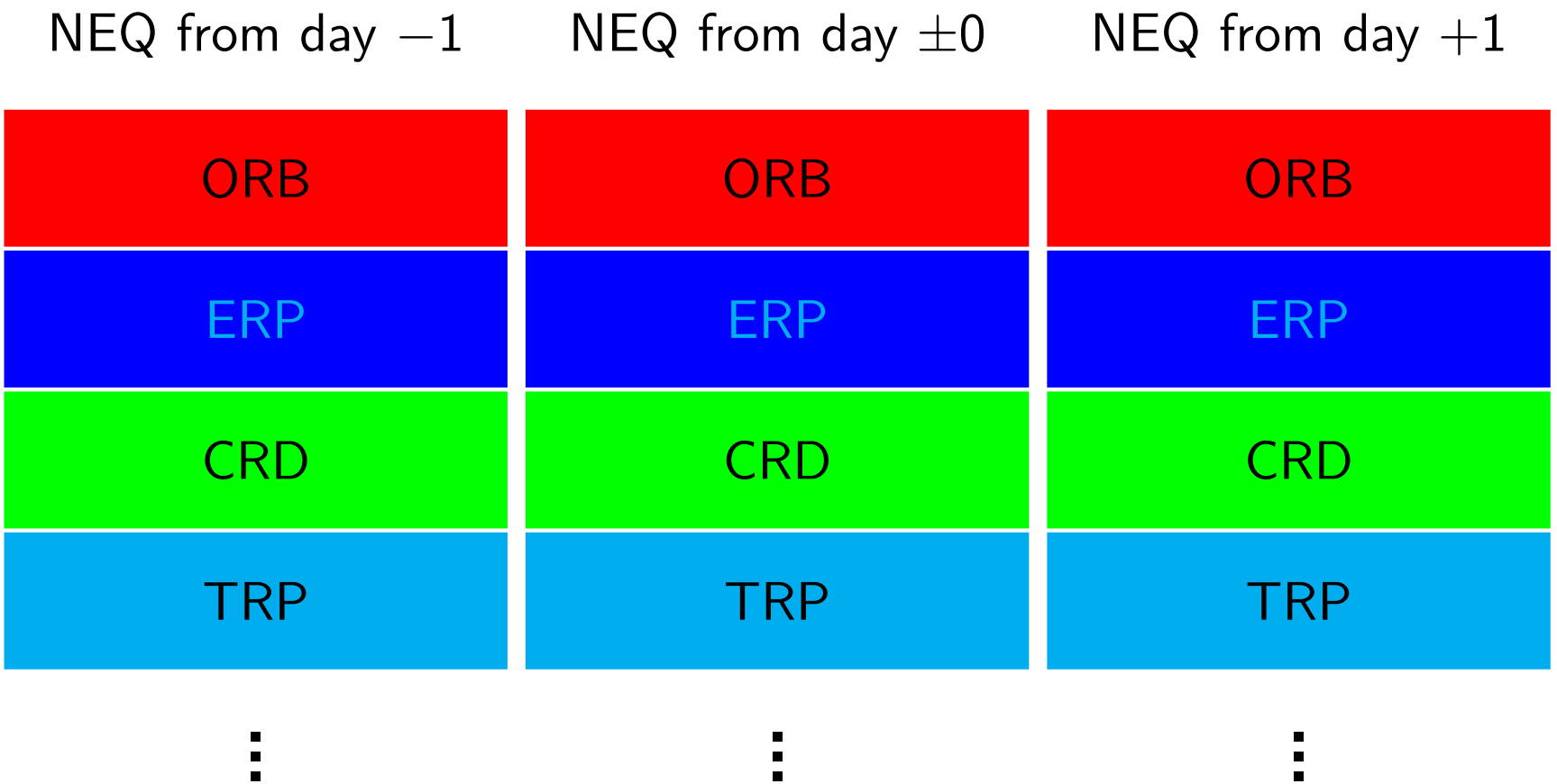
- The most promising orbit parameter setup is: X_1, D_2 (and D_4).

Long–Arc Solutions

Strategy for the long-arc solution

Classical approach to generate three–day solutions at CODE:



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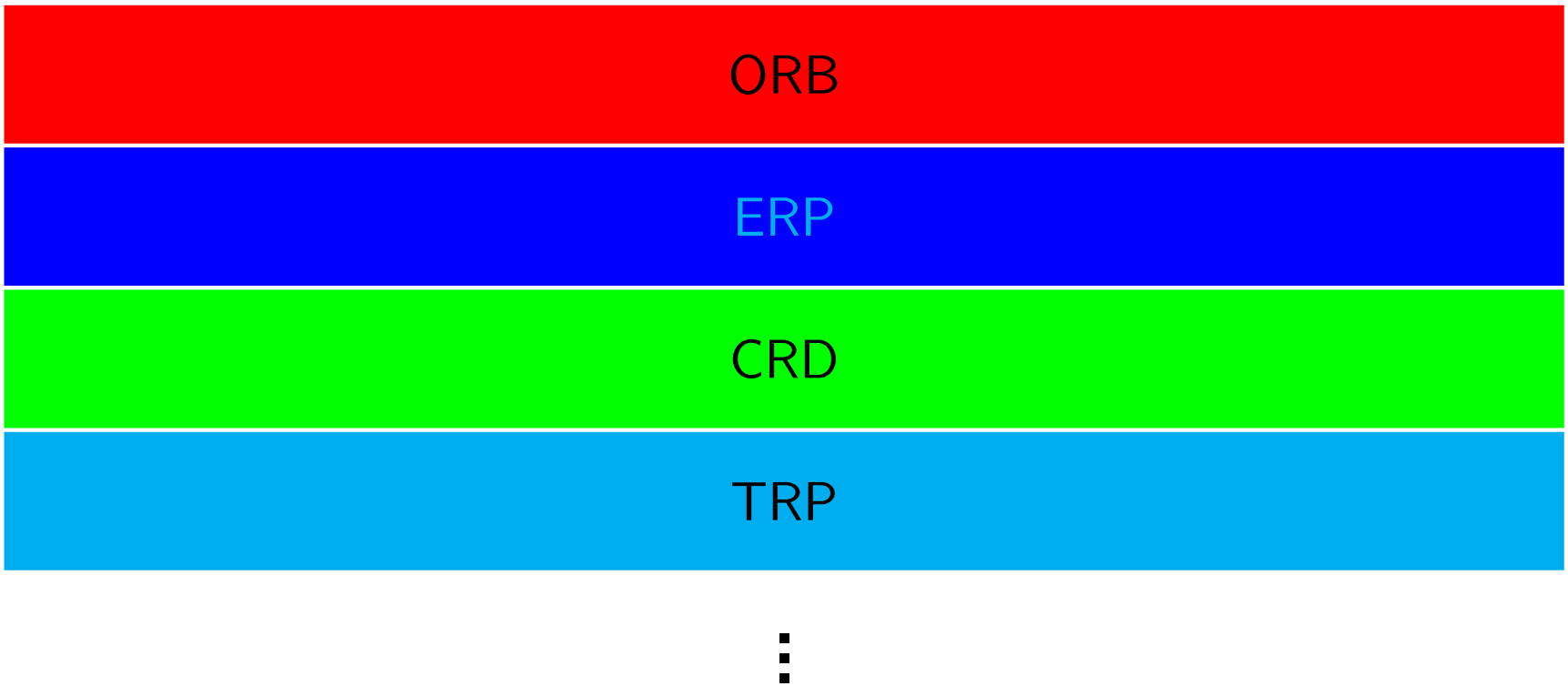

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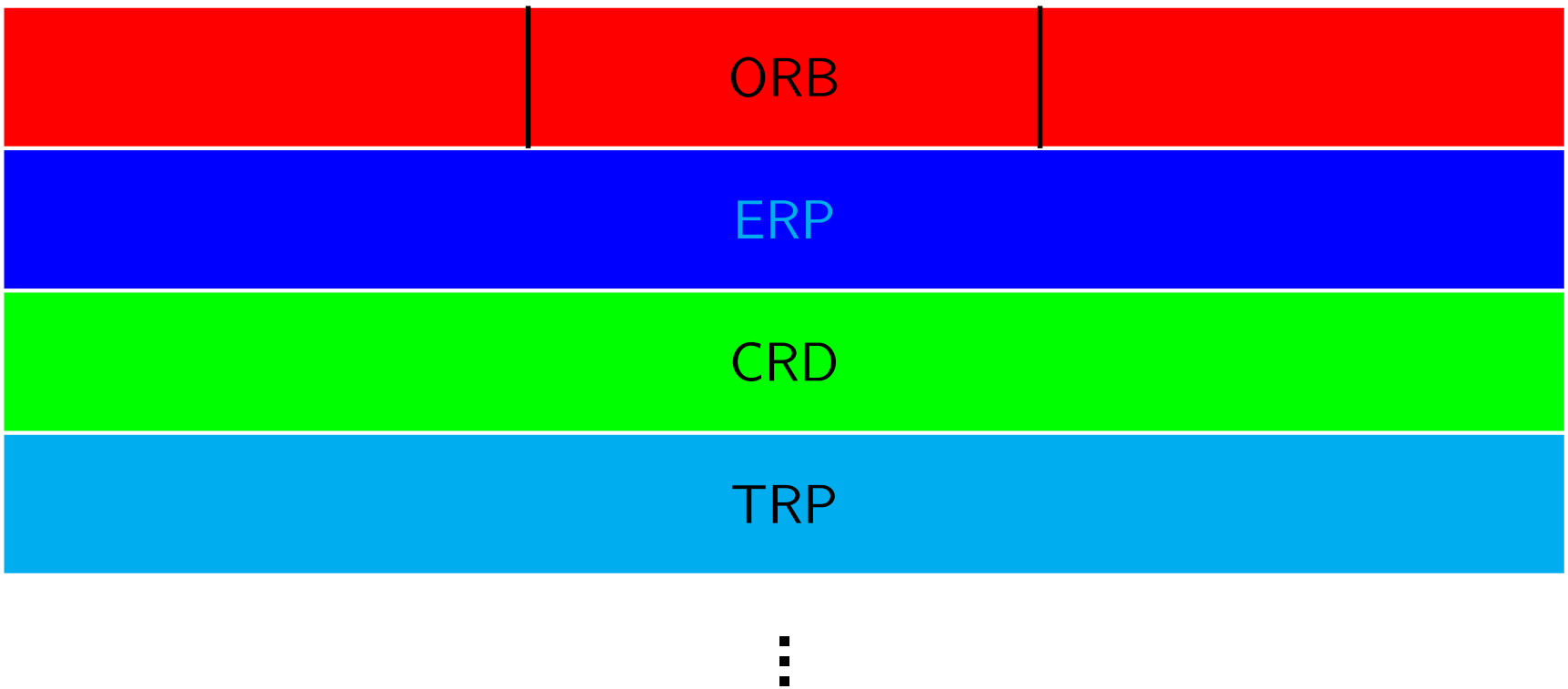

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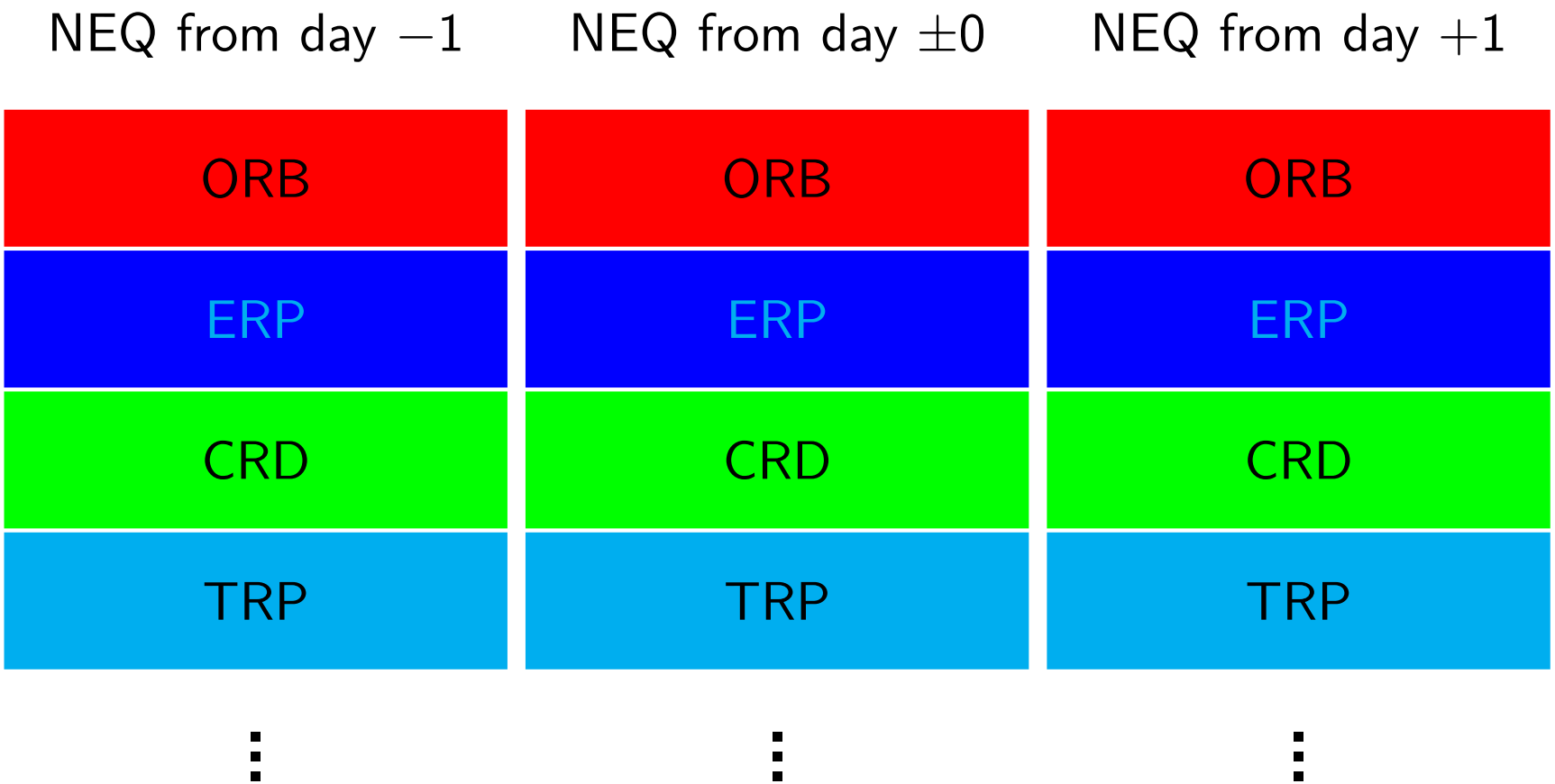

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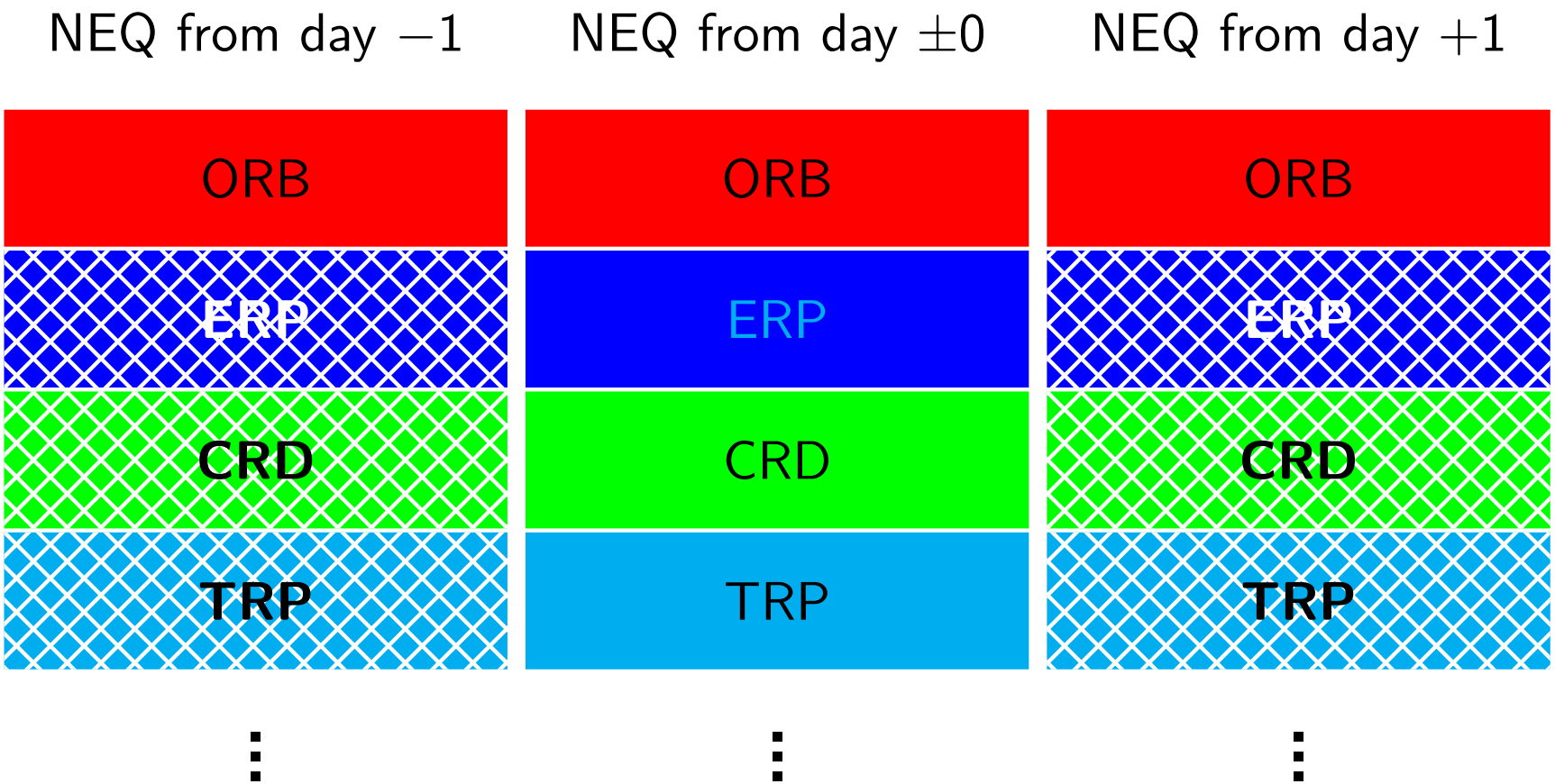

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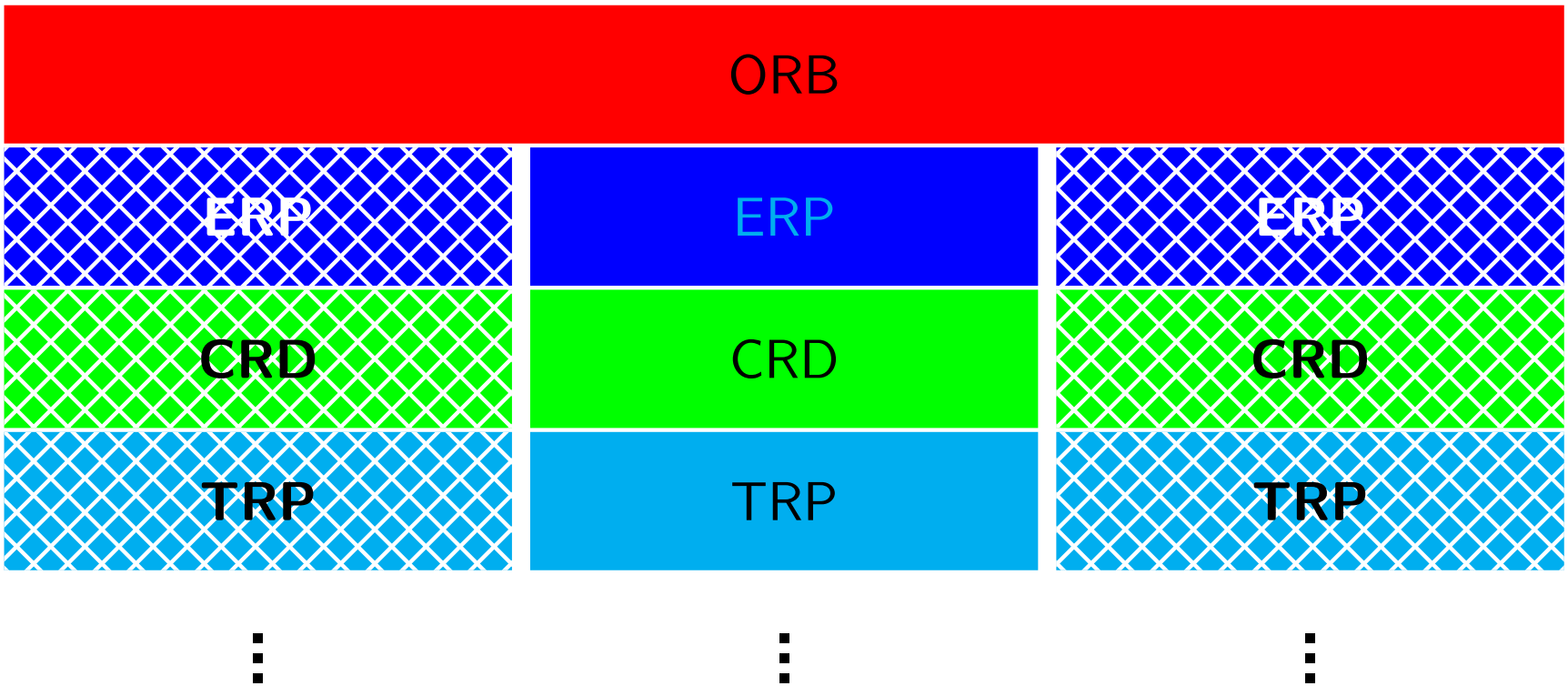

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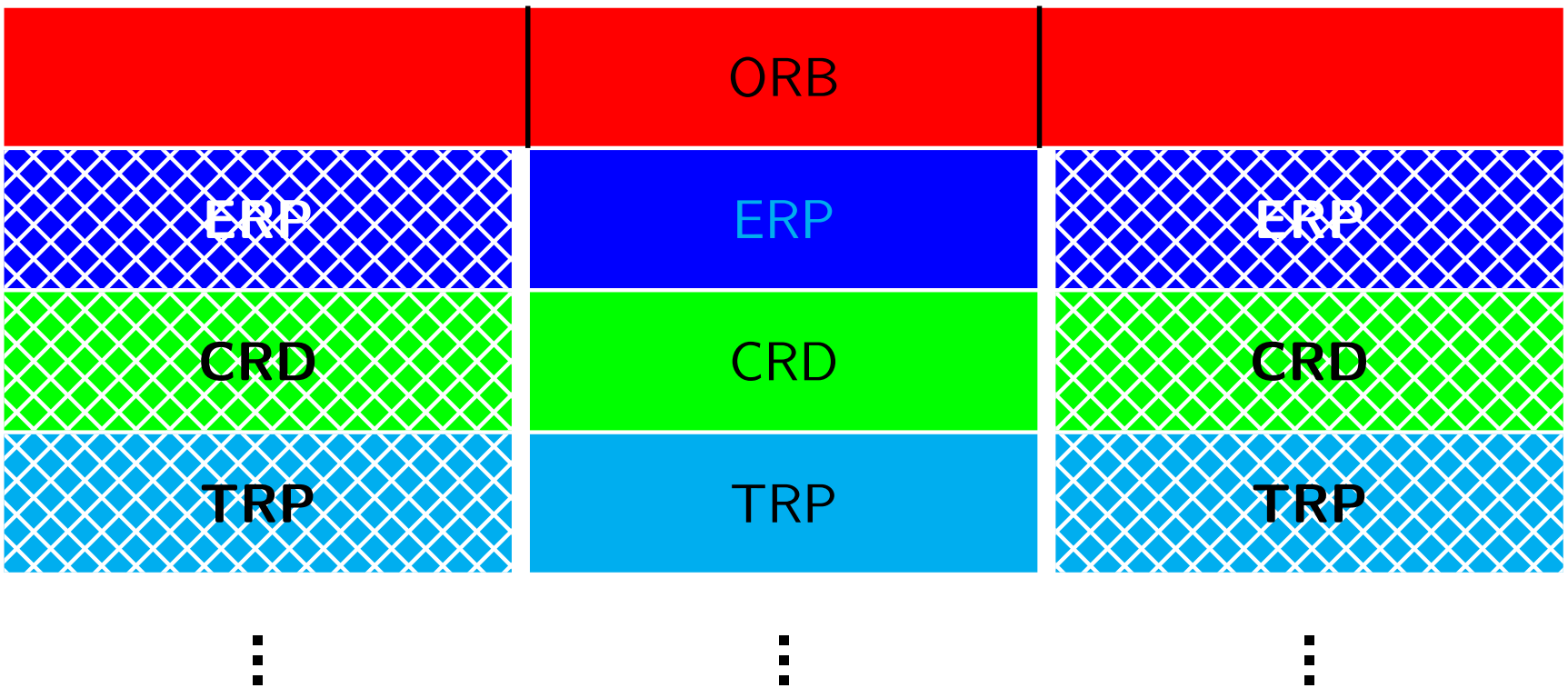

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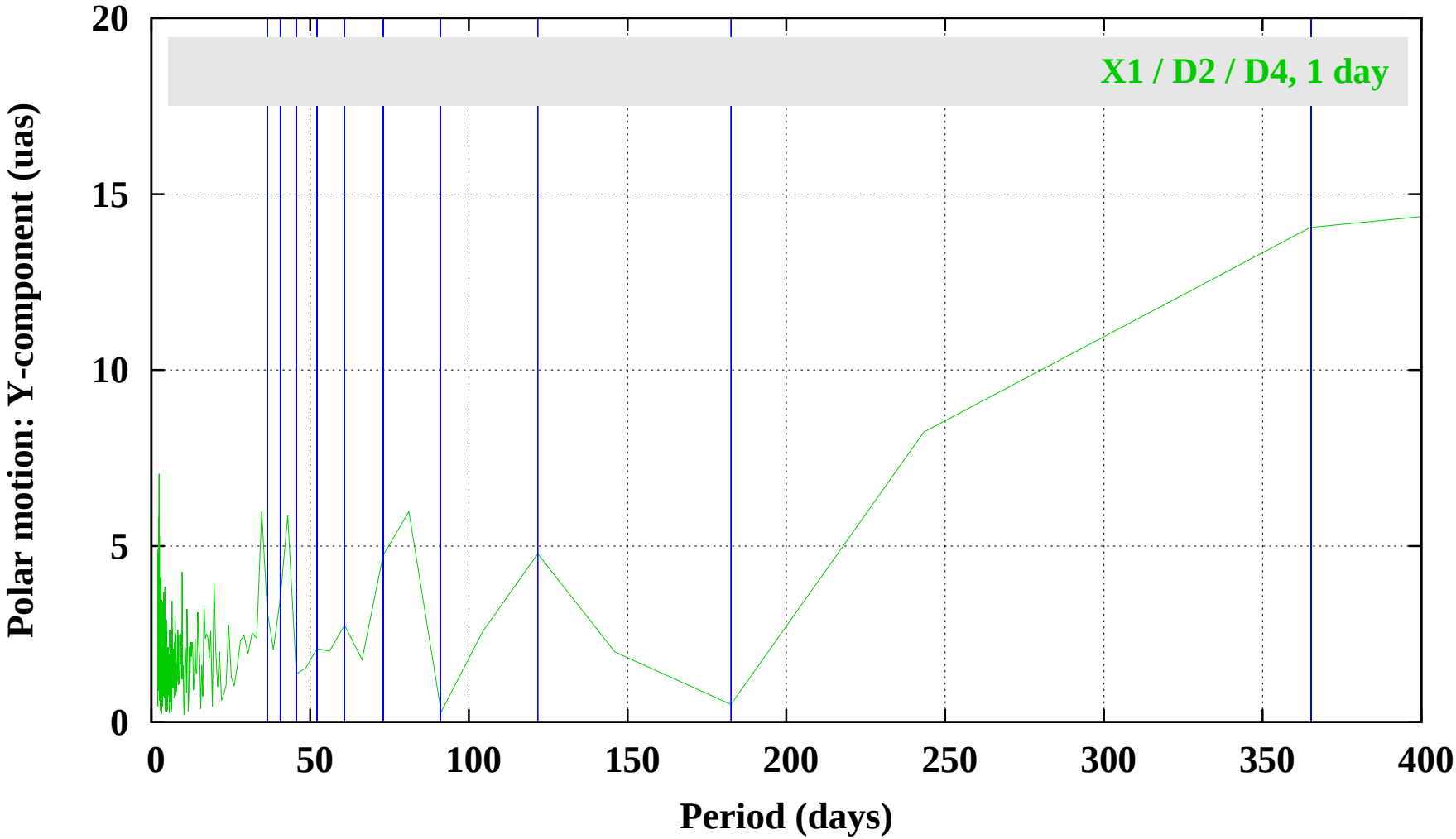

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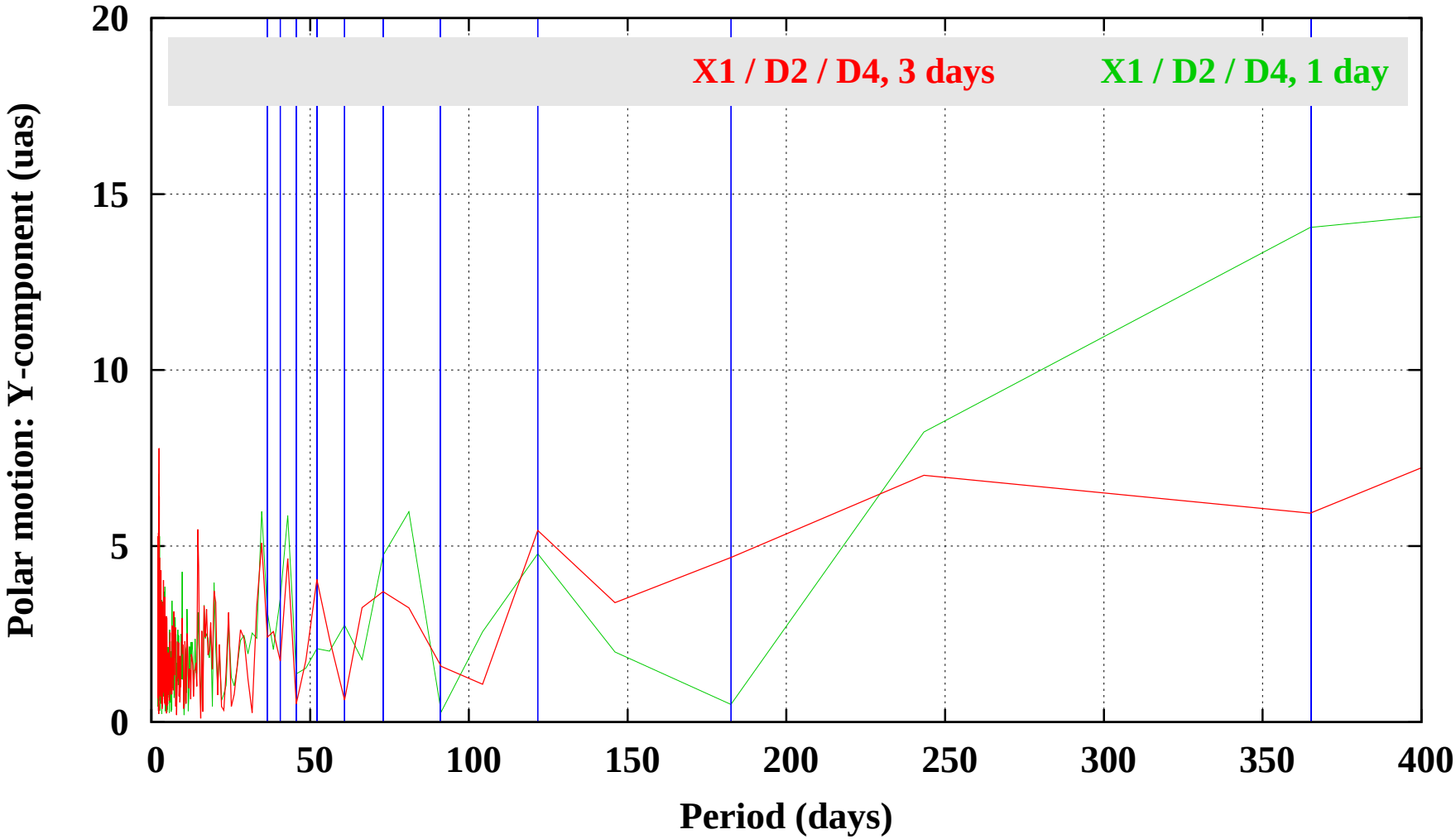

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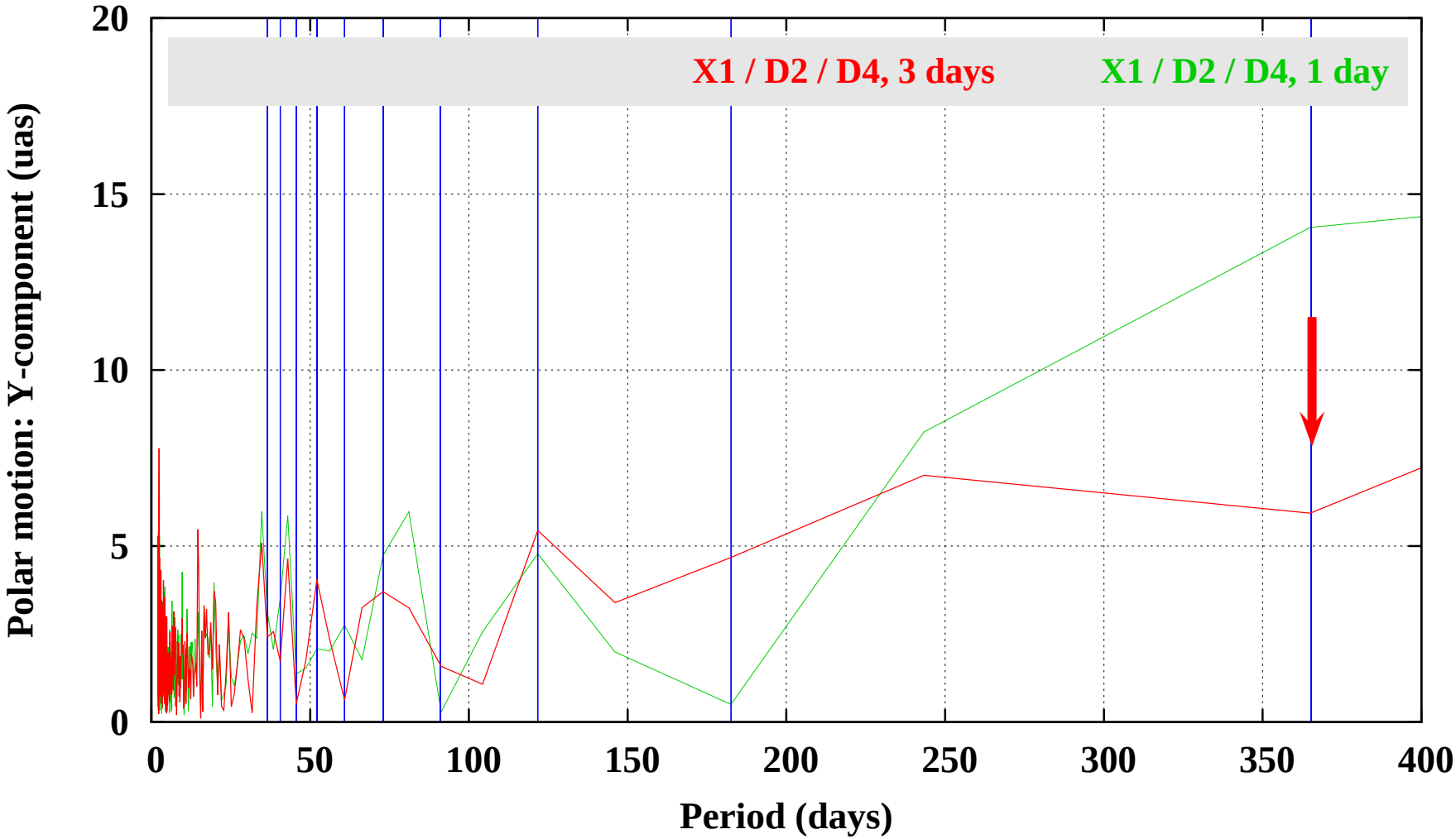

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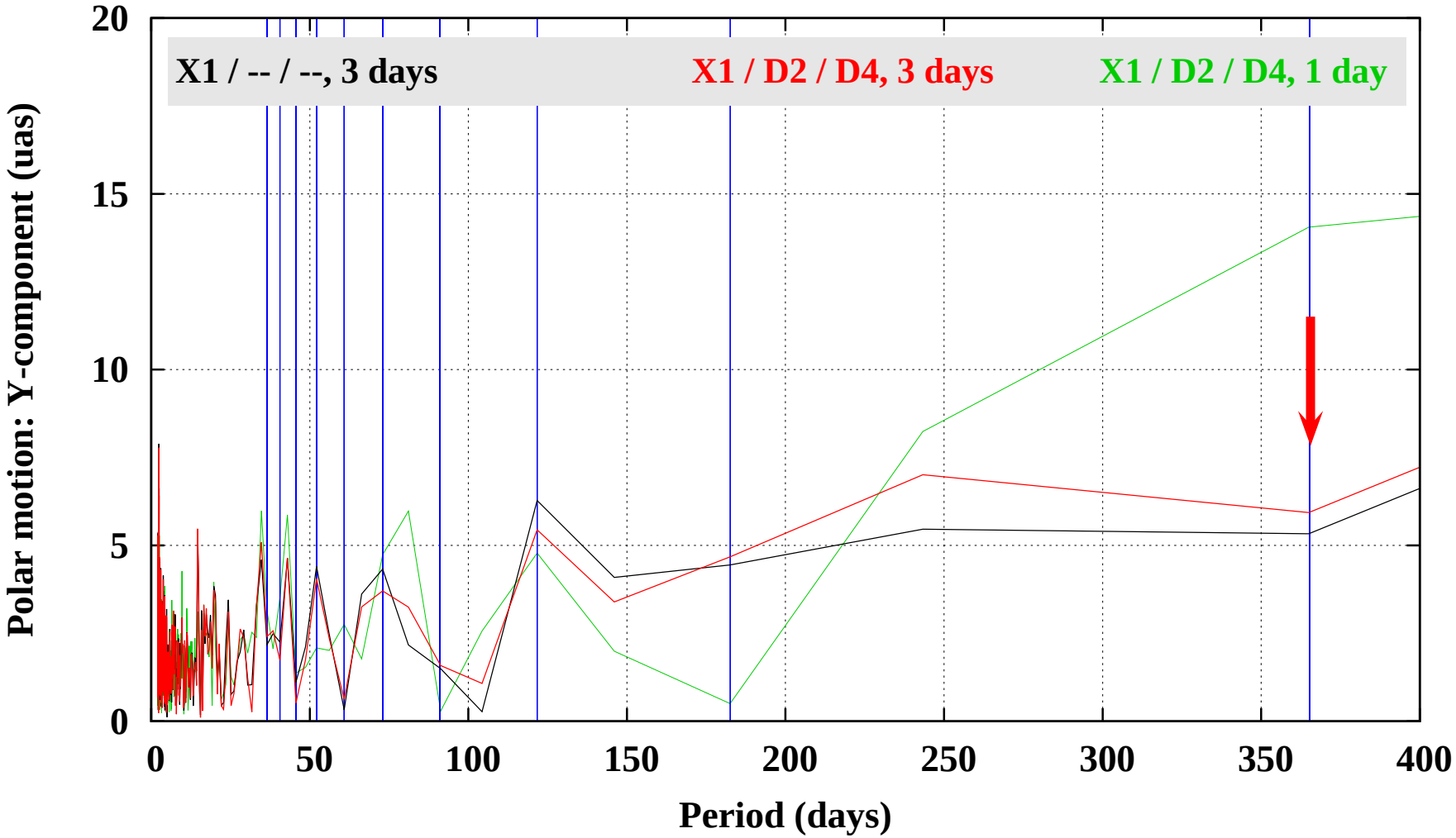

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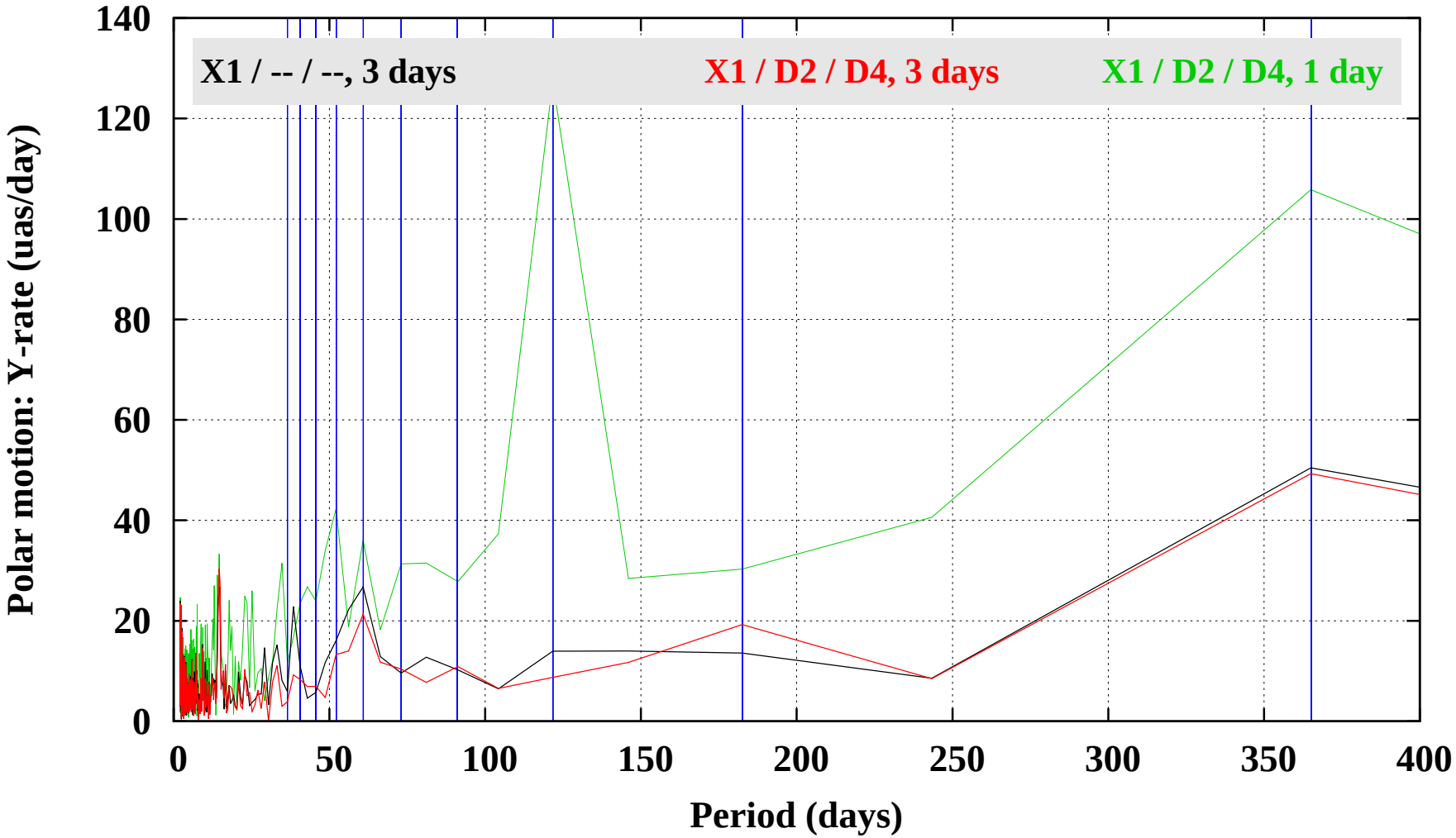

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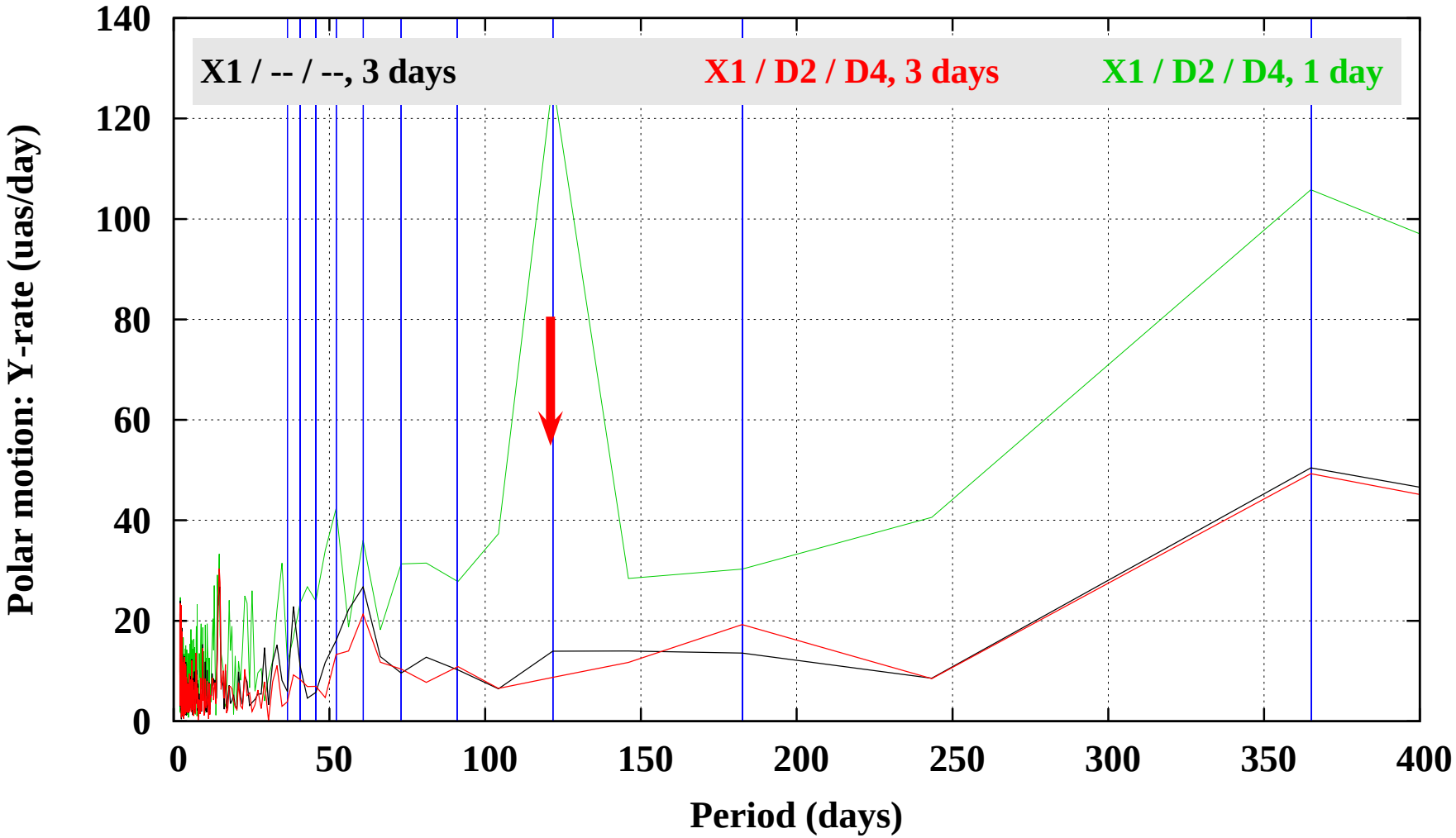

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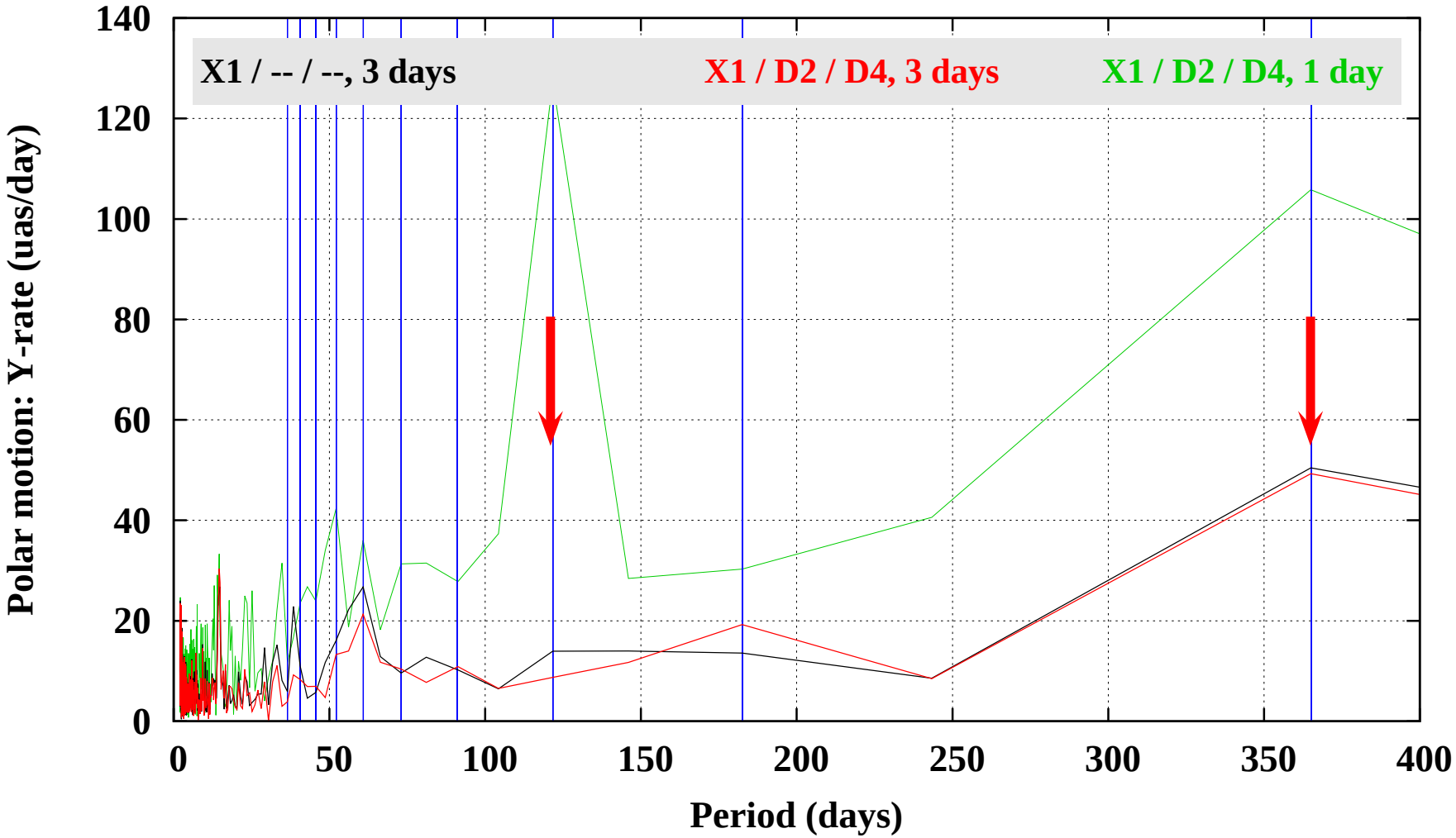

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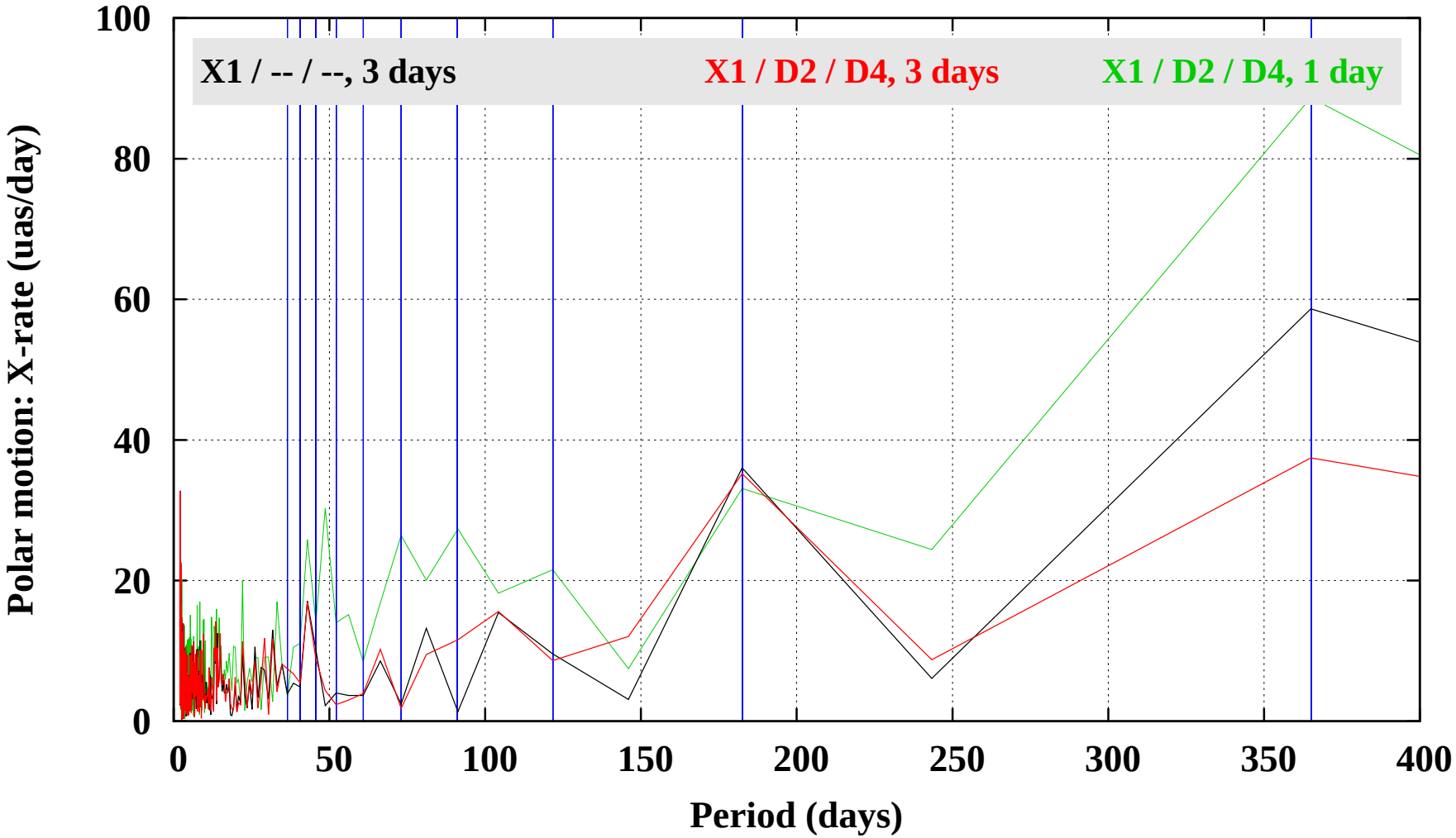

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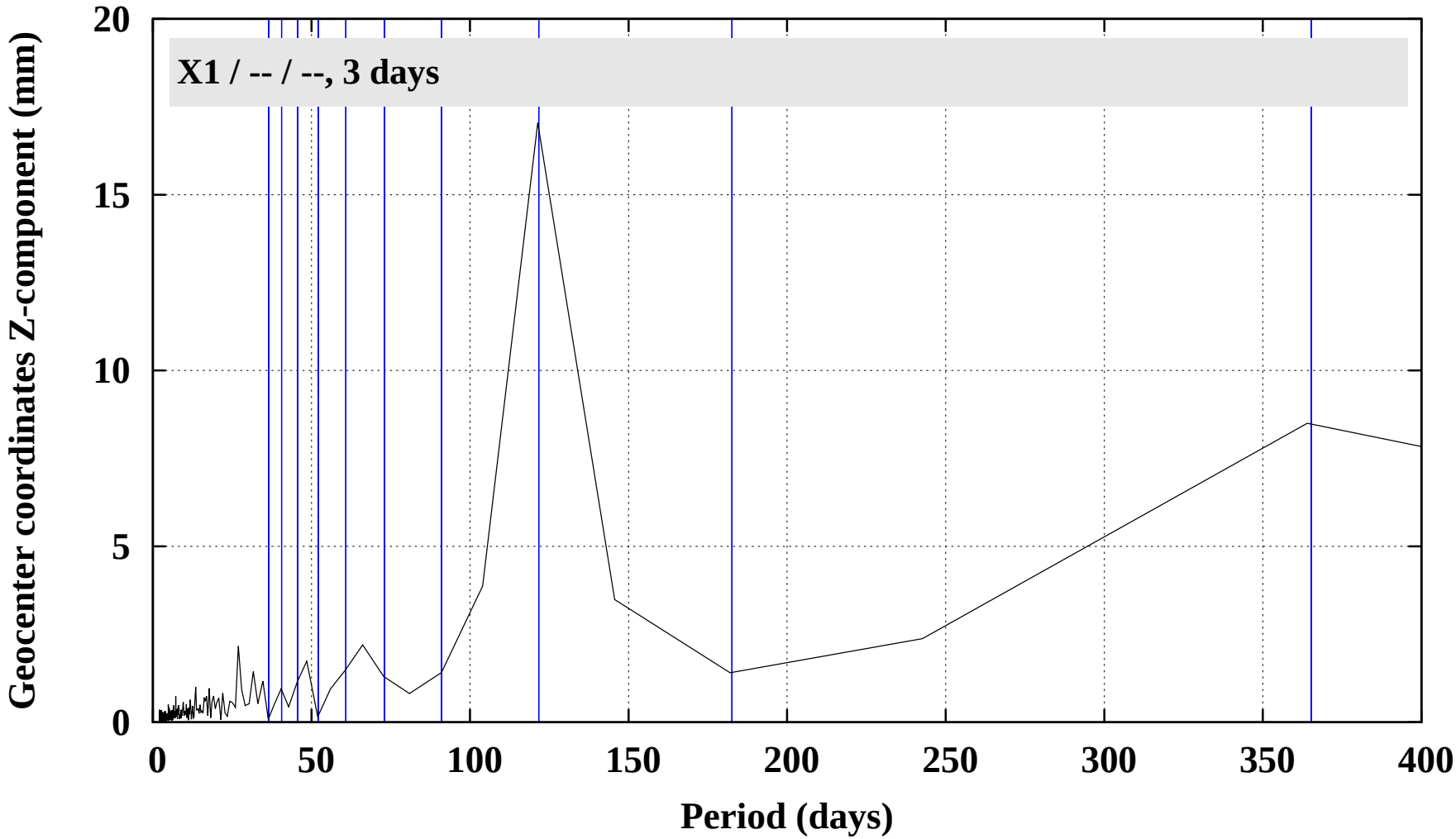

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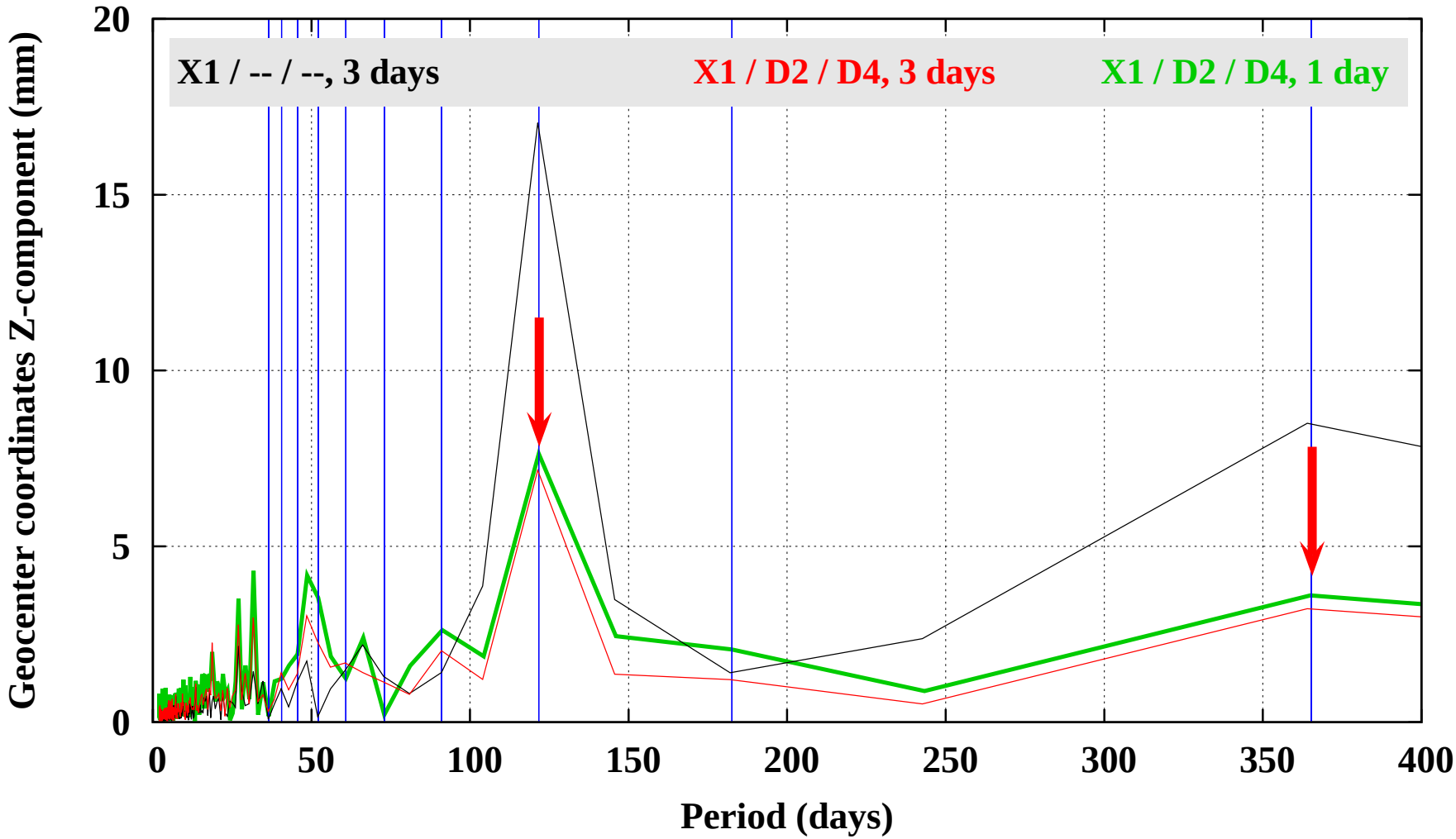

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- **CODE is currently preparing the transfer of this new orbit model into its operational IGS processing.**

THANK YOU
for your attention

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